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# SAR TEST REPORT

Dates of Tests: April 30, 2009

Test Report S/N: DR50110904BS

Test Site : DIGITAL EMC CO., LTD.

FCC ID

**XBQ-S5**

APPLICANT

**YUKYUNG TECHNOLOGIES INC.**

**Device name:** Real Pocket PC  
**Model Name:** S5 PREMIUM H  
**Manufacturer:** YUKYUNG TECHNOLOGIES INC.  
**Test Device Serial No.:** Identical prototype  
**TX Frequency Range:** 2412 ~ 2462 MHz (IEEE 802.11 b/g) / 2402~2480 MHz (Bluetooth)  
**RX Frequency Range:** 2412 ~ 2462 MHz (IEEE 802.11 b/g) / 2402~2480 MHz (Bluetooth)  
**Radio technology:** Wireless LAN: DSSS, OFDM / Bluetooth: FHSS  
**Max. Output power:** 18.03 dBm (802.11b) / 16.55 dBm (802.11g) / - 0.27 dBm (Bluetooth)  
**Max. SAR Measurement:** 0.681 mW/g (802.11b) , 0.279 mW/g (802.11g)  
**Application Type:** Certification  
**Rule Part(s):** §2.1093; FCC/OET Bulletin Supplement C[July 2001]  
**Data of issue:** April 30, 2009

This wireless portable device has been shown to be capable of compliance for localized specific absorption rate (SAR) for uncontrolled environment/general population exposure limits specified in ANSI/IEEE Std. C95.1-1992 and had been tested in accordance with the measurement procedures specified in FCC/OET Bulletin 65 Supplement C (2001) and IEEE Std. 1528-2003.

I attest to the accuracy of data. All measurements reported herein were performed by me or were made under my supervision and are correct to the best of my knowledge and belief. I assume full responsibility for the completeness of these measurements and vouch for the qualifications of all persons taking them.

Tested by :

Sun-Kyu Ryu (Engineer)

Reviewed by :

Harvey Sung (Chief Engineering Director)

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# 1. INTROCUCTION/SAR DEFINITION

In 1974, the International Radiation Protection Association (IRPA) formed a working group on non-ionizing radiation (NIR), which examined the problems arising in the field of Protection against the various types of NIR. At the IRPA Congress in Paris in 1977, this working group became the International Non-Ionizing Radiation Committee (INIRC).

In cooperation with the Environmental Health Division of the World Health Organization (WHO), the IRPA/INIRC developed a number of health criteria documents on NIR as part of WHO'S Environmental Health Criteria Programme, sponsored by the United Nations Environment Programme (UNEP). Each document includes an overview of the physical characteristics, measurement and instrumentation, sources, and applications of NIR, a thorough review of the literature on biological effects, and an evaluation of the health risks of exposure to NIR. These health criteria have provided the scientific database for the subsequent development of exposure limits and codes of practice relating to NIR.

At the Eighth International Congress of the IRPA (Monotreal, 18-22 May 1992), a new, independent scientific organization-the International Commission on Non-Ionizing Radiation Protection (ICNIRP)-was established as a successor to the IRPA/INIRC. The functions of the Commission are to investigate the hazards that may be association with the different forms of NIR, develop international guidelines on NIR exposure to static and extremely-low-frequency (ELF) electric and magnetic field have been reviewed by UNEP/WHO/IRPA (1984, 1987). Those publications and a number of others, including UNEP/WHO/IRPA (1993) and Allen et al. (1991), provided the scientific rationale for these guidelines.

A glossary of terms appears in the Appendix.

## SAR Definition

Specific Absorption Rate (SAR) is defined as the time derivative (rate) of the incremental energy (dU) absorbed by (dissipated in) an incremental mass (dm) contained in a volume element ( dV) of a given density (ρ) It is also defined as the rate of RF energy absorption per unit mass at a point in an absorbing body (see Fig. 1.1)

$$S A R = \frac{d}{d t} \left( \frac{d U}{d m} \right) = \frac{d}{d t} \left( \frac{d U}{\rho d v} \right)$$

**Figure 1.1**  
**SAR Mathematical Equation**

**SAR is expressed in units of Watts per Kilogram (W/kg).**

$$SAR = E^2 / \rho$$

Where:

- σ = conductivity of the tissue-simulant material (S/m)
- ρ = mass density of the tissue-simulant material (kg/m<sup>3</sup>)
- E = Total RMS electric field strength (V/m)

NOTE: The primary factors that control rate of energy absorption were found to be the wavelength of the incident field in relations to the dimensions and geometry of the irradiated organism, the orientation of the organism in relation to the polarity of field vectors, the presence of reflecting surfaces, and whether conductive contact is made by the organism with a ground plane.[6]

## 2. SAR MEASUREMENT SETUP

### Robotic System

Measurements are performed using the DASY4 automated dosimetric assessment system. The DASY4 is made by Schmid & Partner Engineering AG (SPEAG) in Zurich, Switzerland and consists of high precision robotics system (Staubli), robot controller, Pentium III computer, near-field probe, probe alignment sensor, and the generic twin phantom containing the brain equivalent material. The robot is a six-axis industrial robot performing precise movements to position the probe to the location (points) of maximum electromagnetic field (EMF) (see Fig. 2.1).

### System Hardware

A cell controller system contains the power supply, robot controller, teach pendant (Joystick), and a remote control used to drive the robot motors. The PC consists of the Micron Pentium IV 500 MHz computer with Windows NT system and SAR Measurement Software DASY4, A/D interface card, monitor, mouse, and keyboard. The Staubli Robot is connected to the cell controller to allow software manipulation of the robot. A data acquisition electronic (DAE) circuit that performs the signal amplification, signal multiplexing, AD-conversion, offset measurements, mechanical surface detection, collision detection, etc. is connected to the Electro-optical coupler (EOC). The EOC performs the conversion from the optical into digital electric signal of the DAE and transfers data to the PC plug-in card.

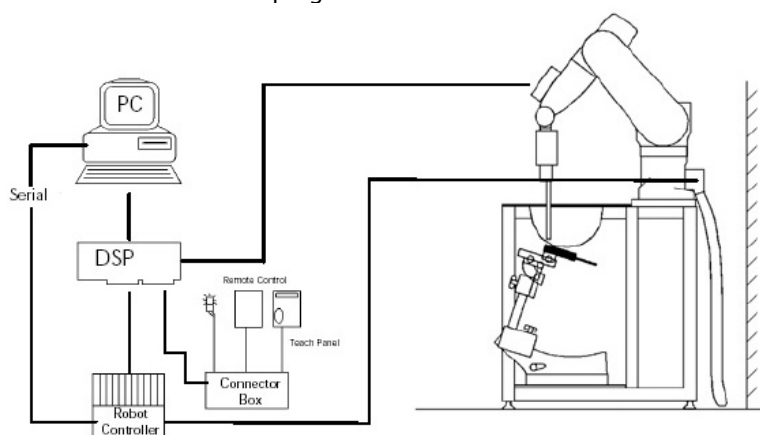


Figure 2.1 SAR Measurement System Setup

### System Electronics

The DAE3 consists of a highly sensitive electrometer-grade preamplifier with auto-zeroing, a channel and gain-switching multiplexer, a fast 16 bit AD-converter and a command decoder and control logic unit. Transmission to the PC-card is accomplished through an optical downlink for data and status information and an optical uplink for commands and clock lines. The mechanical probe mounting device includes two different sensor systems for frontal and sidewise probe contacts. They are also used for mechanical surface detection and probe collision detection. The robot uses its own controller with a built in VME-bus computer. The system is described in detail in [7].

### 3. SAR MEASUREMENT SETUP

#### Probe Measurement System



The SAR measurements were conducted with the dosimetric probe ET3DV6, designed in the classical triangular configuration [7] (see Fig. 3.2) and optimized for dosimetric evaluation. The probe is constructed using the thick film technique; with printed resistive lines on ceramic substrates. The probe is equipped with an optical multifiber line ending at the front of the probe tip (see Fig. 3.3). It is connected to the EOC box on the robot arm and provides an automatic detection of the phantom surface. Half of the fibers are connected to a pulsed infrared transmitter, the other half to a synchronized receiver. As the probe approaches the surface, the reflection from the surface produces a coupling from the transmitting to the receiving fibers. This reflection increases first during the approach, reaches maximum and then decreases. If the probe is flatly touching the surface, the coupling is zero. The distance of the coupling maximum to the surface is independent of the surface reflectivity and largely independent of the surface to probe angle. The DASY4 software reads the reflection during a software approach and looks for the maximum using a 2nd order fitting (see Fig.3.1). The approach is stopped at reaching the maximum.

Figure 3.1 DAE System

#### Probe Specifications

Calibration :	In air from 10 MHz to 6.0 GHz
	In brain and muscle simulating tissue at
	Frequencies of 900 MHz, 1810 MHz, 1950 MHz, 2450 MHz, 2600 MHz
Frequency :	10 MHz to 6 GHz
Linearity :	$\pm 0.2$ dB (30 MHz to 6 GHz)
Dynamic :	10 mW/kg to 100 W/kg
Range :	Linearity: $\pm 0.2$ dB
Dimensions:	Overall length: 330 mm
Tip length :	20 mm
Body diameter :	12 mm
Tip diameter:	2.5 mm
Distance from probe tip to sensor center:	1 mm
Application:	SAR Dosimetry Testing
	Compliance tests of mobile phones

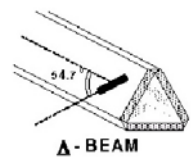


Figure 3.1 Triangular Probe Configuration



Figure 3.2 Probe Thick-Film Technique

## 4. Probe Calibration Process

### Dosimetric Assessment Procedure

Each probe is calibrated according to a dosimetric assessment procedure described in [8] with accuracy better than +/- 10%. The spherical isotropy was evaluated with the procedure described in [9] and found to be better than +/-0.25dB. The sensitivity parameters (NormX, NormY, NormZ), the diode compression parameter (DCP) and the conversion factor (ConvF) of the probe is tested.

### Free Space Assessment

The free space E-field from amplified probe outputs is determined in a test chamber. This is performed in a TEM cell for frequencies below 1 GHz (see Fig. 4.1), and in a waveguide above 1GHz for free space. For the free space calibration, the probe is placed in the volumetric center of the cavity at the proper orientation with the field. The probe is then rotated 360 degrees.

### Temperature Assessment \*

E-field temperature correlation calibration is performed in a flat phantom filled with the appropriate simulated brain tissue. The measured free space E-field in the medium correlates to temperature rise in a dielectric medium. For temperature correlation calibration a RF transparent thermistor-based temperature probe is used in conjunction with the E-field probe (see Fig. 4.2).

$$SAR = C \frac{\Delta T}{\Delta t}$$

$$SAR = \frac{|E|^2 \cdot \sigma}{\rho}$$

where:

$\Delta t$  = exposure time (30 seconds),

$C$  = heat capacity of tissue (brain or muscle),

$\Delta T$  = temperature increase due to RF exposure.

where:

$\sigma$  = simulated tissue conductivity,

$\rho$  = Tissue density (1.25 g/cm<sup>3</sup> for brain tissue)

SAR is proportional to  $\Delta T / \Delta t$ , the initial rate of tissue heating, before thermal diffusion takes place. Now it's possible to quantify the electric field in the simulated tissue by equating the thermally derived SAR to the E- field;

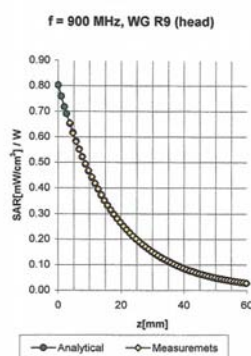


Figure 4.1 E-Field and Temperature Measurements at 900MHz[7]

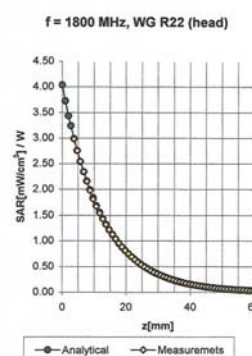


Figure 4.2 E-Field and Temperature Measurements at 1900MHz[7]

## 5. PHANTOM & EQUIVALENT TISSUES

### SAM Phantom



**Figure 5.1 SAM Twin Phantom**

The SAM Twin Phantom V4.0 is constructed of a fiberglass shell integrated in a wooden table. The shape of the shell is based on data from an anatomical study designed to determine the maximum exposure in at least 90% of all users [11][12]. It enables the dosimetric evaluation of left and right hand phone usage as well as body mounted usage at the flat phantom region. A cover prevents the evaporation of the liquid. Reference markings on the Phantom allow the complete setup of all predefined phantom positions and measurement grids by manually teaching three points in the robot. (see Fig. 5.1)

### Brain & Muscle Simulating Mixture Characterization



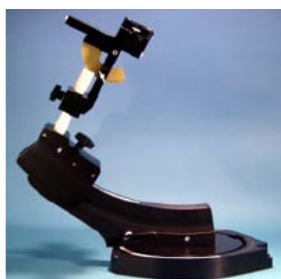
**Figure 5.2 Simulated Tissue**

The brain and muscle mixtures consist of a viscous gel using hydroxethyl cellulose (HEC) gelling agent and saline solution (see Table 6.1). Preservation with a bactericide is added and visual inspection is made to make sure air bubbles are not trapped during the mixing process. The mixture is calibrated to obtain proper dielectric constant (permittivity) and conductivity of the desired tissue. The head tissue dielectric parameters recommended by the IEEE SCC-34/SC-2 have been incorporated in the following table. Other head and body tissue parameters that have not been specified in P1528 are derived from the tissue dielectric parameters computed from the 4-Cole-Cole equations. The mixture characterizations used for the brain and muscle tissue simulating liquids are according to the data by C. Gabriel and G. Hartsgrrove [13]. (see Fig. 5.2)

**Table 5.1 Composition of the Brain & Muscle Tissue Equivalent Matter**

INGREDIENTS		SIMULATING TISSUE	
		2450MHz Brain	2450MHz Muscle
Mixture Percentage			
WATER		62.70	73.20
DGBE		0.000	26.70
SUGAR		0.000	0.000
SALT		0.500	0.040
BACTERICIDE		36.80	0.000
HEC		0.000	0.000
Dielectric Constant	Target	<b>39.2</b>	<b>52.7</b>
Conductivity (S/m)	Target	<b>1.80</b>	<b>1.95</b>

### Device Holder for Transmitters



**Figure 5.2 Mounting Device**

In combination with the SAM Twin Phantom V4.0, the Mounting Device (see Fig. 5.2) enables the rotation of the mounted transmitter in spherical coordinates where by the rotation point is the ear opening. The devices can be easily, accurately, and repeatably be positioned according to the FCC specifications. The device holder can be locked at different phantom locations (left head, right head, flat phantom).

- Note: A simulating human hand is not used due to the complex anatomical and geometrical structure of the hand that may produce infinite number of configurations [12]. To produce the worst-case condition (the hand absorbs antenna output power), the hand is omitted during the tests.



## 6. TEST SYSTEM SPECIFICATIONS

### Automated Test System Specifications

#### Positioner

<b>Robot:</b>	Stäubli Unimation Corp. Robot Model: RX60L
<b>Repeatability:</b>	0.02 mm
<b>No. of axis:</b>	6

#### Data Acquisition Electronic (DAE) System

##### Cell Controller

<b>Processor:</b>	Pentium 4 CPU
<b>Clock Speed:</b>	3 GHz
<b>Operating System:</b>	Window 2000
<b>Data Card:</b>	DASY4 PC-Board



Figure 6.1 DASY4 Test System

##### Data Converter

<b>Features:</b>	Signal, multiplexer, A/D converter. & control logic
<b>Software:</b>	DASY4
<b>Connecting Lines :</b>	Optical downlink for data and status info Optical uplink for commands and clock

#### PC Interface Card

<b>Function:</b>	24 bit (64 MHz) DSP for real time processing Link to DAE 3 16 bit A/D converter for surface detection system serial link to robot direct emergency stop output for robot
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#### E-Field Probes

<b>Model:</b>	EX3DV4 S/N: 3643
<b>Construction:</b>	Triangular core fiber optic detection system
<b>Frequency:</b>	10 MHz to 6 GHz
<b>Linearity:</b>	$\pm 0.2\text{dB}$ (30MHz to 6GHz)

#### Phantom

<b>Phantom:</b>	SAM Twin Phantom (V4.0)
<b>Shell Material :</b>	Vivac Composite
<b>Thickness:</b>	$2.0 \pm 0.2$ mm



## 7. DOSIMETRIC ASSESSMENT & PHANTOM SPECS

### Measurement Procedure

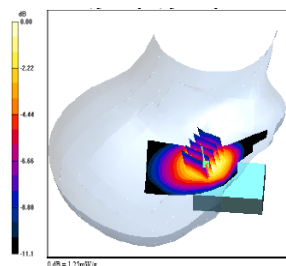


Figure 7.1 Sample Sar Area Scan

The evaluation was performed using the following procedure:

1. The SAR measurement was taken at a selected spatial reference point to monitor power variations during testing. This fixed location point was measured and used as a reference value.
2. The SAR distribution at the exposed side of the head was measured at a distance of 3.9mm from the Inner surface of the shell. The area covered the entire dimension of the head and the horizontal grid spacing was 15mm x 15mm.
3. Based on the area scan data, the area of the maximum absorption was determined by spline interpolation. Around this point, a volume of 30mm x 30mm x 30mm (fine resolution volume scan, zoom scan) was assessed by measuring 7 x 7 x 7 points. On this basis of this data set, the spatial peak SAR value was evaluated with the following procedure (see Fig. 7.1):
  - a. The data at the surface was extrapolated, since the center of the dipoles is 2.7 mm away from the tip of the probe and the distance between the surface and the lowest measuring point is 1.2mm. The extrapolation was based on a least square algorithm [15]. A polynomial of the fourth order was calculated through the points in z-axis. This polynomial was then used to evaluate the points between the surface and the probe tip.
  - b. The maximum interpolated value was searched with a straight-forward algorithm. Around this maximum the SAR values averaged over the spatial volumes (1g or 10g) were computed using the 3D-Spline interpolation algorithm. The 3D-spline is composed of three one-dimensional splines with the "Not a knot" condition (in x, y, and z directions) [15][16]. The volume was integrated with the trapezoidal algorithm. One thousand points (10 x 10 x 10) were interpolated to calculate the average.
  - c. All neighboring volumes were evaluated until no neighboring volume with a higher average value was found.
4. The SAR reference value, at the same location as procedure #1, was re-measured. If the value changed by more than 5%, the evaluation is repeated.

### Specific Anthropomorphic Mannequin (SAM) Specifications

The phantom for handset SAR assessment testing is a low-loss dielectric shell, with shape and dimensions derived from the anthropometric data of the 90th percentile adult male head dimensions as tabulated by the US Army. The SAM Twin Phantom shell is bisected along the mid-sagittal plane into right and left halves (see Fig. 7.2). The perimeter sidewalls of each phantom halves are extended to allow filling with liquid to a depth that is sufficient to minimize reflections from the upper surface. The liquid depth is maintained at a minimum depth of 15cm to minimize reflections from the upper surface.



Figure 7.2 SAM Twin Phantom shell

## 8. DEFINITION OF REFERENCE POINTS

### EAR Reference Point

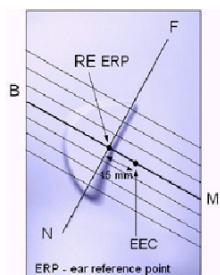


Figure 8.2 Close-up side view of ERPs

Figure 8.1 shows the front, back and side views of the SAM Twin Phantom. The point "M" is the reference point for the center of the mouth, "LE" is the left ear reference point (ERP), and "RE" is the right ERP. The ERPs are 15mm posterior to the entrance to the Ear canal (EEC) along the B-M line (Back-Mouth), as shown in Figure 9.2. The plane passing through the two ear canals and M is defined as the Reference Plane. The line N-F (Neck- Front) is perpendicular to the reference plane and passing through the RE (or LE) is called the Reference Pivoting Line (see Figure 8.2). Line B-M is perpendicular to the N-F line. Both N-F and B-M lines are marked on the external phantom shell to facilitate handset positioning [5]



Figure 8.1 Front, back and side view of SAM Twin Phantom

### Handset Reference Points

Two imaginary lines on the handset were established: the vertical centerline and the horizontal line. The test device was placed in a normal operating position with the "test device reference point" located along the "vertical centerline" on the front of the device aligned to the "ear reference point" (See Fig. 8.3). The "test device reference point" was then located at the same level as the center of the ear reference point. The test device was positioned so that the "vertical centerline" was bisecting the front surface of the handset at its top and bottom edges, positioning the "ear reference point" on the outer surface of the both the left and right head phantoms on the ear reference point.

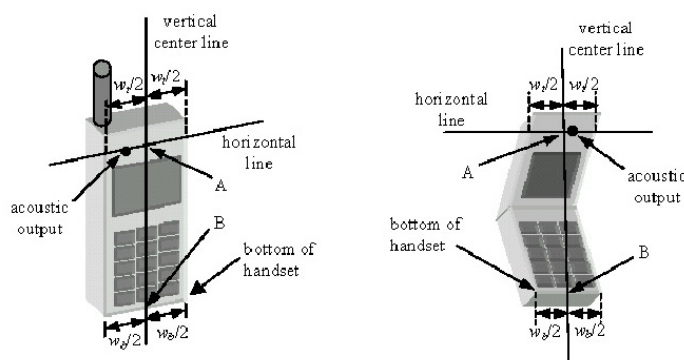


Figure 8.3 Handset Vertical Center & Horizontal Line Reference Points

## 9. TEST CONFIGURATION POSITIONS(Continued)

### Positioning for Cheek/Touch

1. The test device was positioned with the handset close to the surface of the phantom such that point A is on the (virtual) extension of the line passing through points RE and LE on the phantom (see Figure 9.1), such that the plane defined by the vertical center line and the horizontal line of the phone is approximately parallel to the sagittal plane of the phantom.



Figure 9.1 Front, Side and Top View of Cheek/Touch Position

2. The handset was translated towards the phantom along the line passing through RE & LE until the handset touches the ear.
3. While maintaining the handset in this plane, the handset was rotated around the LE-RE line until the vertical centerline was in the plane normal to MB-NF including the line MB (reference plane).
4. The phone was then rotated around the vertical centerline until the phone(horizontal line) was symmetrical with respect to the line NF.
5. While maintaining the vertical centerline in the reference plane, keeping point A on the line passing through RE and LE, and maintaining the phone contact with the ear, the handset was rotated about the line NF until any point on the handset made contact with a phantom point below the ear (cheek). See Figure 9.2)

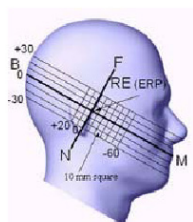


Figure 9.2 Side view w/ relevant markings

## 9. TEST CONFIGURATION POSITIONS(Continued)

### Positioning for Ear / 15 ° Tilt

With the test device aligned in the "Cheek/Touch Position":

1. While maintaining the orientation of the phone, the phone was retracted parallel to the reference plane far enough to enable a rotation of the phone by 15degree.
2. The phone was then rotated around the horizontal line by 15 degree.
3. While maintaining the orientation of the phone, the phone was moved parallel to the reference plane until any part of the phone touches the head. (In this position, point A was located on the line RE-LE). The tilted position is obtained when the contact is on the pinna. If the contact was at any location other than the pinna, the angle of the phone would then be reduced. The tilted position was obtained when any part of the phone was in contact of the ear as well as a second part of the phone was in contact with the head (see Figure 9.3).

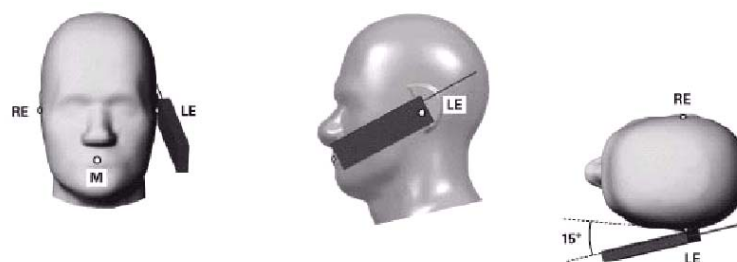


Figure 9.3 Front, Side and Top View of Ear/15° Tilt Position

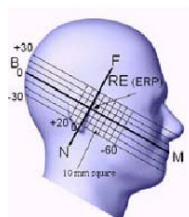


Figure 9.4 Side view w/ relevant markings

## 9. TEST CONFIGURATION POSITIONS

### Body Holster /Belt Clip Configurations

Body-worn operating configurations are tested with the belt-clips and holsters attached to the device and positioned against a flat phantom in a normal use configuration (see Figure 9.5). A device with a headset output is tested with a headset connected to the device. Body dielectric parameters are used.

Accessories for Body- worn operation configurations are divided into two categories: those that do not contain metallic components and those that do contain metallic components. When multiple accessories that do not contain metallic components are supplied with the device, the device is tested with only the accessory that dictates the closest spacing to the body. Then multiple accessories that contain metallic components are supplied with the device, the device is tested with each accessory that contains a unique metallic component. If multiple accessories share an identical metallic component (i.e. the same metallic belt-clip used with different holsters with no other metallic components) only the accessory that dictates the closest spacing to the body is tested.



**Figure 9.5 Body Belt Clip & Holster Configurations**

Body-worn accessories may not always be supplied or available as options for some Devices intended to be authorized for body-worn use. In this case, a test configuration where a separation distance between the back of the device and the flat phantom is used. All test position spacings are documented.

Transmitters that are designed to operate in front of a person's face, as in push-to-talk configurations, are tested for SAR compliance with the front of the device positioned to face the flat phantom. For devices that are carried next to the body such as a shoulder, waist or chest-worn transmitters, SAR compliance is tested with the accessory(ies), including headsets and microphones, attached to the device and positioned against a flat phantom in a normal use configuration.

In all cases SAR measurements are performed to investigate the worst-case positioning. Worst-case positioning is then documented and used to perform Body SAR testing. In order for users to be aware of the body-worn operating requirements for meeting RF exposure compliance, operating instructions and cautions statements are included in the user's manual.

## 10. ANSI / IEEE C95.1-1992 RF EXPOSURE LIMITS

### Uncontrolled Environment

UNCONTROLLED ENVIRONMENTS are defined as locations where there is the exposure of individuals who have no knowledge or control of their exposure. The general population/uncontrolled exposure limits are applicable to situations in which the general public may be exposed or in which persons who are exposed as a consequence of their employment may not be made fully aware of the potential for exposure or cannot exercise control over their exposure. Members of the general public would come under this category when exposure is not employment-related; for example, in the case of a wireless transmitter that exposes persons in its vicinity.

### Controlled Environment

CONTROLLED ENVIRONMENTS are defined as locations where there is exposure that may be incurred by persons who are aware of the potential for exposure, (i.e. as a result of employment or occupation). In general, occupational/controlled exposure limits are employment, who have been made fully aware of the potential for exposure and can exercise control over their exposure. This exposure category is also applicable when the exposure is of a transient nature due to incidental passage through a location where the exposure levels may be higher than the general population/uncontrolled limits, but the exposed person is fully aware of the potential for exposure and can exercise control over his or her exposure by leaving the area or by some other appropriate means.

Table 10.1.

SAR Human Exposure Specified in ANSI/IEEE C95.1-1992

	HUMAN EXPOSURE LIMITS	
	General Public Exposure (W/kg) or (mW/g)	Occupational Exposure (W/kg) or (mW/g)
Whole-Body average SAR (W/kg)	0.08	0.40
Localized SAR (head and trunk) (W/kg)	1.60	8.00
Localized SAR (limbs) (W/kg)	4.00	20.0

## 11. IEEE P1528 – MEASUREMENT UNCERTAINTIES

Error Description	Uncertainty value $\pm\%$	Probability Distribution	Divisor	(C <sub>i</sub> ) 1g	Standard (1g)	v <sub>i</sub> 2 or V <sub>eff</sub>
<b>Measurement System</b>						
Probe calibration	$\pm 4.8$	Normal	1	1	$\pm 4.8 \%$	$\infty$
Axial isotropy	$\pm 4.7$	Rectangular	$\sqrt{3}$	0.7	$\pm 1.9 \%$	$\infty$
Hemispherical isotropy	$\pm 9.6$	Rectangular	$\sqrt{3}$	0.7	$\pm 3.9 \%$	$\infty$
Boundary Effects	$\pm 1.0$	Rectangular	$\sqrt{3}$	1	$\pm 0.6 \%$	$\infty$
Probe Linearity	$\pm 4.7$	Rectangular	$\sqrt{3}$	1	$\pm 2.7 \%$	$\infty$
Detection limits	$\pm 1.0$	Rectangular	$\sqrt{3}$	1	$\pm 0.6 \%$	$\infty$
Readout Electronics	$\pm 1.0$	Normal	1	1	$\pm 1.0 \%$	$\infty$
Response time	$\pm 0.8$	Rectangular	$\sqrt{3}$	1	$\pm 0.5 \%$	$\infty$
Integration time	$\pm 2.6$	Rectangular	$\sqrt{3}$	1	$\pm 1.5 \%$	$\infty$
RF Ambient Conditions	$\pm 3.0$	Rectangular	$\sqrt{3}$	1	$\pm 1.7 \%$	$\infty$
Probe Positioner	$\pm 0.4$	Rectangular	$\sqrt{3}$	1	$\pm 0.2 \%$	$\infty$
Probe Positioning	$\pm 2.9$	Rectangular	$\sqrt{3}$	1	$\pm 1.7 \%$	$\infty$
Algorithms for Max. SAR Eval.	$\pm 1.0$	Rectangular	$\sqrt{3}$	1	$\pm 0.6 \%$	$\infty$
<b>Test Sample Related</b>						
Device Positioning	$\pm 2.9$	Normal	1	1	$\pm 2.9 \%$	145
Device Holder	$\pm 3.6$	Normal	1	1	$\pm 3.6 \%$	5
Power Drift	$\pm 5.0$	Rectangular	$\sqrt{3}$	1	$\pm 2.9 \%$	$\infty$
<b>Physical Parameters</b>						
Phantom Shell	$\pm 4.0$	Rectangular	$\sqrt{3}$	1	$\pm 2.3 \%$	$\infty$
Liquid conductivity (Target)	$\pm 5.0$	Rectangular	$\sqrt{3}$	0.64	$\pm 1.8 \%$	$\infty$
Liquid conductivity (Meas.)	$\pm 2.5$	Normal	1	0.64	$\pm 1.6 \%$	$\infty$
Liquid permittivity (Target)	$\pm 5.0$	Rectangular	$\sqrt{3}$	0.6	$\pm 1.7 \%$	$\infty$
Liquid permittivity (Meas.)	$\pm 2.5$	Normal	1	0.6	$\pm 1.5 \%$	$\infty$
<b>Combined Standard Uncertainty</b>					$\pm 10.3 \%$	330
<b>Expanded Uncertainty (k=2)</b>					$\pm 20.6 \%$	

The above measurement uncertainties are according to IEEE P1528 (2003)



## 12. SYSTEM VERIFICATION

### Tissue Verification

Table 12.1 Simulated Tissue Verification [5]

MEASURED TISSUE PARAMETERS					
Date(s)	Target Frequency	Dielectric constant: $\epsilon$		Conductivity: $\sigma$	
		Target	Measured	Target	Measured
April. 30, 2009	2450 MHz Brain	39.2	37.8	1.80	1.830
April. 30, 2009	2450 MHz Muscle	52.7	52.2	1.95	1.998

### Test System Validation

Prior to assessment, the system is verified to the  $\pm 10\%$  of the specifications at 2450 MHz by using the system validation kit(s). (Graphic Plots Attached)

Table 12.2 System Validation [5]

SYSTEM DIPOLE VALIDATION TARGET & MEASURED					
(2450 MHz values are normalized to a forward power of 1/4 W)					
Date(s)	System Validation Kit:	Target Frequency	Targeted SAR <sub>1g</sub> (mW/g)	Measured SAR <sub>1g</sub> (mW/g)	Deviation (%)
April. 30, 2009	D-2450V2, S/N: 726	2450 MHz Brain	13.1	13.6	3.82

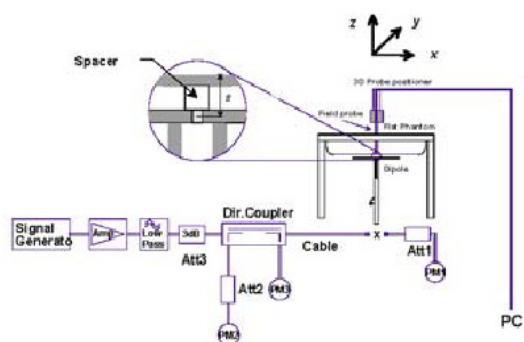


Figure 12.1 Dipole Validation Test Setup

## 13. SAR TEST DATA SUMMARY

### 13.1 SEE MEASUREMENT RESULT DATA PAGES

#### Procedures Used To Establish Test Signal

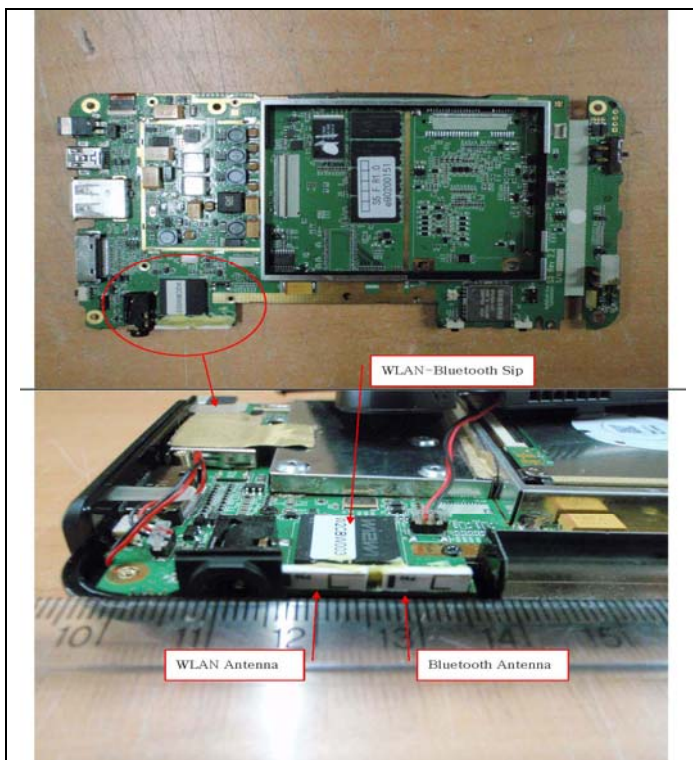
This device was tested WLAN test program to control DUT. The channel was selected at Low, Middle, and High channel. The output power level was set to rated max output power using the WLAN test program. This output power level was measured and recorded on the report as a begin power..

#### Device Test Conditions

This device is battery operated. Each SAR measurement was taken with a fully charged battery. In order to verify that the device was tested at full power, conducted output power measurements were performed before and after each SAR measurement to confirm the output power. If a conducted power deviation of more than 5% occurred, the test was repeated.

**Note :** The 802.11 b/g modes of this DUT were programmed to be in continuously transmitting mode.

### 13.2 DESCRIPTION OF ANTENNA LOCATION







**NOTE :** The closest separation distance between W-LAN and Bluetooth antenna

Antenna	W-LAN and BT
Distance	2 mm

## 13-1. TEST CONFIGURATION

**13.3 The following test configurations have been applied in this test report:**

	
<p><b>A:</b> The Back of the EUT face to the phantom with 0mm separation distance.</p>	<p><b>C:</b> The side of the EUT face to the phantom with 0mm separation distance.</p>
	
<p><b>B:</b> The Front of the EUT face to the phantom with 0mm separation distance.</p>	<p><b>D:</b> The Left Top of the EUT face to the phantom with 0mm separation distance.</p>

## 14. Configuring 802.11 a/b/g Transmitters for SAR Measurement

### 14.1 SAR Testing with IEEE 802.11 a/b/g Transmitters

Normal network operating configurations are not suitable for measuring the SAR of 802.11 a/b/g transmitters. Unpredictable in network traffic and antenna diversity conditions can introduce undesirable variations in SAR results. The SAR for these devices should be measured using chipset based test mode software to ensure the results are consistent and reliable.

### 14.2 General Device Setup

Chipset based test mode software is hardware dependent and generally varies among manufacturers. The device operating parameters established in test mode for SAR measurements must be identical to those programmed in production units, including output power levels, amplifier gain settings and other RF performance tuning parameters. The test frequencies should correspond to actual channel frequencies defined for domestic use. SAR for devices with switched diversity should be measured with only one antenna transmitting at a time during each SAR measurement, according to a fixed modulation and data rate. The same data pattern should be used for all measurements.

### 14.3 Frequency Channel Configurations

802.11 a/b/g and 4.9 GHz operation modes are tested independently according to the service requirements in each frequency band. 802.11 b/g modes are tested on channels 1, 6 and 11. 802.11a is tested for UNII operations on channels 36 and 48 in the 5.15-5.25 GHz Band; channels 52 and 64 in the 5.25-5.35 GHz band; channels 104, 116, 124 and 136 in the 5.470-5.725 GHz BAND; and channel 149 and 161 in the 5.8 GHz band. When 5.8 GHz § 15.247 is also available, channels 149, 157 and 165 should be tested of the UNII channels. 4.9 GHz is tested on channels 1, 10 and 5 or 6, whichever has the higher output power, for 5MHz channels; channels 11, 15 and 19 for 10MHz channels; and channels 21 and 25 for 20MHz channels. These are referred to as the " default test channels". 802.11g mode was evaluated only if the output power was 0.25 dB higher than the 802.11b mode.

Mode	GHz	Channel	Turbo Channel	"Default Test Channels"		UNII
				§15.247 802.11b	802.11g	
802.11 b/g	2.412	1 <sup>#</sup>		✓	✓	
	2.437	6	6	✓	✓	
	2.462	11 <sup>#</sup>		✓	✓	
802.11a	5.18	36				✓
	5.20	40	42 (5.21 GHz)			*
	5.22	44				*
	5.24	48	50 (5.25 GHz)			✓
	5.26	52				✓
	5.28	56	58 (5.29 GHz)			*
	5.30	60				*
	5.32	64				✓
	5.500	100	Unknown			*
	5.520	104				✓
	5.540	108				*
	5.560	112				*
	5.580	116				✓
	5.600	120				*
	5.620	124				✓
	5.640	128				*
	5.660	132				*
	5.680	136				✓
	5.700	140				*
	5.745	149		✓		✓
	5.765	153	152 (5.76 GHz)		*	*
	5.785	157		✓		*
	5.805	161	160 (5.80 GHz)		*	✓
	5.825	165		✓		

Table 14.1

802.11 Test channels per FCC Requirements

## 15. SAR TEST DATA SUMMARY

Mixture Type : 2450MHz body

15.1 MEASUREMENT RESULTS (W-LAN(802.11b) Body SAR)						
FREQUENCY		Begin Power (dBm)	End Power (dBm)	Spacing	Device Test Position	SAR (W/kg)
MHz	Ch					
2437	6	18.03	17.79	0 mm [Phantom]	A	0.029
2437	6	18.03	18.02	0 mm [Phantom]	B	0.088
<b>2412</b>	<b>1</b>	<b>17.74</b>	<b>17.74</b>	<b>0 mm [Phantom]</b>	<b>C</b>	<b>0.681</b>
2437	6	18.03	18.03	0 mm [Phantom]	C	0.637
2462	11	17.19	17.18	0 mm [Phantom]	C	0.547
2437	6	18.03	17.90	0 mm [Phantom]	D	0.037
2412(WLAN)+2402(B/T)	1 + 1	17.74	17.73	0 mm [Phantom]	C	*0.635
ANSI / IEEE C95.1 1992 – SAFETY LIMIT Spatial Peak Uncontrolled Exposure/General Population					Head 1.6 W/kg (mW/g) averaged over 1 gram	

NOTE:

1. The test data reported are the worst-case SAR value with the antenna-head position set in a typical configuration. Test procedures used are according to FCC/OET Bulletin 65, Supp.C [July 2001].
2. All modes of operation were investigated, and worst-case results are reported.
3. Prior to testing the conducted output power was measured.
4. The EUT is tested 2<sup>nd</sup> hot-spot peak, if it is less than 2dB below the highest peak.
5. Battery is fully charged for all readings.
6. Test Signal Call Mode ☒ Continuous Tx On ☐ Manu. Test Codes ☐ BaseStation Simulator
7. Tissue parameters and temperatures are listed on the SAR plots.
8. Liquid tissue depth is 15.0 cm.±0.1
9. \* Simultaneous SARs were repeated with each worst case channel of W-LAN and B/T on
10. The 802.11 b/g modes of this DUT were programmed to be in continuously transmitting mode.

## 15. SAR TEST DATA SUMMARY

Mixture Type : 2450MHz body

15.2 MEASUREMENT RESULTS (W-LAN(802.11g) Body SAR)						
FREQUENCY		Begin Power (dBm)	End Power (dBm)	Spacing	Device Test Position	SAR (W/kg)
MHz	Ch					
2437	6	16.55	16.30	0 mm [Phantom]	A	0.018
2437	6	16.55	16.51	0 mm [Phantom]	B	0.031
<b>2412</b>	<b>1</b>	<b>16.26</b>	<b>16.12</b>	<b>0 mm [Phantom]</b>	<b>C</b>	<b>0.279</b>
2437	6	16.55	16.55	0 mm [Phantom]	C	0.263
2462	11	16.34	16.32	0 mm [Phantom]	C	0.240
2437	6	16.55	16.26	0 mm [Phantom]	D	0.017
ANSI / IEEE C95.1 1992 - SAFETY LIMIT Spatial Peak Uncontrolled Exposure/General Population					Head 1.6 W/kg (mW/g) averaged over 1 gram	

### NOTE:

1. The test data reported are the worst-case SAR value with the antenna-head position set in a typical configuration. Test procedures used are according to FCC/OET Bulletin 65, Supp.C [July 2001].
2. All modes of operation were investigated, and worst-case results are reported.
3. Prior to testing the conducted output power was measured.
4. The EUT is tested 2nd hot-spot peak, if it is less than 2dB below the highest peak.
5. Battery is fully charged for all readings.
6. Test Signal Call Mode ☒ Continuous Tx On ☐ Manu. Test Codes ☐ Base Station Simulator
7. Tissue parameters and temperatures are listed on the SAR plots.
8. Liquid tissue depth is 15.0 cm.±0.1
9. The 802.11 b/g modes of this DUT were programmed to be in continuously transmitting mode.
10. Simultaneous SAR test was not performed in 802.11g mode since simultaneous SAR test was performed in 802.11b mode as the worst case

## 16. SAR TEST EQUIPMENT

**Table 16.1 Test Equipment Calibration**

EQUIPMENT SPECIFICATIONS			
Type	Calibration Date	Next Calibration Date	Serial Number
Robot	N/A	N/A	F02/5Q85A1/A/01
Robot Controller	N/A	N/A	F02/5Q85A1/C/01
Joystick	N/A	N/A	D221340031
Hicron Computer 1.1GHz Pentium Celeron ,Window 2000	N/A	N/A	N/A
Data Acquisition Electronics	November 12, 2008	November 12, 2009	519
Dosimetric E-Field Probe	January 14, 2009	January 14, 2010	3643
Dummy Probe	N/A	N/A	N/A
Sam Phantom	N/A	N/A	N/A
Probe Alignment Unit LB	N/A	N/A	321
SPEAG Validation Dipole D835 MHz	January 28, 2008	January 28, 2010	464
SPEAG Validation Dipole D1900 MHz	March 17, 2009	March 17, 2011	5d029
SPEAG Validation Dipole D2450 MHz	March 17, 2009	March 17, 2011	726
Head/Body Equivalent Matter(835 MHz)	January 2009	January 2010	N/A
Head/Body Equivalent Matter(1900 MHz)	January 2009	January 2010	N/A
Head/Body Equivalent Matter(2450 MHz)	January 2009	January 2010	N/A
HP EPM-442A Power Meter	March 13, 2009	March 13, 2010	GB37170267
HP E4421A Signal Generator	July 09, 2008	July 09, 2009	US37230529
Attenuator (10dB)	January 19, 2009	January 19, 2010	BP4387
Attenuator (3dB)	July 15, 2008	July 15, 2009	MY39260699
Low pass filter (1.5GHz)	February 03, 2009	February 03, 2010	N/A
Low pass filter (3.0GHz)	October 01, 2008	October 01, 2009	N/A
Dual Directional Coupler	February 03, 2009	February 03, 2010	50228
Amplifier	February 02, 2009	February 02, 2010	1020 D/C 0221
Network Analyzer	March 13, 2009	March 13, 2010	8753D
HP85070D Dielectric Probe Kit	N/A	N/A	LISO1440118
SEMITEC Engineering	N/A	N/A	Shield Room

**NOTE:**

The E-field probe was calibrated by SPEAG, by temperature measurement procedure. Dipole Validation measurement is performed by Digital EMC. before each test. The brain simulating material is calibrated by Digital EMC using the dielectric probe system and network analyzer to determine the conductivity and permittivity (dielectric constant) of the brain-equivalent material.



## 17. CONCLUSION

### Measurement Conclusion

The SAR measurement indicates that the EUT complies with the RF radiation exposure limits of the FCC. These measurements are taken to simulate the RF effects exposure under worst-case conditions. Precise laboratory measures were taken to assure repeatability of the tests. The tested device complies with the requirements in respect to all parameters subject to the test. The test results and statements relate only to the item(s) tested.

Please note that the absorption and distribution of electromagnetic energy in the body are very complex phenomena that depend on the mass, shape, and size of the body, the orientation of the body with respect to the field vectors, and the electrical properties of both the body and the environment. Other variables that may play a substantial role in possible biological effects are those that characterize the environment (e.g. ambient temperature, air velocity, relative humidity, and body insulation) and those that characterize the individual (e.g. age, gender, activity level, debilitation, or disease).

Because innumerable factors may interact to determine the specific biological outcome of an exposure to electromagnetic fields, any protection guide shall consider maximal amplification of biological effects as a result of field-body interactions, environmental conditions, and physiological variables.

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