H500V Sub6_mmw Part0 RF Exposure Report

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1. Product Description

Product Type	Mobile Hotspot
Product Name	H500V
	WCDMA Band II: 1850 MHz ~ 1910 MHz
	WCDMA Band IV: 1710 MHz ~ 1755 MHz
	WCDMA Band V: 824 MHz ~ 849 MHz
	LTE Band 2: 1850 MHz ~ 1910 MHz
	LTE Band 4: 1710 MHz ~ 1755 MHz
	LTE Band 5: 824 MHz ~ 849 MHz
	LTE Band 7: 2500 MHz ~ 2570 MHz
	LTE Band 12: 699 MHz ~ 716 MHz
	LTE Band 13: 777 MHz ~ 787 MHz
	LTE Band 17: 704 MHz ~ 716 MHz
Operated Band	LTE Band 46 (RX): 5150 MHz ~ 5925 MHz
	LTE Band 48: 3550 MHz ~ 3700 MHz
	LTE Band 66: 1710 MHz ~ 1780 MHz
	5G NR n2: 1850 MHz ~ 1910 MHz
	5G NR n5: 824 MHz ~ 849 MHz
	5G NR n48: 3550 MHz ~ 3700 MHz
	5G NR n66: 1710 MHz ~ 1780 MHz
	5G NR n77: 3450 MHz ~ 3550 MHz; 3700 MHz ~ 3980 MHz
	5G NR n78: 3450 MHz ~ 3550 MHz; 3700 MHz ~ 3800 MHz
	5G NR n260 :37 GHZ~40 GHz5G
	NR n261 : 27.5 GHz~28.35 GHz

Table 1-1 Production describtion

2. SAR Characterization

SAR char must be generated to cover all radio configurations and usage scenarios that the wireless device supports for operating at 6 GHz or below. It will then be used as input for Smart Transmit to control and manage RF exposure for f < 6 GHz. Table 2.1 Usage scenarios in SAR evaluation SAR char should be evaluated per the wireless device position relative to the human body. For a smartphone operating at frequencies < 6 GHz, SAR must be evaluated at low, mid, and high channels for each supported band, technology, and Tx antenna in usage scenarios described in Table 2-1.

Scenario	DSI State	Description					
Full power	0	Full power					
	1	LB SA/NSA					
	2	UHB NSA					
	3	Wifi2 Standalone					
	4	MHB NSA					
	5	WIFI1 Standalone					
	6	UHB SA/NSA					
	7	MHB SA/NSA					
Body	8	MHB NSA+WIFI1					
	9	UHB SA + WIFI1					
	10	MHB SA/NSA + WIFI2					
	11	LB SA/NSA + WIFI2					
	12	LB + UHB NSA					
	13	MHB + UHB + WIFI1					
	14	LB + UHB NSA + WIFI2					
	15	ALL simultaneously					

Table 2-1 Usage scenarios

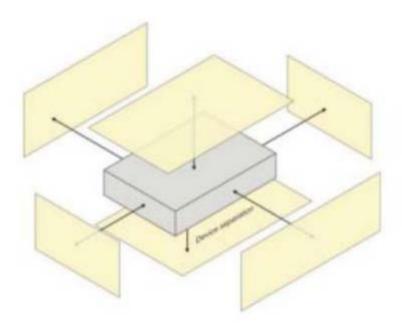


Figure 2-1 Illustration for Hotspot Position

The device state index (DSI) represents each usage scenario (or exposure scenario). Depending on the detection scheme implemented in the smartphone, the worst-case SAR is further grouped and determined for each or combined exposure scenario(s):

If the device does not have any detection mechanism (all "no" in Figure 2-2), then the worst- case 1gSAR is determined by taking the maximum 1gSAR value among all exposure scenarios, i.e., worst-case 1gSAR = max{SARhead, SARhotypot}.

If the device can distinguish each of the above scenarios (all "yes" in Figure 2-2), then the worst-case 1gSAR for each individual exposure scenario is given by corresponding SARhead, SARbody, and SAR hotspot.

If the device can only distinguish a subset of the scenarios (some "yes", some "no" in Figure 2-2), then the worst-case SAR is given by:

Corresponding 1gSAR for each exposure scenario that can be distinguished (DSI=yes) Maximum 1gSAR among all other exposure scenario(s) that cannot be distinguished (DSI=no)

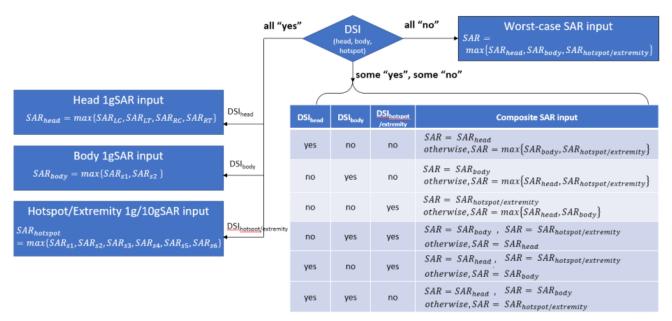


Figure 2-2 Worst-case 1gSAR determination based on DSI

2.1 SAR char generation

The design target for SAR compliance (1gSAR compliance for FCC), denoted as SAR_design_target, must be specified before generating SAR char.

SAR char determines the power level the device meets the SAR_design_target for each radio configuration and usage case supported. For SAR char generation, the SAR measurement should be performed in a static Tx power transmission mode, i.e., FTM mode at maximum power, or with callbox requesting maximum power and Smart Transmit disabled. To generate SAR char for a EUT:

1. Specify SAR_design_target: The SAR_design_target shall be less than regulatory SAR limit (i.e., 1gSAR limit for FCC) after accounting for all device design related uncertainties.

- 2. Measure conducted power and SAR for each Tx antenna and supported technology/band. For a given technology/band, if the device supports multiple modulations (for example, QPSK, 16-QAM and 64-QAM in the case of LTE), then measurement on one modulation is sufficient for SAR char generation. For each supported band, SAR is evaluated at low, mid, high channels and the highest SAR among the three channels is chosen for the respective band.
- 3. Based on 1gSAR values obtained in Step 2, see Figure 2-2 to derive the worst-case 1gSAR for each DSI (i.e., DSI = "yes") and for all Tx antenna and supported technology/band.
- 4. Determine the Tx power level at which the corresponding worst-case 1gSAR is equal to SAR_design_target for each DSI and for all Tx antenna and supported technology/band.
- 5. FCC has specified 1gSAR and 10gSAR for different RF exposure scenarios. In this case, SAR_design_target is defined for 1gSAR first, and then calculate the Tx power level at which the corresponding worst-case 10gSAR is equal to the design target for 10gSAR compliance, SAR_design_target_extremity, as follows:
 - a. Derive SAR_design_target_extremity for hand exposure scenario using

$$SAR_design_target_extremity \ = \frac{SAR_design_target}{1gSAR\ limit} \times 10gSAR\ limit$$

- b. Determine the Tx power level that corresponds to SAR_design_target_extremity for all Tx antenna and supported technologies/bands, denoted as Tx_power_at_SAR_design_target_extremity
- 6. Generate SAR char and tabulate Tx_power_at_SAR_design_target versus DSI for each Tx antenna and for all supported technologies/bands.

2.2 SAR design target and uncertainty

The total device design and related uncertainties of the EUT, including TXAGC and device to device variation, are accounted for in the SAR design Target per the following equation:

$$\mathit{SAR}_{\mathit{Design}\,\mathit{Target}} < \mathit{SAR}_{\mathit{regulatory}_{limit}} \times 10^{\frac{-total\,\mathit{uncertainty}}{10}}$$

For the FCC SAR requirement of 1.6W/Kg , the SAR design target for the EUT is determined as :

CAD regulary limit(\M/Ka)	Total upcortainty/dP)	SAR design
SAR regulary limit(W/Kg)	Total uncertainty(dB)	target(W/Kg)
1.6	1	1.2

Per FCC, KDB Publication 447498 D01v06, when SAR is not measured at the maximum power level allowed for production units, the results must be scaled to the maximum tune-up tolerance limit according to the power applied to the individual channels tested to determine compliance, For simultaneous transmission. the measured aggregate SAR must be scaled according to the sum of the differences between the maximum tune-up tolerance and actual power used to test each transmitter. When SAR is measured at or scaled to the maximum tune-up tolerance limit, the results are referred to as reported SAR

2.3 Worst case reported SAR

	Worst Case Reported SAR										
Exposure Scenario						Hotsp	oot				
Antenna	Antenna	AN	Γ0		ANT4	AN	T2	I	ANT3	ANT1	
Transmission mode	Antenna	Standalone	Simultaneous	Standalone	Simultaneous	Standalone	Simultaneous	Standalone	Simultaneous	Standalone	Simultaneous
Power Mode(DSI)		DS7	DSI10/15	DSI1	DSI11/12/14/15	DSI6	DSI9/13/15	DSI2	DSI12/14/15	DSI4	DSI8/13/15
WCDMA Band II	ANT0	0.797	1	/	1	1	1	1	1	/	1
WCDMA Band IV	ANT0	0.780	/	/	1	/	1	1	1	1	1
WCDMA Band V	ANT4	1	1	0.382	0.342	1	1	1	1	1	1
LTE Band 2	ANT0	0.683	0.539	1	1	/	1	1	1	1	1
LTE Band 5	ANT4	1	1	0.337	0.292	1	1	1	1	1	1
LTE Band 7	ANT0	0.741	1	/	1	/	1	1	1	1	1
LTE Band 12/17	ANT4	1	1	0.457	0.312	/	1	1	1	1	1
LTE Band 13	ANT4	1	1	0.421	0.300	/	1	1	1	1	1
LTE Band 48	ANT2	1	/	/	1	1.007	0.319	1	1	/	1
LTE Band 48	ANT3	1	1	1	1	1	1	1	0.797	1	1
LTE Band 4/66	ANT0	0.609	0.497	/	1	/	1	1	1	1	1
LTE Band 4/66	ANT1	1	1	1	1	1	1	1	1	1	0.367
5G NR N2	ANT0	0.697	0.493	1	1	/	1	1	1	1	1
5G NR N2	ANT1	1	1	/	1	/	1	1	1	1	0.590
5G NR N5	ANT4	1	1	0.532	0.210	1	1	1	1	1	1
5G NR N48	ANT2	1	1	1	1	1.009	0.267	1	1	1	1
5G NR N66	ANT0	0.750	0.468	1	1	1	1	1	1	1	1
5G NR N66	ANT1	/	1	/	1	/	1	1	1	/	0.217
5G NR N77	ANT2	1	1	1	1	1.103	0.220	1	1	1	1
5G NR N77	ANT3	1	1	/	1	1	1	1	0.776	1	1
5G NR N78	ANT2	1	1	1	1	1.088	0.294			1	1

Table 2.3-1 Worst case reported SAR

2.4 SAR characterization

	DSI	0		2	3	4	5	6	7	8	9	10	11	12	13	14	15
			Doob						I								
Tools Doord	category	Body	Body	Body	Body	Body	Body	Body	Body	Body	Body	Body	Body	Body	Body	Body	Body
Tech_Band	Antenna	Tx powe	Tx powe	Tx powe	Tx powe	Tx powe	Tx powe	Tx powe		Tx powe		Tx powe	Tx powe		Tx powe		
LTE_B1 LTE_B12	0	23	23	23 23		23 23		23	23 23	23 23		23 23	23		23		
LTE_B12	4	23	23	23				23							23		
	4							23		23		23			23		
LTE_B17	0	23	23	23						23		23			23		
LTE_B2	0	23	23	23 23						23		22					
LTE_B2	1	23	23							23							
LTE_B20	4		23	23				23		23		23					
LTE_B28	4	23	23	23						23		23					
LTE_B3	·	23	23	23						23							
LTE_B4	0	23	23	23				23		23		22					
LTE_B4	2	23	23	23						21	23	23					
LTE_B48	2	23	23	23				21	23	23		23					
LTE_B48	3	23	23	23						23		23					
LTE_B5	4	23	23	23						23		23			23		
LTE_B66	0	23	23	23		23		23		23		22	23				
LTE_B66	1	23	23	23				23		21	23	23					
LTE_B7	0	23	23	23				23		23		23					
NR5G_N2	0	23	23	23				23		23		22					
NR5G_N2	1	23	23	23						23		23					
NR5G_N48	2	23	23	23						23		23					
NR5G_N48	3	23	23	23						23							
NR5G_N5	4	23	23	23				23		23		23					
NR5G_N66	0	23	23	23		23		23		23		22	23				
NR5G_N66	1	23	23	23						21		23					
NR5G_N77	2	23	23	23				17		23		23					
NR5G_N77	3	23	23	23						23		23					
NR5G_N77	0	23	23	23				23		23		23					
NR5G_N77	1	23	23	23						23		23					
NR5G_N78	2	23	23	23					23	23		23					
NR5G_N78	3	23	23	23						23		23					
NR5G_N78	0	23	23	23						23		23					
NR5G_N78	1	23	23	23				23		23		23					
WCDMA_B1	0	23	23	23		23		23		23		23					
WCDMA_B2	0	23	23	23						23		23					
WCDMA_B4	0	23	23	23						23		23					
WCDMA_B5	4	23	23	23						23							
WCDMA_B8	4	23	23	23	23	23	23	23	23	23	23	23	23	23	23	23	23

Table 2.4-1 SAR characterization

3. PD characterization

3.1 Electromagnetic simulation method for power density

EM simulation tool description

The mmWave power density (PD) simulation method for calculating PD (Power Density) for mobile phones with mmWave antenna modules is available in ANSYS Electromagnetics suite HFSS ver. 21.1 (2021 R1) is used. ANSYS HFSS is one of several commercial tools for 3D fullwave electromagnetic simulation used for antenna and RF structure design of high frequency component. ANSYS Electromagnetics suite HFSS ver. 21.1 (2021 R1) is implemented based on Finite Element Method (FEM), which operates in the frequency domain.

Mesh and convergence criteria

ANSYS Electromagnetic suite HFSS ver. 21.1 (2021 R1) uses the Finite Element Method (FEM) to solve the structure for 3D EM simulations to analyze power density. The volume area containing the simulated object should be subdivided into electrically small parts called finite elements with unknown functions. To subdivide system, the adaptive mesh technique in ANSYS Electromagnetics suite HFSS ver. 21.1 (2021 R1) is used. ANSYS Electromagnetics suite HFSS ver. 21.1 (2021 R1) starts to refine the initial mesh based on wavelength and calculate the error to iterative process for adaptive mesh refinement. The determination parameter of the number of iterations in ANSYS Electromagnetics suite HFSS ver. 21.1 (2021 R1) is defined as convergence criteria, delta S, and the iterative adaptive mesh process repeats until the delta S is met. In ANSYS Electromagnetics suite HFSS ver. 21.1 (2021 R1), the accuracy of converged results depends on the delta S. Figure 1 is an example of final adaptive mesh of the device (cross-section of top view).

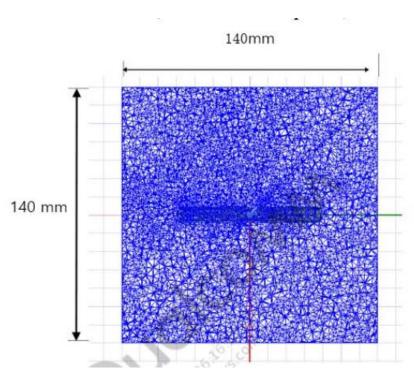


Figure 3.1-1: Example of HFSS mesh in a model of the device (Top view)

Time-averaged power density calculation

It is possible to get various kinds of physical quantities can be obtained after finishing 3D fullwave electromagnetic simulation. To calculate PD evaluation, two physical quantities, an electric field () and a magnetic field () are needed. The actual consumption power can be expressed as the real term of the time-averaged Poynting vector () from the cross product of and complex conjugation of as shown below:

$$(\vec{S}) = \operatorname{Re}(\frac{1}{2}\vec{E} \times \vec{H}^*)$$

(can be expressed as point power density based on a peak value of each spatial point on mesh grids and obtained directly from ANSYS Electromagnetics suite HFSS ver. 21.1 (2021 R1). From the point power density (, the spatial-averaged power density () on an evaluated area (A) can be derived as shown below:

$$PD_{av} = \frac{1}{A} \int_{A} \overrightarrow{(S)} . ds = \frac{1}{2A} \int_{A} |Re(\vec{E} \times \vec{H} *)| . ds$$

Simulation setup

Modeling for simulation

The simulation approach to perform PD assessment for a smartphone requires accurate modeling for mmWave antenna module as well as the smartphone itself. Figure shows the simulation model which is mounted one mmWave antenna module. The simulation modeling includes most of the entire structure of device itself such as PCB, metal frame, battery, cables, and legacy antennas as well as mmWave antenna module called as QMTO#. The position of QTMO#(module0) as the pictures of attachment (Figure 3.1-1).

PD evaluation surfaces

Attached Figure (Figure 3.1-2) shows the PD evaluation planes and truncation area of the simulation model to find worst case surfaces for evaluation. Table 1-1 shows the surfaces selected for PD evaluation planes for QTM#0

Please note that the "right" and "left" edge of mentioned in this report are defined from the perspective of looking at the device from the front side.

	Table 3.1 1. 1D evaluation surfaces								
			Left	Right					
	Front	Back	From Front	From Front	Тор	Bottom			
			View	View					
	S1	S2	S3	S4	S5	S6			
QTM#O	√	√				√			

Table 3.1-1: PD evaluation surfaces

Radiation boundary condition

For radiation boundary, the 2nd order absorbing boundary condition (ABC) is used for all simulations in this report. This radiation boundary simulates an electrically open surface that allows waves to radiate infinitely far into space. The system absorbs the wave via the 2nd order radiation boundary, essentially ballooning the boundary infinitely far away from the structure and into space. The radiation boundaries may also be placed relatively close to a structure and can be of arbitrary shape.

Per ANSYS recommendations for their simulation tool, the radiation boundary plane must be located at least a quarter wavelength from strongly radiating structure, or at least a tenth of a wavelength from a weakly radiating structure. In this simulation report, about two or three wavelengths spacing from the device surfaces in all main beam directions are applied to ensure convergence.

By changing convergence error (i.e., maximum magnitude delta S) from 2% to 4% and moving the radiation boundary closer towards the device by 20%, the combined influence in PD value is < 0.04 dB which confirms that the simulation model is reliable using this setup.

Source excitation condition

Each of the two 5G mmWave array modules is the same part containing a 1x4 element array of dual-polarization patch antennas. The number of antenna ports of QTM#O and QTM#1for source excitation is equal to 16. The port of each patch antenna is separated in frequency and polarization. That is, the ports of each patch antenna are divided into a feed for 28 GHz and a feed for 39 GHz, and a vertical polarity feed and a horizontal polarity feed are divided. Pictrue "EUT simulation model" as attachment shows the QTM#1 module structure and surrounding structure. The QTM#1 module is encrypted in the ANSYS Electromagnetics suite (HFSS) and can only check the feeding position is encrypted in the ANSYS Electromagnetics suite (HFSS) and can only check the feeding position.

After finishing 3D full wave electromagnetic simulation of modeling structure, the magnitude and phase information and be loaded for each port by using "Edit Sources" function in ANSYS Electromagnetics suite (HFSS). Figure 2 shows an example of antenna port excitations.

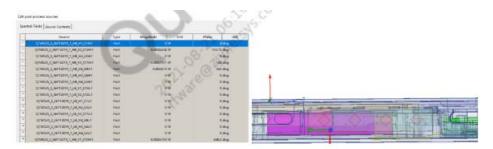


Figure 3.1-3: An example of port excitation (QTM#1)

Since ANSYS Electromagnetics suite (HFSS) uses FEM solver based on frequency domainanalysis method, the input source for the port excitation applies sinusoidal waveform for each frequency.

Condition of simulation completion

The simulation completion condition of ANSYS Electromagnetics suite (HFSS) is defined as delta S. The ANSYS Electromagnetics suite (HFSS) calculates the S-parameter for the mesh conditions of each step and determines whether to proceed with the operation of the next step by comparing the difference between the S-parameters in the previous step. A difference between the previous step and the current step of S-parameter is expressed as delta S, and the delta S generally sets 0.02. The simulation result of this report is the result of setting delta S to 0.02.

3.2. Codebook

The codebook supported by this EUT is shown in Table 3.2-1 below.

N260 codebook

Band	Beam_ID	Module	Ant_Group	Ant_Type	Ant_Feed	Paired_With
260	0	0	0	PATCH	13	128
260	1	0	0	PATCH	12	129
260	2	0	0	PATCH	11	130
260	3	0	0	PATCH	10	131
260	4	0	0	PATCH	9	132
260	5	0	0	PATCH	11;10	133
260	6	0	0	PATCH	11;10	134
260	7	0	0	PATCH	12;11	135
260	8	0	0	PATCH	10;9	136
260	9	0	0	PATCH	10;9	137
260	10	0	0	PATCH	11;10	138
260	11	0	0	PATCH	11;10	139
260	12	0	0	PATCH	13;12;11;10;9	140
260	13	0	0	PATCH	13;12;11;10;9	141
260	14	0	0	PATCH	13;12;11;10;9	142
260	15	0	0	PATCH	13;12;11;10;9	143
260	16	0	0	PATCH	13;12;11;10;9	144
260	17	0	0	PATCH	13;12;11;10;9	145
260	18	0	0	PATCH	13;12;11;10;9	146
260	19	0	0	PATCH	13;12;11;10;9	147
260	20	0	0	PATCH	13;12;11;10;9	148
260	128	0	1	PATCH	4	0
260	129	0	1	PATCH	5	1
260	130	0	1	PATCH	3	2
260	131	0	1	PATCH	2	3
260	132	0	1	PATCH	1	4
260	133	0	1	PATCH	5;3	5
260	134	0	1	PATCH	4;5	6
260	135	0	1	PATCH	5;3	7
260	136	0	1	PATCH	2;1	8
260	137	0	1	PATCH	3;2	9
260	138	0	1	PATCH	5;3	10

260	139	0	1	PATCH	3;2	11
260	140	0	1	PATCH	4;5;3;2;1	12
260	141	0	1	PATCH	4;5;3;2;1	13
260	142	0	1	PATCH	4;5;3;2;1	14
260	143	0	1	PATCH	4;5;3;2;1	15
260	144	0	1	PATCH	4;5;3;2;1	16
260	145	0	1	PATCH	4;5;3;2;1	17
260	146	0	1	PATCH	4;5;3;2;1	18
260	147	0	1	PATCH	4;5;3;2;1	19
260	148	0	1	PATCH	4;5;3;2;1	20

■ N261 codebook

Band	Beam_ID	Module	Ant_Group	Ant_Type	Ant_Feed	Paired_With
261	0	0	0	PATCH	9	128
261	1	0	0	PATCH	10	129
261	2	0	0	PATCH	11	130
261	3	0	0	PATCH	12	131
261	4	0	0	PATCH	13	132
261	5	0	0	PATCH	10;11	133
261	6	0	0	PATCH	10;11	134
261	7	0	0	PATCH	11;12	135
261	8	0	0	PATCH	12;13	136
261	9	0	0	PATCH	10;11	137
261	10	0	0	PATCH	9;10	138
261	11	0	0	PATCH	10;11	139
261	12	0	0	PATCH	9;10;11;12;13	140
261	13	0	0	PATCH	9;10;11;12;13	141
261	14	0	0	PATCH	9;10;11;12;13	142
261	15	0	0	PATCH	9;10;11;12;13	143
261	16	0	0	PATCH	9;10;11;12;13	144
261	17	0	0	PATCH	9;10;11;12;13	145
261	18	0	0	PATCH	9;10;11;12;13	146
261	19	0	0	PATCH	9;10;11;12;13	147
261	20	0	0	PATCH	9;10;11;12;13	148
261	128	0	1	PATCH	1	0
261	129	0	1	PATCH	2	1
261	130	0	1	PATCH	3	2
261	131	0	1	PATCH	4	3
261	132	0	1	PATCH	5	4
261	133	0	1	PATCH	1;2	5
261	134	0	1	PATCH	3;4	6
261	135	0	1	PATCH	4;5	7
261	136	0	1	PATCH	4;5	8
261	137	0	1	PATCH	2;3	9

261	138	0	1	PATCH	2;3	10
261	139	0	1	PATCH	1;2	11
261	140	0	1	PATCH	1;2;3;4;5	12
261	141	0	1	PATCH	1;2;3;4;5	13
261	142	0	1	PATCH	1;2;3;4;5	14
261	143	0	1	PATCH	1;2;3;4;5	15
261	144	0	1	PATCH	1;2;3;4;5	16
261	145	0	1	PATCH	1;2;3;4;5	17
261	146	0	1	PATCH	1;2;3;4;5	18
261	147	0	1	PATCH	1;2;3;4;5	19
261	148	0	1	PATCH	1;2;3;4;5	20

Table 3.2-1: EUT codebook

3.3. Simulation verification

The beams selected for simulation verification are highlighted in yellow in Table 2-1. Input power level used for comparison is listed in Table 3.3-1

Mode/Band	Antenna	Input Power (dBm)SISO	Input Power (dBm)MIMO		
5G NR n260(39 GHz)	QTM#O Patch	6	6		
5G NR n261(28 GHz)	QTM#O Patch	6	6		

Table 3.3-1: Input power used in simulation validation

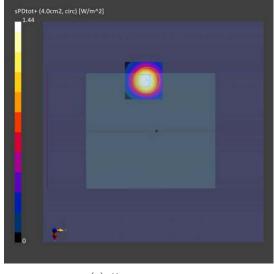
The simulation and measurement were performed at 2mm evaluation distance. The simulated and measured 4cm2 averaged PD results are shown in Table 3.3-2.

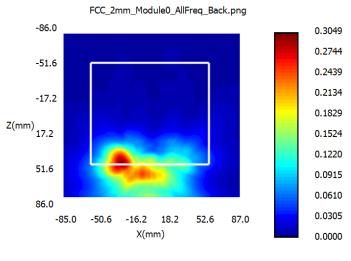
				6dBı	m input measu	rement / simu	lation		
Band	Ant Type	Module	Ant Group (Ant Polarization	beam ID	Surface	Channel	Measured	Simulated(Middle)	Delta (Simulated- Measured)
					Bottomface	Mid	10.8	18.13	2.25
					Frontface	Mid	5.25	9.49	2.57
			AG0(V)	14	Backface	Mid	1.28	2.2	2.35
			AG0(V)	14	Top	Mid	0.017	0.03	2.47
					Right	Mid	0.011	0.02	2.59
n261	Patch	QTM0			Left	Mid	0.023	0.04	2.40
11201	Paten	Q11VIO			Bottomface	Mid	10.4	18.42	2.48
					Frontface	Mid	4.05	9.51	3.71
			ACIAN	142	Backface	Mid	1.3	2.26	2.40
			AG1(H)	142	Top	Mid	0.021	0.04	2.80
					Right	Mid	0.024	0.05	3.19
					Left	Mid	0.01	0.02	3.01
					Bottomface	Mid	8.06	14.26	2.48
					Frontface	Mid	3.45	9.32	4.32
			4 CO CD	19	Backface	Mid	1.44	1.34	-0.31
			AG0(V)	19	Top	Mid	0.013	0.02	1.87
					Right	Mid	0.031	0.04	1.10
260	D. 1	0771 60			Left	Mid	0.05	0.11	3.42
n260	Patch	QTM0			Bottomface	Mid	9.33	13.66	1.66
					Frontface	Mid	5.32	7.82	1.67
			ACIED	147	Backface	Mid	0.978	1.82	2.70
			AG1(H)	147	Top	Mid	0.018	0.03	2.22
					Right	Mid	0.031	0.06	2.87
					Left	Mid	0.05	0.09	2.55

Table 3.3-2: Simulated and measured 4cm2 averaged PD comparison

Below Figures show Measured and simulated PD distributions for selected beams. As can be seen, the Simulated point PD distribution and Measured point PD distribution have good correlation on all surfaces evaluated.

• N260 QTMO: mid channel, Beam19, Back face, Point PD

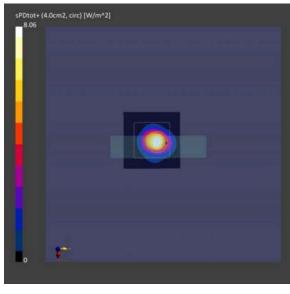




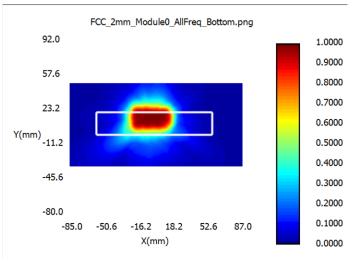
(a) Measurement

(b) Simulation

• N260 QTMO: mid channel, Beam19, Bottom face, Point PD

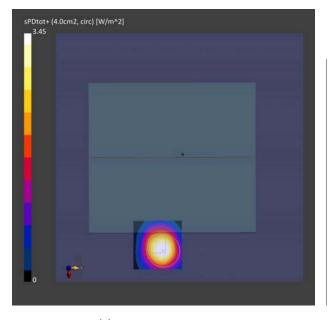


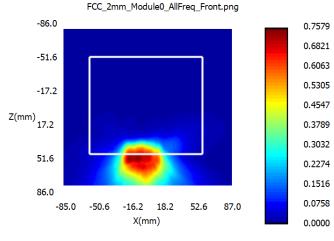




(b) Simulation

• N260 QTMO: Middle channel, Beam19, Front face, Point PD

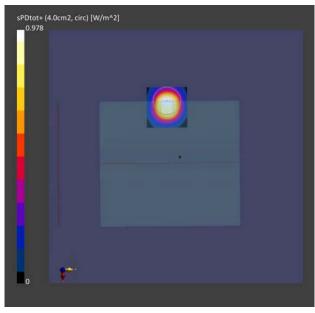




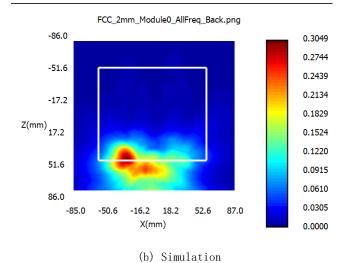
(a) Measurement

(b) Simulation

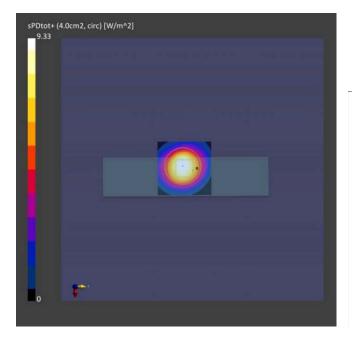
• N260 QTMO: mid channel, Beam147, Back face, Point PD

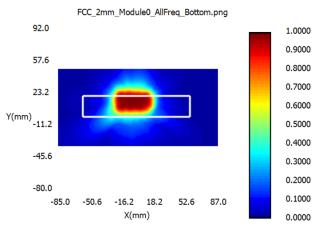






• N260 QTMO: mid channel, Beam147, Bottom face, Point PD

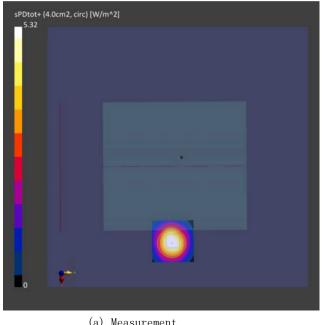




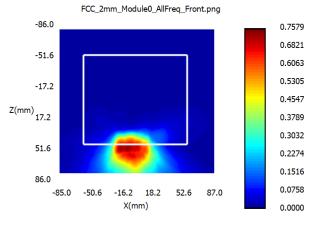
(a) Measurement

(b) Simulation



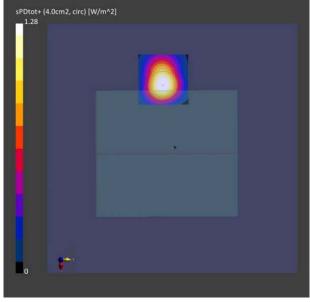


(a) Measurement

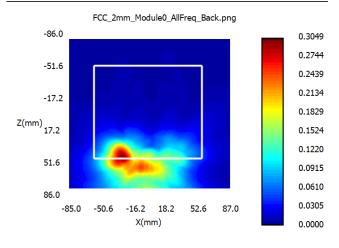


(b) Simulation

• N261 QTMO: mid channel, Beam14, Back face, Point PD

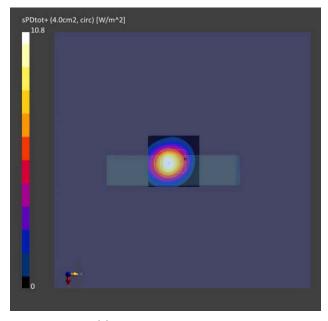




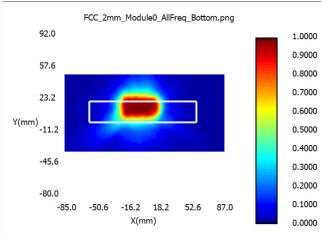


(b) Simulation

• N261 QTMO: mid channel, Beam14, Bottom face, Point PD

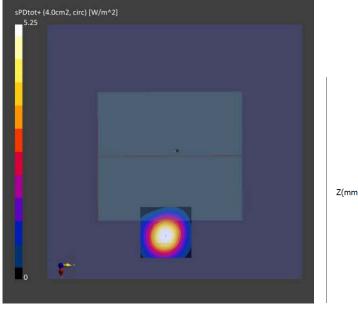


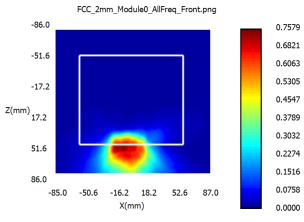
(a) Measurement



(b) Simulation

• N261 QTMO: Middle channel, Beam14, Front face, Point PD

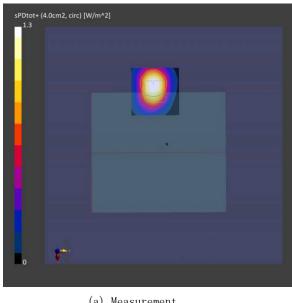




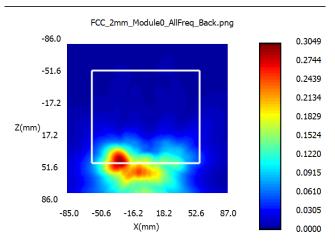
(a) Measurement

(b) Simulation

• N261 QTMO: mid channel, Beam142, Back face, Point PD

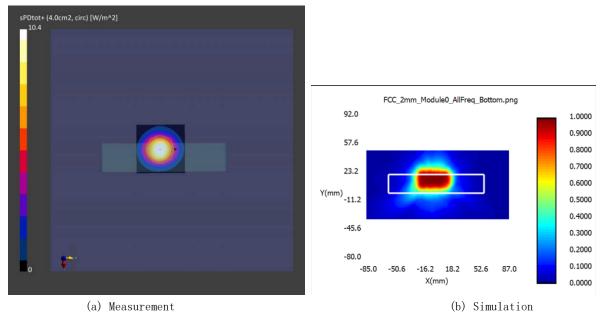


(a) Measurement

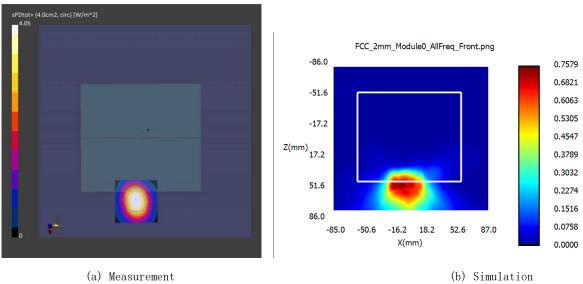


(b) Simulation

• N261 QTMO: mid channel, Beam142, Bottom face, Point PD



• N261 QTMO: Middle channel, Beam142, Front face, Point PD



3.4. Simulation Result

The model is validated in Section 3, the PD exposure of EUT can be reliably assessed using the validated simulation approach. The PD simulation was performed at n261 and n260. The simulated PD results are reported in this section. The Ratio of PD exposure from front surface to the worst surface at 2mm, and the ratio of PD exposure from 2mm to 10mm evaluation distance for each beam are also reported for simultaneous transmission analysis in Part 1. The relative phase between beam pairs is not controlled in the chipset design. Therefore, the relative phase between each beam pair was considered mathematically to identify the worst-case conditions, the below PD result for each MIMO beam represents the highest PD value after sweeping the relative phase between two SISO beams with a '5 degree' step interval from 0 degree to 360 degree.

PD for Low/Mid/High Channel at n260 and n261

Below Tables show the PD simulation evaluation of QTMO at N260 and N261 for those surface which need to take it into consideration as shown in Figure 3.1-2.

• QTMO N260 Low channel SISO

						((Max Ratio			(- (·				Max	Ratio	
F						2 PD(\/) ation su			0.64	0.11	0.07	4cm2 evaluat	PD(W/m2			0.33	0.09	0.70	0.05
Frequency (GHz)	Module	Antenna tvpe	Beam 2	Beam 1	evalua	ation su	riaces	noorn		Ratio		evaluat	on su	riaces	мостеш		Ra	tio	
(GIL)		type			Front	Back	Bottom	Left	Front/worse surface	Back/worse surface	Left/worse surface	Front	Back	Bottom	Left	Front/worse surface	Back/worse surface	Bottom/wor se surface	Left/worse surface
37	0	Path		0		0.12	2.9	0.03	0.50	0.04	0.01	0.54	0.08	1.44	0.02	0.19	0.03	0.50	0.01
37	0	Path		1	1.32	0.18	2, 85	0.03	0.46	0.06	0.01	0.51	0.11		0.02	0.18	0.04	0.48	0.01
37	0	Path		2		0.19	3, 47	0.05	0.45	0.05	0.01	0.55	0.1	1.63	0.04	0.16	0.03	0.47	0.01
37	0	Path		3		0.18	3, 19	0.08	0.46	0.06	0.03	0.54	0.11	1.53	0.06	0.17	0.03	0.48	0.02
37	0	Path		4	1.66	0.24	3, 46	0.06	0.48	0.07	0.02	0.63	0.16		0.04	0.18	0.05	0.50	0.01
37	0	Path		5		0.4	6.34	0.17	0.32	0.06	0.03	0.71	0.25		0.13	0.11	0.04	0.32	0.02
37 37	0	Path Path		7		0. 47 0. 52	6, 1	0.08	0.56	0.08	0.01	1.55	0.3		0.06	0.25	0.05	0.61 0.64	0.01
37	0	Path		8		0.32	6. 91	0.04	0.40	0.08	0.01	1.16	0.24		0.03	0.26	0.03	0.45	0.00
37	0	Path		9		0.38	6. 24	0.23	0.40	0.03	0.03	1.10	0.24		0.10	0.17	0.05	0.45	0.03
37	0	Path		10		0.51	6, 26	0.11	0.63	0.08	0.02	1.8	0.29		0.09	0.29	0.05	0.70	0.02
37	ŏ	Path		11	3, 14	0. 4	6, 55	0.22	0.48	0.06	0.02	1.27	0.24		0.18	0.19	0.04	0.51	0.03
37	Ů,	Path		12		0.79	10.5	0.78	0.42	0.08	0.07	1.84	0.58		0.57	0.18	0.06	0.38	0.05
37	0	Path		13		1.3	12, 44	0.05	0.55	0.10	0.00	3.42	1.01	7, 48	0.03	0, 27	0.08	0.60	0.00
37	0	Path		14	8, 86	1.56	14.03	0.07	0.63	0.11	0.00	4. 46	0.9	9.8	0.05	0.32	0.06	0.70	0.00
37	0	Path		15	8. 51	1.46	13.64	0.26	0.62	0.11	0.02	4.04	0.85	8.96	0.2	0.30	0.06	0.66	0.01
37	0	Path		16	6	0.88	11.46	0.48	0.52	0.08	0.04	2.37	0.55	6.58	0.37	0.21	0.05	0.57	0.03
37	0	Path		17	5.09	0.99	10.71	0.35	0.48	0.09	0.03	2.38	0.65	5.66	0.21	0.22	0.06	0.53	0.02
37	0	Path		18		1.44	13.2	0.04	0.62	0.11	0.00	4.14	0.85	9	0.03	0.31	0.06	0.68	0.00
37	0	Path		19	9.1	1.44	14. 21	0.15	0.64	0.10	0.01	4.57	0.87		0.11	0.32	0.06	0.68	0.01
37	0	Path		20		1.34	12, 71	0.37	0.58	0.11	0.03	3.3	0.71	7.97	0.3	0.26	0.06	0.63	0.02
37	0	Path		128		0.11	2. 9	0.02	0.47	0.04	0.01	0.51	0.06		0.02	0.18	0.02	0.49	0.01
37	0	Path		129		0.19	3.19	0.03	0.39	0.06	0.01	0.41	0.1	1.42	0.02	0.13	0.03	0.45	0.01
37 37	0	Path Path		130 131	1.53	0.28	3, 5	0.04	0.44	0.08	0.01	0.62	0.18		0.03	0.18	0.05	0.45	0.01
37	0	Path		131		0.28	3, 15	0.07	0.43	0.09	0.02	0.53	0.15		0.04	0.17	0.05	0.45 0.50	0.02
37	0	Path		133		0.37	6, 28	0.03	0.34	0.11	0.01	0. 74	0. 3	2.4	0.04	0.12	0.03	0.38	0.01
37	0	Path		134	3, 19	0.38	5, 82	0.03	0.55	0.00	0.02	1.4	0.23		0.02	0.12	0.03	0.60	0.00
37	0	Path		135		0.61	6. 49	0.05	0.53	0.09	0.01	1.46	0.37		0.04	0.22	0.04	0.63	0.00
37	ŏ	Path		136	2	0.59	6, 51	0, 21	0.31	0.09	0.03	0.72	0.4		0.16	0.11	0.06	0.35	0.02
37	0	Path		137	2.6	0.67	6, 25	0.17	0.42	0.11	0.03	1.14	0.45		0.13	0.18	0.07	0.37	0.02
37	Ŏ	Path		138	3, 55	0.58	6.34	0.04	0.56	0.09	0.01	1.56	0.36		0.03	0. 25	0.06	0.62	0.00
37	0	Path		139	2.4	0.58	6. 35	0.19	0.38	0.09	0.03	1.02	0.4	3.09	0.15	0.16	0.06	0.49	0.02
37	0	Path		140	4. 91	1.08	10.7	0.57	0.46	0.10	0.05	2.04	0.5	5. 52	0.43	0.19	0.05	0.52	0.04
37	0	Path		141	7.47	1.43	12, 65	0.26	0.59	0.11	0.02	3.75	1.06	7. 55	0.15	0.30	0.08	0.60	0.01
37	0	Path		142	8.96	1.54	14.11	0.04	0.64	0.11	0.00	4.66	0.99	9.46	0.03	0.33	0.07	0.67	0.00
37	0	Path		143	7.02	1.66	13, 45	0.25	0.52	0.12	0.02	3.45	1.21	8. 51	0.19	0.26	0.09	0.63	0.01
37	0	Path		144	5.07	1.02	11.21	0.46	0.45	0.09	0.04	2.03	0.55		0.37	0.18	0.05	0.54	0.03
37	0	Path		145	4.95	1.1	10.9	0.65	0.45	0.10	0.06	2. 21	0.76		0.45	0.20	0.07	0.47	0.04
37	0	Path		146	8.5	1.49	13, 65	0.02	0.62	0.11	0.00	4.4	1.08		0.02	0.32	0.08	0.63	0.00
37	0	Path		147	8. 81	1.93	14.86	0.11	0.59	0.13	0.01	4.58	1.17		0.09	0.31	0.08	0.68	0.01
37	0	Path		148	5.56	1.31	12	0.26	0.46	0.11	0.02	2.48	0.88	7. 27	0.2	0.21	0.07	0.61	0.02

• QTMO N260 Low channel MIMO

										Max Ratio							Max	Ratio	
_							m2) at 2		0.64	0.14	0.07			.2) at 1		0.32	0, 09	0, 71	0.05
Frequency (GHz)	Module	Antenna type	Beam 2	Beam 1	evalu	ation su	urfaces (16dEn		Ratio		evaluat	tion su	riaces	@6dBm		Ra	tio	
(0112)		type			Front	Back	Bottom	Left	Front/worse	Back/worse	Left/worse	Front	Back	Bottom	I of+	Front/worse	Back/worse	Bottom/wor	Left/worse
					PIOII	Dack	Боссон	reit	surface	surface	surface	PIONE	Dack	Bottom	reit	surface	surface	se surface	surface
37	0	Path	128	0	2.97	0.29	5, 95	0.08	0.50	0.05	0.01	1.15	0.14	3.09	0.06	0.19	0.02	0.52	0.01
37	0	Path	129	1	2.74	0.44	6. 42	0.1	0.43	0.07	0.02	1.04	0.27	3.06	0.07	0.16	0.04	0.48	0.01
37	0	Path	130	2	3.33	0.62	7.67	0.18	0.43	0.08	0.02	1.33	0.36	3.68	0.15	0.17	0.05	0.48	0.02
37	0	Path	131	3	2.95	0.6	6. 81	0.28	0.43	0.09	0.04	1.16	0.38	3.51	0.22	0.17	0.06	0.52	0.03
37	0	Path	132	4	3.63	0.78	7.12	0.21	0.51	0.11	0.03	1.38	0.62	3.92	0.15	0.19	0.09	0.55	0.02
37	0	Path	133	5	4.85	1.17	12, 93	0.37	0.38	0.09	0.03	1.84	0.65	5.27	0.27	0.14	0.05	0.41	0.02
37	0	Path	134	6	6.31	0.9	11.47	0.13	0.55	0.08	0.01	2.91	0.54	6.86	0.09	0.25	0.05	0.60	0.01
37	0	Path	135	7	7.64	1.46	14.13	0.16	0.54	0.10	0.01	3.26	0.9	9.42	0.13	0.23	0.06	0.67	0.01
37	0	Path	136	8	6.33	1.33	15.04	0.8	0.42	0.09	0.05	2.48	0.86	7.84	0.62	0.16	0.06	0.52	0.04
37	0	Path	137	9	5. 71	1.54	12, 89	0.54	0.44	0.12	0.04	2.53	1.03	5.53	0.4	0.20	0.08	0.43	0.03
37	0	Path	138	10	8.1	1.23	13, 61	0.25	0.60	0.09	0.02	3.47	0.74	9.12	0.2	0.25	0.05	0.67	0.01
37	0	Path	139	11	7.08	1.41	15, 56	0.77	0.46	0.09	0.05	2.8	0.95	8.87	0.61	0.18	0.06	0.57	0.04
37	0	Path	140	12	10.37	2.94	25, 76	1.85	0.40	0.11	0.07	4. 42	1.52	11.82	1.4	0.17	0.06	0.46	0.05
37	0	Path	141	13	15.32	3.05	28, 36	0.41	0.54	0.11	0.01	7.6	2.08	16.75	0.25	0.27	0.07	0.59	0.01
37	0	Path	142	14	18.59	4.08	29. 2	0.17	0.64	0.14	0.01	9.4	2.26	20.71	0.13	0.32	0.08	0.71	0.00
37	0	Path	143	15	17.71	4.11	32, 65	0.99	0.54	0.13	0.03	8.46	2.58	21.61	0.78	0.26	0.08	0.66	0.02
37	0	Path	144	16	13.27	2. 44	28, 49	1.57	0.47	0.09	0.06	5.19	1.43	15.92	1.18	0.18	0.05	0.56	0.04
37	0	Path	145	17	11.66	2. 71	24. 4	1.18	0.48	0.11	0.05	5. 29	1.61	11.94	0.79	0.22	0.07	0.49	0.03
37	0	Path	146	18	18.7	3.37	28. 48	0.1	0.66	0.12	0.00	9.6	2	18.66	0.08	0.34	0.07	0.66	0.00
37	0	Path	147	19	19.52	4.55	32, 58	0.48	0.60	0.14	0.01	10.04	2, 56	22. 73	0.38	0.31	0.08	0.70	0.01
37	0	Path	148	20	15.56	3.52	31.44	1.15	0.49	0.11	0.04	6.89	2.16	19.95	0.89	0.22	0.07	0.63	0.03

• QTMO N260 Middle channel SISO

										Max Ratio							Max	Ratio	
_							m2) at 2		0, 66	0.12	0, 05			 at 1 		0.34	0, 09	0, 71	0.04
Frequency (GHz)	Module	Antenna	Beam 2	Beam 1	evalu	ation su	ırfaces (@6dBm		Ratio		evaluat	ion su	rfaces	@6dBm		Ra	tio	
(GHZ)		type			- ·	- 1	5	. c.	Front/worse	Back/worse	Left/worse		n 1		* C.	Front/worse	Back/worse	Bottom/wor	Left/worse
					Front	Back	Bottom	Left	surface	surface	surface	Front	Back	Bottom	Left	surface	surface	se surface	surface
38.5	0	Path		0	1.58	0.1	2, 95	0.03	0.54	0.03	0.01	0.63	0.06	1.41	0.02	0.21	0.02	0.48	0.01
38.5	0	Path		1	1.44	0.18	2, 82	0.02	0.51	0.06	0.01	0.56	0.12	1.34	0.02	0.20	0.04	0.48	0.01
38.5	0	Path		2		0.2		0.06	0.45	0.06	0.02	0.48	0.11		0.05		0.03	0.49	0.02
38.5	0	Path		3		0.19		0.07	0.46	0.06	0.02	0.51	0.13		0.05		0.04	0.49	0.02
38.5	0	Path		4	1.62	0.21	3, 33	0.06	0.49	0.06	0.02	0.57	0.15		0.04		0.05	0.52	0.01
38.5	0	Path		5	2.28	0.49	6, 25	0.15	0.36	0.08	0.02	0.72	0.33		0.11	0.12	0.05	0.32	0.02
38.5	0	Path		6	2.9	0.53	5, 72	0.07	0.51	0.09	0.01	1.22	0.33		0.05		0.06	0.63	0.01
38.5	0	Path		7		0.44	5, 89	0.05	0.61	0.07	0.01	1.57	0.24		0.04		0.04	0.63	0.01
38.5	0	Path		8		0.37	6.9	0.22	0.43	0.05	0.03	1.22	0.22		0.16		0.03	0.46	0.02
38.5	0	Path		9		0.53	5, 98	0.15	0.35	0.09	0.03	0.77	0.37	2.38	0.1	0.13	0.06	0.40	0.02
38.5	0	Path		10		0.57	5, 98	0.13	0.61	0.10	0.02	1.56	0.33	4.23	0.1	0.26	0.06	0.71	0.02
38.5	0	Path		11	3.41	0.4	6, 59	0.2	0.52	0.06	0.03	1.39	0.2		0.16		0.03	0.53	0.02
38.5	0	Path		12		1.01	11.14	0.56	0.39	0.09	0.05	1.66	0.68		0.4	0.15	0.06	0.39	0.04
38.5	0	Path		13		1.18		0.06	0.50	0.11	0.01	2.65	0.84		0.04		0.08	0.60	0.00
38.5	0	Path		14		1.48		0.08	0.65	0.11	0.01	4.1	0.83		0.06		0.06	0.70	0.00
38.5	0	Path		15		1.15		0.28	0.66	0.09	0.02	4.06	0.59		0.23		0.05	0.66	0.02
38.5	0	Path		16		0.8		0.56	0.56	0.07	0.05	2.78	0.54		0.45		0.05	0.57	0.04
38.5	0	Path		17		1.12		0.27	0.41	0.11	0.03	1.85	0.71	5. 26	0.16		0.07	0.52	0.02
38.5 38.5	0	Path Path		18 19		1.45		0.06	0.63	0.12	0.00	3. 64 4. 44	0.76		0.05		0.00	0.69	0.00
38.5	0	Path		20		1.09		0.11	0.64	0.09	0.01	3, 61	0.76		0.09		0.05	0.62	0.01
38.5	0	Path		128		0.14	2, 81	0.02	0.42	0.09	0.03	0.41	0.03		0.02		0.03	0.02	0.03
38.5	0	Path		129		0.14	3, 13	0.02	0.42	0.00	0.01	0. 41	0.07	1. 41	0.02		0.02	0.45	0.01
38.5	0	Path		130		0.28	3, 51	0.05	0.46	0.08	0.01	0.68	0.11		0.02		0.04	0.45	0.01
38.5	0	Path		131	1.4	0. 25	3, 11	0.03	0.45	0.08	0.02	0.55	0.16		0.05		0.05	0.43	0.02
38.5	0	Path		132		0.38	3, 33	0.04	0.49	0.11	0.02	0.65	0.3		0.02		0.09	0.51	0.02
38.5	0	Path		133		0.34	6.4	0.09	0.32	0.05	0.01	0.71	0.21	2. 43	0.02		0.03	0.38	0.01
38.5	Ů.	Path		134		0.43	5, 61	0.02	0.52	0.08	0.00	1.29	0.24		0.02		0.04	0.60	0.00
38.5	0	Path		135	3, 25	0.55	6, 29	0.05	0.52	0.09	0.00	1.38	0.32		0.02		0.05	0.62	0.00
38.5	Ů.	Path		136	2, 03	0.63	6, 6	0.19	0.31	0.10	0.03	0.75	0, 46		0.14		0.07	0.35	0.02
38.5	0	Path		137	2.83	0.56	6, 41	0.17	0.44	0.09	0.03	1.3	0.34		0.12		0.05	0.35	0.02
38.5	0	Path		138		0.57		0.05	0.54	0.10	0.01	1.42	0.38		0.03		0.06	0.60	0.01
38. 5	0	Path		139	2.3	0.67		0.17	0.35	0.10	0.03	0.94	0.47		0.13		0.07	0.48	0.02
38. 5	0	Path		140	4. 45	1.12		0.57	0.38	0.10	0.05	1.73	0.67		0.44		0.06	0.53	0.04
38.5	0	Path		141	7.54	0.94		0. 21	0.66	0.08	0.02	3.88	0.67		0.12		0.06	0.59	0.01
38.5	0	Path		142		1.46		0.04	0.61	0.11	0.00	4. 24	1.01	8.69	0.03		0.07	0.64	0.00
38.5	0	Path		143	6.56	1.6	12, 74	0.23	0.51	0.13	0.02	3.24	1.15		0.18		0.09	0.64	0.01
38.5	0	Path		144	4.61	1.11	11.55	0.54	0.40	0.10	0.05	1.7	0.73	6.53	0.43	0.15	0.06	0.57	0.04
38.5	0	Path		145	4. 98	1.23	11.03	0.53	0.45	0.11	0.05	2. 33	0.74	4. 92	0.35	0.21	0.07	0.45	0.03
38.5	0	Path		146	8.8	1.04		0.04	0.68	0.08	0.00	4.57	0.83	7. 99	0.03	0.35	0.06	0.62	0.00
38.5	0	Path		147	7.82	1.82		0.09	0.57	0.13	0.01	4	1.22	9.18	0.07	0.29	0.09	0.67	0.01
38.5	0	Path		148	5.15	1.3	11.6	0.32	0.44	0.11	0.03	2. 26	0.93	7.02	0.24	0.19	0.08	0.61	0.02

• QTMO N260 Middle channel MIMO

										Max Ratio							Max	Ratio	
							n2) at 2		0, 67	0.13	0, 06			 at 1 		0.32	0, 09	0, 70	0, 04
Frequency (GHz)	Module	Antenna tvoe	Beam 2	Beam 1	evalu	ation su	urfaces (96dBm		Ratio		evaluat	tion su	rfaces	@6dBm		Ra	tio	
(0112)		type			Front	Back	Bottom	Left	Front/worse	Back/worse	Left/worse	Front	Back	Bottom	Lof+	Front/worse	Back/worse	Bottom/wor	Left/worse
					PIOII	Dack	Воссон	reit	surface	surface	surface	PIONE	Dack	DO C COM	reit	surface	surface	se surface	surface
38.5	0	Path	128	0		0.31	6.07	0.08	0.48	0.05	0.01	1.18	0.18		0.06	0.19	0.03	0.50	0.01
38.5	0	Path	129	1	2.87	0.43		0.09	0.45	0.07	0.01	1.1	0.27		0.07	0.17	0.04	0.50	0.01
38.5	0	Path	130	2		0.68	7. 21	0.19	0.50	0.09	0.03	1.36	0.39	3.76	0.16	0.19	0.05	0.52	0.02
38.5	0	Path	131	3	3.07	0.65	6, 56	0.24	0.47	0.10	0.04	1.16	0.45	3.48	0.19	0.18	0.07	0.53	0.03
38.5	0	Path	132	4	3.82	0.79	6.86	0.18	0.56	0.12	0.03	1.5	0.62	3.85	0.12	0.22	0.09	0.56	0.02
38.5	0	Path	133	5	5.46	1.15	13, 64	0.34	0.40	0.08	0.02	2	0.75	5. 29	0.25	0.15	0.05	0.39	0.02
38.5	0	Path	134	6	5.98	0.92	10.69	0.1	0.56	0.09	0.01	2.75	0.53	6.77	0.07	0.26	0.05	0.63	0.01
38.5	0	Path	135	7	7.73	1.23	13, 45	0.17	0.57	0.09	0.01	3.37	0.72	9. 22	0.14	0.25	0.05	0.69	0.01
38. 5	0	Path	136	8	6.72	1.53	15, 15	0.74	0.44	0.10	0.05	2. 78	0.92	8. 29	0.55	0.18	0.06	0.55	0.04
38.5	0	Path	137	9	6.44	1.44	13.36	0.56	0.48	0.11	0.04	2.62	0.96	6.35	0.4	0.20	0.07	0.48	0.03
38.5	0	Path	138	10	7.83	1.24	13, 57	0.28	0.58	0.09	0.02	3.28	0.77	9.33	0.22	0.24	0.06	0.69	0.02
38.5	0	Path	139	11	7.69	1.5	15, 61	0.68	0.49	0.10	0.04	3.19	1.04	9.59	0.53	0.20	0.07	0.61	0.03
38.5	0	Path	140	12	10.77	3. 21	27.09	1.53	0.40	0.12	0.06	4. 44	2.07	13.7	1.13	0.16	0.08	0.51	0.04
38.5	0	Path	141	13	16.97	2.7	27, 22	0.46	0.62	0.10	0.02	8.11	1.95	16.88	0.29	0.30	0.07	0.62	0.01
38.5	0	Path	142	14	19.32	3.67	28. 99	0.15	0.67	0.13	0.01	9.32	1.99	19.89	0.12	0.32	0.07	0.69	0.00
38.5	0	Path	143	15	18.64	4.12	31.4	0.98	0.59	0.13	0.03	9.26	2. 21	22.01	0.77	0.29	0.07	0.70	0.02
38. 5	0	Path	144	16	14	2.89	29.34	1.56	0.48	0.10	0.05	5. 98	1.94	17.25	1.24	0.20	0.07	0.59	0.04
38.5	0	Path	145	17	13.17	3.3	24, 47	1.22	0.54	0.13	0.05	6.11	2.17	13.35	0.81	0.25	0.09	0.55	0.03
38. 5	0	Path	146	18	20.44	2.94	29. 7	0.13	0.69	0.10	0.00	10.04	1.77	19.57	0.1	0.34	0.06	0.66	0.00
38.5	0	Path	147	19	18.72	4. 31	30. 42	0.34	0.62	0.14	0.01	9.55	2. 31	21.64	0.27	0.31	0.08	0.71	0.01
38. 5	0	Path	148	20	16.7	3.45	30, 51	1.25	0.55	0.11	0.04	7.94	2.02	20.51	0.98	0.26	0.07	0.67	0.03

• QTMO N260 High channel SISO

							-> -			Max Ratio							Max	Ratio	
_							m2) at 2		0.69	0.15	0.05		PD(W/m			0.34	0.10	0.70	0.03
Frequency (GHz)	Module	Antenna	Beam 2	Beam 1	evalu	ation si	urfaces (96dBm		Ratio		evaluat	ion su	riaces	@6dBm		Ra	tio	
(GHZ)		type			Front	Back	Bottom	Left	Front/worse	Back/worse	Left/worse	Front	D1-	Bottom	Left	Front/worse	Back/worse	Bottom/wor	Left/worse
					Front	Баск	Bottom	Leit	surface	surface	surface	Front	васк	Bottom	Leit	surface	surface	se surface	surface
40	0	Path		0		0.13	2, 95	0.02	0.53	0.04	0.01	0.66	0.08		0.02		0.03	0.47	0.01
40	0	Path		1		0.21	2.8	0.02	0.45	0.08	0.01	0.47	0.13		0.02		0.05	0.46	0.01
40	0	Path		2		0.17		0.05	0.53	0.05	0.02	0.56	0.11	1.69	0.04		0.03	0.52	0.01
40	0	Path		3		0.18		0.06	0.53	0.06	0.02	0.48	0.11	1.45	0.05		0.04	0.49	0.02
40	0	Path		4	1.53	0.2		0.05	0.49	0.06	0.02	0.49	0.13	1.61	0.03		0.04	0.52	0.01
40	0	Path		5		0.38	6, 39	0.15	0.46	0.06	0.02	0.87	0.24	2.32	0.1	0.14	0.04	0.36	0.02
40	0	Path		6		0.51	5. 47	0.07	0.58	0.09	0.01	1.37	0.32		0.04		0.06	0.63	0.01
40	0	Path		7		0.43	5, 55	0.05	0.59	0.08	0.01	1.43	0.23		0.04		0.04	0.62	0.01
40	0	Path		8		0.34	6, 51	0.2	0.49	0.05	0.03	1.22	0.24	3.09	0.14		0.04	0.47	0.02
40	0	Path		10		0.42	5. 85 5. 44	0.13	0.42	0.07	0.02	0.88	0.29	2.46	0.09		0.05	0.42	0.02
40	0	Path Path		11	3.6	0.47		0.15	0.68 0.56	0.09	0.02	1.58	0.3	3.8	0.13	0.29	0.00	0.70 0.54	0.02
40	0	Path		12		0.88		0.16	0.56	0.05	0.02	1.84	0.63		0.13		0.03	0.54	0.02
40	0	Path		13		1.16		0.05	0.55	0.00	0.00	2.61	0.72		0.03		0.00	0. 42	0.00
40	0	Path		14		1.3		0.03	0.69	0.11	0.00	3.97	0. 72	7.86	0.08		0.07	0.67	0.00
40	Ů.	Path		15		1.04	12, 16	0.29	0.65	0.09	0.02	3, 84	0.61	7.66	0.23		0.05	0.63	0.02
40	0	Path		16		0.89	11, 31	0.46	0.57	0.08	0.04	3.02	0.53	6, 74	0.35		0.05	0.60	0.03
40	0	Path		17		0.96	10, 32	0.2	0.50	0.09	0.02	2, 21	0.7	5.86	0.11	0, 21	0.07	0.57	0,01
40	0	Path		18		1.31	10.99	0.08	0.67	0.12	0.01	3.68	0.8		0.06		0.07	0.67	0.01
40	0	Path		19	8.52	1.3	12, 65	0.13	0.67	0.10	0.01	4	0.82	8. 47	0.1	0.32	0.06	0.67	0.01
40	0	Path		20	7.35	1.06	11.84	0.31	0.62	0.09	0.03	3.63	0.66	7.36	0.24	0.31	0.06	0.62	0.02
40	0	Path		128	1.06	0.15	2, 63	0.02	0.40	0.06	0.01	0.31	0.09	1.31	0.02	0.12	0.03	0.50	0.01
40	0	Path		129		0.17		0.03	0.39	0.06	0.01	0.4	0.1	1.48	0.02	0.13	0.03	0.49	0.01
40	0	Path		130	1.27	0.39	3, 38	0.04	0.38	0.12	0.01	0.48	0.27		0.03		0.08	0.45	0.01
40	0	Path		131	1.12	0.34	3.1	0.07	0.36	0.11	0.02	0.44	0.2		0.05		0.06	0.41	0.02
40	0	Path		132		0.4	3, 17	0.03	0.47	0.13	0.01	0.64	0.31	1.63	0.02		0.10	0.51	0.01
40	0	Path		133		0.44	6.17	0.09	0.34	0.07	0.01	0.83	0.3		0.07		0.05	0.41	0.01
40	0	Path		134		0.47	5, 18	0.02	0.50	0.09	0.00	1.1	0.29	3.08	0.02		0.06	0.59	0.00
40	0	Path		135		0.58	5. 97	0.05	0.52	0.10	0.01	1.3			0.04		0.05	0.62	0.01
40	0	Path		136		0.69	6.46	0.17	0.29	0.11	0.03	0.73	0.47	2.29	0.12		0.07	0.35	0.02
40	0	Path		137		0.8	6. 41	0.16	0.37	0.12	0.02	1.09	0.54		0.12		0.08	0.33	0.02
40	0	Path		138 139		0.66	5. 7 6. 4	0.04	0.48	0.12	0.01	1.18	0.41	3.43	0.03		0.07	0.60	0.01
40	0	Path			2.16 4.48	1.08	11.6	0.17	0.34	0.12	0.03	1.74	0.5	6.32		0.14		0.49	
40	0	Path Path		140	6, 29	1.08		0.09	0.39	0.09	0.05	3.34	1.07	6. 45	0.4		0.06	0.54	0.03
40	0	Path		141	6, 45	1.82		0.09	0.53	0.15	0.01	3.34	1.18		0.06		0.10	0.50	0.01
40	0	Path		143		1.66		0.06	0.50	0.15	0.00	2. 95	1.18	7.83	0.16		0.10	0.64	0.00
40	0	Path		143		1.00	11, 41	0. 21	0.30	0.14	0.02	1.91	0.7		0.10	0.24	0.09	0.58	0.01
40	0	Path		145		1. 45		0. 44	0.44	0.13	0.03	2. 41	0.87	5.4	0.41		0.08	0.38	0.04
40	0	Path		146		1. 57		0. 44	0.44	0.13	0.04	3.65	1.14		0.25		0.10	0.40	0.00
40	0	Path		147	6.5	1.9		0.03	0.54	0.16	0.00	3, 34	1.21	7.87	0.09		0.10	0.66	0.00
40	0	Path		148		1.25		0.32	0.47	0.10	0.03	2.4	0.83		0.25		0.10	0.63	0.02

• QTMO N260 High channel MIMO

										Max Ratio							Max	Ratio	
_							n2) at 2		0, 66	0.14	0.05			.2) at 1		0.32	0.10	0.73	0.04
Frequency (GHz)	Module	Antenna type	Beam 2	Beam 1	evalu	ation su	rfaces (96dBm		Ratio		evaluat	tion su	rfaces	@6dBm		Ra	tio	
(GHZ)		type			Front	Back	Bottom	Left	Front/worse	Back/worse	Left/worse	Front	Back	Bottom	T _ C.	Front/worse	Back/worse	Bottom/wor	Left/worse
					Tront	Dack	ростош	reit	surface	surface	surface	Front	Dack	POLLOW	reit	surface	surface	se surface	surface
40	0	Path	128	0	2.8	0.34	5. 91	0.07	0.47	0.06	0.01	1.06	0.2	2.84	0.05	0.18	0.03	0.48	0.01
40	0	Path	129	1	3.13	0.39	6, 59	0.07	0.47	0.06	0.01	1.14	0.24	3.68	0.06	0.17	0.04	0.56	0.01
40	0	Path	130	2	3.29	0.8	7.17	0.17	0.46	0.11	0.02	1.21	0.48	4.09	0.14	0.17	0.07	0.57	0.02
40	0	Path	131	3	2.94	0.77	6.49	0.23	0.45	0.12	0.04	1.16	0.49	3.49	0.18	0.18	0.08	0.54	0.03
40	0	Path	132	4	3.47	0.85	6.46	0.13	0.54	0.13	0.02	1.39	0.65	3.66	0.09	0.22	0.10	0.57	0.01
40	0	Path	133	5	6.43	1	13.36	0.36	0.48	0.07	0.03	2.32	0.72	6	0.25	0.17	0.05	0.45	0.02
40	0	Path	134	6	6.18	1.12	9, 96	0.1	0.62	0.11	0.01	2.84	0.72	6.36	0.07	0.29	0.07	0.64	0.01
40	0	Path	135	7	8.16	1.29	13.42	0.17	0.61	0.10	0.01	3.46	0.68	9.78	0.14	0.26	0.05	0.73	0.01
40	0	Path	136	8	7.06	1.55	14, 52	0.63	0.49	0.11	0.04	3.01	0.98	8.34	0.45	0.21	0.07	0.57	0.03
40	0	Path	137	9	6.96	1.46	13.16	0.49	0.53	0.11	0.04	2. 91	1.01	6.36	0.34	0.22	0.08	0.48	0.03
40	0	Path	138	10	7.66	1.5	12.61	0.25	0.61	0.12	0.02	3.2	0.92	8.76	0.21	0.25	0.07	0.69	0.02
40	0	Path	139	11	8.48	1.52	15.44	0.57	0.55	0.10	0.04	3.65	1.06	10.04	0.44	0.24	0.07	0.65	0.03
40	0	Path	140	12	11.57	2.82	26, 15	1.32	0.44	0.11	0.05	4.92	2.07	14.81	0.92	0.19	0.08	0.57	0.04
40	0	Path	141	13	17.67	3.81	26, 77	0.27	0.66	0.14	0.01	8.57	2.54	16.83	0.16	0.32	0.09	0.63	0.01
40	0	Path	142	14	15.56	3.69	25. 47	0.2	0.61	0.14	0.01	7.61	2. 23	17.73	0.16	0.30	0.09	0.70	0.01
40	0	Path	143	15	20.18	4.3	31.6	0.93	0.64	0.14	0.03	10.17	2.43	22.8	0.74	0.32	0.08	0.72	0.02
40	0	Path	144	16	15.48	2.97	29, 26	1.33	0.53	0.10	0.05	7.11	2	18.99	1.02	0.24	0.07	0.65	0.03
40	0	Path	145	17	14.06	3.39	24.14	0.98	0.58	0.14	0.04	6.54	2.34	13.73	0.63	0.27	0.10	0.57	0.03
40	0	Path	146	18	18.31	3. 26	26, 96	0.21	0.68	0.12	0.01	9.08	2.16	18.03	0.17	0.34	0.08	0.67	0.01
40	0	Path	147	19	18	4.12	28.1	0.35	0.64	0.15	0.01	8.85	2. 25	20.34	0.28	0.31	0.08	0.72	0.01
40	0	Path	148	20	18.4	3.92	30, 98	1.04	0.59	0.13	0.03	9. 22	2.36	21.77	0.8	0.30	0.08	0.70	0.03

• QTMO N261 LOW channel SISO

					4	0 DD/#/-	n2) at 2			Max Ratio		40	DD /# /- :	2) at 1	0		Max	Ratio	
Frequency		Antenna					mz) at z erfaces (0.59	0.15	0.05	evaluat				0.30	0.10	0.62	0.04
(GHz)	Module	type	Beam 2	Beam 1						Ratio								tio	
		7.			Front	Back	Bottom	Left	Front/worse		Left/worse	Front	Back	Bottom	Left	Front/worse			Left/worse
									surface	surface	surface					surface	surface	se surface	surface
27.5	0	Path		0		0.25	3, 24	0.05	0.38	0.08	0.02	0.41	0.14		0.04	0.13	0.04	0.42	0.01
27.5	0	Path		1	1.1	0.29	3, 15	0.07	0.35	0.09	0.02	0.34	0.18		0.05	0.11	0.06	0.37	0.02
27.5	0	Path		2		0.21	3, 31	0.04		0.06	0.01	0.49	0.12		0.03	0.15	0.04	0.44	0.01
27.5	0	Path		3		0.17	2.84	0.05	0.54	0.06	0.02	0.54	0.11		0.04	0.19	0.04	0.43	0.01
27.5	0	Path		4		0.19	2. 61	0.05		0.07	0.02	0.5	0.11	1.3	0.03	0.19	0.04	0.50	0.01
27.5	0	Path		5		0.63	6. 37	0.16	0.43	0.10	0.03	1.02	0.38		0.11	0.16	0.06	0.43	0.02
27.5	0	Path		6		0.66	7. 01	0.05	0.52	0.09	0.01	1.45	0.38		0.04	0. 21	0.05	0.57	0.01
27. 5	0	Path				0.56	7.03	0.03	0.56	0.08	0.00	1.7	0.32		0.02	0.24	0.05	0.58	0.00
27.5		Path		8		0.34	4, 63 6, 82	0.1	0.56	0.07	0.02	1.06	0.21	1.83	0.08	0.23	0.05	0.40	0.02
27.5	0	Path		10		0.67	7.6	0.12	0.48	0.10	0.02	1.25	0.39		0.09	0.18	0.06	0.49	0.01
27.5		Path				0.84					0.01	1.31	0.46					0.54	
27.5	0	Path		11	2.65	0.58	6.04	0.11	0.44	0.10	0.02	1.05	0.35 1.13		0.09	0.17	0.06	0.48	0.01
27.5	0	Path		12 13		1.65 1.88		0.81	0.53 0.55	0.10	0.05	3.88	1.13		0.59	0.25	0.07	0.49	0.04
27. 5 27. 5	0	Path Path		14		2.06		0.06	0.53	0.12	0.00	4. 49	1. 41	10, 82	0.04	0. 27	0.08	0.60 0.61	0.00
27.5	0	Path Path		14		1.59	14, 73	0.04	0.53	0.12	0.00	4.71	1.41		0.03	0.27	0.08	0.60	0.00
27.5	0	Path		16		1.22		0.03	0.59	0.11	0.00	2.51	0.84		0.02	0.30	0.08	0.44	0.00
27.5	0	Path		17	8, 89	2.01	16, 44	0.45	0.54	0.09	0.02	4, 27	1.44		0.23	0.19	0.00	0.44	0.02
27.5	0	Path		18		1.97		0.40	0.54	0.12	0.00	4. 57		10.49	0.04	0.20	0.09	0.04	0.02
27.5	0	Path		19		1.85	16, 87	0.00	0.54	0.11	0.00	4, 57		10.15	0.02	0.27	0.08	0.60	0.00
27.5	o l	Path		20		1. 47		0.02	0.59	0.11	0.00	3, 77	1.05		0.06	0.28	0.08	0.55	0.00
27.5	ŏ	Path		128		0.15	3, 5	0.04	0.50	0.04	0.01	0, 67	0.09		0.03	0.19	0.03	0.43	0.00
27.5	0	Path		129		0.15	2, 99	0.03	0.46	0.05	0.01	0.49	0.1	1.27	0.03	0.16	0.03	0.42	0.01
27.5	ŏ	Path		130		0.34		0.05	0.32	0.10	0.01	0.33	0.1		0.04	0.10	0.00	0.40	0.01
27.5	ů i	Path		131	1.17	0.37	3. 2	0.05	0.37	0.10	0.02	0.37	0.24		0.04	0.12	0.08	0.41	0.01
27.5	ŏ	Path		132	1.15	0.33	2, 89	0.06	0.40	0.11	0.02	0.42	0.22		0.04	0.15	0.08	0.43	0.01
27.5	ů	Path		133	3	0.4	5, 66	0.14	0.53	0.07	0.02	1, 31	0.19		0.1	0.23	0.03	0.45	0.02
27. 5	ů	Path		134	2.94	0.95	6.7	0.1	0.44	0.14	0.01	1.09	0.62		0.07	0.16	0.09	0.55	0.01
27. 5	ŏ	Path		135	2, 99	0.96	6, 45	0.05	0.46	0.15	0.01	1.19	0.65		0.04	0.18	0.10	0.48	0.01
27.5	0	Path		136	2. 29	0.63	5, 43	0.11	0.42	0.12	0.02	0.88	0.4		0.08	0.16	0.10	0.38	0.01
27. 5	ŏ	Path		137	2.94	0.61	5, 94	0, 11	0.49	0.10	0.02	1,12	0.34		0.08	0.19	0.06	0.54	0.01
27. 5	0	Path		138		0.73	6, 99	0.04	0.48	0.10	0.01	1.31	0.45		0.03	0.19	0.06	0.58	0.00
27. 5	ŏ	Path		139	3, 33	0.47	6.32	0.05	0.53	0.07	0.01	1, 45	0. 27		0.04	0.23	0.04	0.53	0.01
27. 5	0	Path		140	7.04	1.7		0.74	0.52	0.13	0.05	3, 45	1.18		0.56	0.25	0.09	0.51	0.04
27. 5	ů	Path		141	8. 81	2.01	16.64	0.07	0.53	0.12	0.00	4. 43	1.48		0.06	0, 27	0.09	0.62	0,00
27.5	o l	Path		142	9, 23	2.35		0.03	0.52	0.13	0.00	4, 78	1.59		0.02	0, 27	0.09	0.60	0.00
27. 5	ů	Path		143	8, 62	2. 4		0, 11	0.56	0.16	0.01	4. 24	1.74		0.08	0. 28	0.11	0.57	0.01
27. 5	Ŏ	Path		144	6.79	1.65	16, 63	0.15	0, 41	0.10	0.01	2, 97	1.09		0.11	0.18	0.07	0.41	0.01
27.5	0	Path		145	8, 05	1.8	15, 12	0. 21	0.53	0.12	0.01	4.05	1.4		0.13	0. 27	0.09	0.58	0.01
27. 5	Ŏ	Path		146	9, 34	2.17		0.07	0,53	0.12	0.00	4. 78	1.52		0.05	0, 27	0.09	0.61	0.00
27.5	0	Path		147	8, 79	2, 52		0.13	0.54	0.16	0.01	4, 52	1.81	9.8	0.1	0, 28	0.11	0.61	0.01
27. 5	Ö	Path		148		2.03		0.1	0.51	0.13	0.01	3.84	1.4		0.08	0.24	0.09	0.48	0.01

• QTMO N261 LOW channel MIMO

						0.00/2/	6) . 6			Max Ratio			PD(W/m	٥)	^		Max	Ratio	
P						12 PD(W/1			0.58	0.14	0.05					0.30	0.10	0.63	0.04
Frequency (GHz)	M≎dule	Antenna type	Beam 2	Beam 1	evalu	ation su	iriaces	ROORE		Ratio		evaluat	tion su	riaces	шапра		Ra	tio	
(0112)		type			Front	Back	Bottom	Left	Front/worse	Back/worse	Left/worse	Front	Back	Bottom	Left	Front/worse	Back/worse	Bottom/wor	Left/worse
					FIOIIC	Dack	DOCCOM	reit	surface	surface	surface	PIONE	Dach	DO C COM	reit	surface	surface	se surface	surface
27.5	0	Path	128	0	3.75	0.53	7.9	0.13	0.47	0.07	0.02	1.35	0.3	3.4	0.1	0.17	0.04	0.43	0.01
27.5	0	Path	129	1	2.83	0.51	7. 32	0.15	0.39	0.07	0.02	0.92	0.31	2.73	0.11	0.13	0.04	0.37	0.02
27.5	0	Path	130	2	2.58	0.65	7, 25	0.12	0.36	0.09	0.02	0.88	0.41	2.9	0.09	0.12	0.06	0.40	0.01
27.5	0	Path	131	3	2.96	0.62	7.06	0.13	0.42	0.09	0.02	0.97	0.43	2.85	0.1	0.14	0.06	0.40	0.01
27.5	0	Path	132	4	2.75	0.56	6, 59	0.11	0.42	0.08	0.02	0.98	0.33	2.93	0.08	0.15	0.05	0.44	0.01
27.5	0	Path	133	5	6.41	1.28	14, 62	0.37	0.44	0.09	0.03	2.49	0.87	6.51	0.27	0.17	0.06	0.45	0.02
27.5	0	Path	134	6	6.63	1.83	14.3	0.21	0.46	0.13	0.01	2.63	1.17	7.86	0.16	0.18	0.08	0.55	0.01
27.5	0	Path	135	7	7.27	1.82	14, 23	0.1	0.51	0.13	0.01	2.98	1.25	7.8	0.08	0.21	0.09	0.55	0.01
27.5	0	Path	136	8	5. 49	1.11	12.44	0.25	0.44	0.09	0.02	2.18	0.69	5.1	0.19	0.18	0.06	0.41	0.02
27.5	0	Path	137	9	6.73	1.49	14.79	0.33	0.46	0.10	0.02	2.48	0.84	7.47	0.25	0.17	0.06	0.51	0.02
27.5	0	Path	138	10	7.31	2.06	15.06	0.09	0.49	0.14	0.01	2.98	1.22	8.82	0.08	0.20	0.08	0.59	0.01
27.5	0	Path	139	11	7.05	1.22	13.64	0.27	0.52	0.09	0.02	2.84	0.68	7.13	0.21	0.21	0.05	0.52	0.02
27.5	0	Path	140	12	17.31	4.34	36, 78	1.95	0.47	0.12	0.05	8. 27	3.28	18.93	1.45	0.22	0.09	0.51	0.04
27.5	0	Path	141	13	20.75	4.2	36, 96	0.12	0.56	0.11	0.00	10.43	2.81	23. 24	0.11	0.28	0.08	0.63	0.00
27.5	0	Path	142	14	20.01	5.18	36, 35	0.09	0.55	0.14	0.00	10.19	3.54	22. 41	0.06	0.28	0.10	0.62	0.00
27.5	0	Path	143	15	20.64	4.34	35, 47	0.17	0.58	0.12	0.00	10.49	3.29	21.81	0.11	0.30	0.09	0.61	0.00
27.5	0	Path	144	16	14.17	3.48	38, 05	0.63	0.37	0.09	0.02	6.37	2.18	16.36	0.47	0.17	0.06	0.43	0.01
27.5	0	Path	145	17	19.64	4.56	37. 22	0.83	0.53	0.12	0.02	9.67	3.37	22	0.55	0.26	0.09	0.59	0.01
27. 5	0	Path	146	18	20.29	5.07	36, 41	0.2	0.56	0.14	0.01	10.13	3.44	22.56	0.15	0. 28	0.09	0.62	0.00
27.5	0	Path	147	19	20.37	4. 43	35, 92	0.17	0.57	0.12	0.00	10.24	3.21	22.57	0.14	0.29	0.09	0.63	0.00
27.5	0	Path	148	20	17.84	4.06	34, 65	0.19	0.51	0.12	0.01	8.6	2.78	18.3	0.15	0.25	0.08	0.53	0.00

• QTMO N261 Middle channel SISO

						(m (Max Ratio			mm /m (e\			Max	Ratio	
Frequency		Antenna					n2) at 2 urfaces (0.58	0.14	0.05	4cm2 evaluat		2) at 1		0.28	0.09	0.63	0.04
(GHz)	Module	type	Beam 2	Beam 1	evalua	ttion su	uraces (wouds.		Ratio		evaluat	Jon Su	11aces	eoubii			tio	
(0112)		0,00			Front	Back	Bottom	Left	Front/worse		Left/worse	Front	Back	Bottom	Left	Front/worse			Left/worse
									surface	surface	surface					surface		se surface	surface
28	0	Path		0		0.24	3, 39	0.05	0.37	0.07	0.01	0.42	0.14		0.04	0.12	0.04	0.43	0.01
28	0	Path		1	1.13	0.28	3, 27	0.06	0.35	0.09	0.02	0.36	0.16		0.05	0.11	0.05	0.39	0.02
28	0	Path		2		0.21	3, 34	0.04	0.41	0.06	0.01	0.49	0.13		0.03	0.15	0.04	0.43	0.01
28	0	Path		3		0.19	2, 9	0.04	0.52	0.07	0.01	0.56	0.12		0.03	0.19	0.04	0.44	0.01
28	0	Path Path		<u>4</u> 5		0.19	6, 33	0.04	0.50 0.44	0.07	0.01	0.51	0.12		0.03	0.19	0.04	0.50	0.01
28	0	Path Path		6	3, 71	0.65	7, 34	0.14	0.44	0.09	0.02	1.05	0.34		0.04	0.17	0.05	0.43	0.02
28	0	Path		7		0. 65	6, 92	0.03	0.56	0.09	0.01	1.47	0.35		0.04	0.24	0.05	0.57	0.01
28	0	Path		8		0.39	4, 75	0.03	0.53	0.08	0.00	1.08	0. 24		0.03	0.24	0.05	0.39	0.00
28	0	Path		9		0. 62	6. 93	0.09	0.48	0.00	0.02	1. 27	0.36		0.08	0.18	0.05	0.42	0.01
28	0	Path		10		0.85	7, 79	0.03	0.44	0.11	0.00	1.31	0.49		0.02	0.17	0.06	0.56	0.00
28	ŏ	Path		11	2, 61	0.62	6, 26	0.1	0.42	0.10	0.02	0.98	0.39		0.08	0.16	0.06	0.49	0.01
28	o o	Path		12		1.55	15.5	0.84	0.54	0.10	0.05	4.01	1.06		0.6	0, 26	0.07	0.49	0.04
28	0	Path		13		1.94		0.05	0.54	0.11	0,00	4, 73		10, 49	0.04	0, 27	0.07	0,60	0,00
28	0	Path		14		2. 2		0.04	0.52	0.12	0.00	4. 73		11.26	0.02	0.26	0.08	0.62	0.00
28	0	Path		15	8.63	1.61		0.04	0.57	0.11	0.00	4. 23	1.17	9.07	0.03	0.28	0.08	0.60	0.00
28	0	Path		16	5.49	1.35	12.78	0.34	0.43	0.11	0.03	2.4	0.93	5.88	0.26	0.19	0.07	0.46	0.02
28	0	Path		17	9.02	1.84		0.42	0.54	0.11	0.03	4. 4	1.33		0.26	0.26	0.08	0.54	0.02
28	0	Path		18		2.15		0.07	0.52	0.12	0.00	4.63		10.97	0.05	0.26	0.07	0.61	0.00
28	0	Path		19		1.94		0.03	0.53	0.11	0.00	4. 51		10.69	0.02	0.26	0.07	0.61	0.00
28	0	Path		20		1.61	13, 52	0.1	0.58	0.12	0.01	3.75	1.17		0.08	0.28	0.09	0.56	0.01
28	0	Path		128		0.13	3, 63	0.05	0.50	0.04	0.01	0.69	0.08		0.03	0.19	0.02	0.44	0.01
28	0	Path		129		0.15	3, 17	0.03	0.44	0.05	0.01	0.49	0.09		0.03	0.15	0.03	0.43	0.01
28	0	Path		130		0.33	3. 4	0.04	0.33	0.10	0.01	0.34	0.2		0.03	0.10	0.06	0.41	0.01
28	0	Path		131	1.17	0.34	3, 28 2, 94	0.05	0.36	0.10	0.02	0.38	0.23		0.03	0.12	0.07	0.41	0.01
28	0	Path		132	1.1	0.34		0.05	0.37	0.12	0.02	0.39	0.23		0.03	0.13	0.08	0.43	0.01
28 28	0	Path Path		133 134	2. 97 2. 94	0.4	5.9 6.7	0.14	0.50 0.44	0.07 0.14	0.02	1.29	0.19		0.1	0.22	0.03	0.45 0.57	0.02 0.01
28	0	Path		135	3.06	0. 92	6, 75	0.09	0.45	0.14	0.01	1.19	0.59		0.04	0.10	0.09	0.50	0.01
28	0	Path Path		136	2, 32	0.68	5. 47	0.08	0.42	0.13	0.01	0.89	0. 59		0.04	0.18	0.09	0.38	0.01
28	0	Path		137	2.32	0.08	6, 28	0.13	0.42	0.12	0.02	1.15	0.36		0.08	0.10	0.08	0.52	0.02
28	0	Path		138	3, 45	0.71	7.37	0.11	0.47	0.10	0.02	1.34	0. 44		0.03	0.18	0.06	0.57	0.00
28	ŏ	Path		139	3, 61	0.46	6.7	0.05	0.54	0.10	0.01	1.55	0. 27		0.03	0.23	0.04	0.54	0.00
28	ů i	Path		140	6, 99	1. 77		0.7	0.50	0.13	0.05	3. 41	1.29		0.52	0.24	0.09	0.51	0.01
28	ŏ	Path		141	8. 95	2.12		0, 07	0.52	0.12	0.00	4. 42		10.85	0.06	0. 26	0.09	0.63	0.00
28	ŏ	Path		142	9, 51	2, 26	18, 42	0.02	0.52	0.12	0.00	4, 88		11.21	0.02	0, 26	0.09	0.61	0.00
28	Ů,	Path		143	8. 97	2. 42		0.09	0.55	0.15	0.01	4.5	1.74		0.08	0, 28	0.11	0.58	0.00
28	0	Path		144	7, 25	1.64		0.19	0.44	0.10	0.01	3, 15	1.08		0.15	0.19	0.07	0.42	0.01
28	0	Path		145	8.46	1. 91	16.04	0. 21	0.53	0.12	0.01	4.17	1.46		0.13	0.26	0.09	0.59	0.01
28	0	Path		146	9.39	2. 23		0.05	0.52	0.12	0.00	4.74		11.23	0.04	0.26	0.08	0.62	0.00
28	0	Path		147	9.17	2. 38	16.93	0.11	0.54	0.14	0.01	4.7	1.7	10.35	0.09	0.28	0.10	0.61	0.01
28	0	Path		148	8. 51	2.16	16, 52	0.11	0.52	0.13	0.01	4.09	1.49	8. 27	0.09	0.25	0.09	0.50	0.01

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						0. DD /w /	e)			Max Ratio			DD /W /	o)	^		Max	Ratio	
P						2 PD(W/1			0.58	0.14	0.05		PD(W/m			0. 29	0.09	0.63	0.04
Frequency (GHz)	Module	time	Beam 2	Beam 1	evalua	ation su	riaces	MOORN		Ratio		evaluat	ion su	riaces	Moorru		Ra	tio	
(0112)		сурс			Front	Back	Bottom	Left	Front/worse	Back/worse	Left/worse	Front	Pools	Bottom	Loft	Front/worse	Back/worse	Bottom/wor	Left/worse
					FIOIT	Dack	Воссон	reit	surface	surface	surface	PIONE	Dack	DO C COM	reit	surface	surface	se surface	surface
28	0	Path	128	0	3.75	0.52	7, 99	0.16	0.47	0.07	0.02	1.31	0.3	3.5	0.12	0.16	0.04	0.44	0.02
28	0	Path	129	1	2.93	0.5	7, 52	0.15	0.39	0.07	0.02	0.97	0.31	2.88	0.12	0.13	0.04	0.38	0.02
28	0	Path	130	2	2.7	0.68	7.32	0.11	0.37	0.09	0.02	0.96	0.43	2.95	0.08	0.13	0.06	0.40	0.01
28	0	Path	131	3	2.74	0.68	7, 28	0.12	0.38	0.09	0.02	1.05	0.48	2.9	0.09	0.14	0.07	0.40	0.01
28	0	Path	132	4	2.63	0.57	6, 74	0.11	0.39	0.08	0.02	0.95	0.36	2.96	0.08	0.14	0.05	0.44	0.01
28	0	Path	133	5	6.49	1.22	14.7	0.36	0.44	0.08	0.02	2.56	0.84	6.57	0.25	0.17	0.06	0.45	0.02
28	0	Path	134	6	6.88	1.75	14. 91	0.19	0.46	0.12	0.01	2.71	1.16	8.09	0.14	0.18	0.08	0.54	0.01
28	0	Path	135	7	7. 28	2	14.76	0.13	0.49	0.14	0.01	3.03	1.33	7.84	0.09	0.21	0.09	0.53	0.01
28	0	Path	136	8	5.49	1.32	13, 21	0.3	0.42	0.10	0.02	2.12	0.8	5.49	0.23	0.16	0.06	0.42	0.02
28	0	Path	137	9	6.72	1.41	15, 31	0.31	0.44	0.09	0.02	2. 53	0.82	7.53	0.22	0.17	0.05	0.49	0.01
28	0	Path	138	10	7.3	2.08	15, 43	0.1	0.47	0.13	0.01	2.94	1.26	8.9	0.08	0.19	0.08	0.58	0.01
28	0	Path	139	11	7.31	1.19	14.3	0.26	0.51	0.08	0.02	2. 91	0.7	7.45	0.21	0.20	0.05	0.52	0.01
28	0	Path	140	12	17.98	3.88	38, 56	1.99	0.47	0.10	0.05	8.59	3.03	19.97	1.46	0.22	0.08	0.52	0.04
28	0	Path	141	13	20. 41	4.59	37. 62	0.13	0.54	0.12	0.00	10.14	3	23.54	0.1	0.27	0.08	0.63	0.00
28	0	Path	142	14	19.53	5.2	37. 44	0.07	0.52	0.14	0.00	9.7	3.46	22.7	0.05	0.26	0.09	0.61	0.00
28	0	Path	143	15	20.73	4.66	36, 01	0.18	0.58	0.13	0.00	10.5	3.39	22. 25	0.14	0.29	0.09	0.62	0.00
28	0	Path	144	16	15.09	3. 24	38. 73	0.84	0.39	0.08	0.02	6.55	2.09	16.92	0.64	0.17	0.05	0.44	0.02
28	0	Path	145	17	19.65	4.14	38.18	0.79	0.51	0.11	0.02	9.63	2.94	22. 47	0.52	0.25	0.08	0.59	0.01
28	0	Path	146	18	19.94	5. 21	37.3	0.19	0.53	0.14	0.01	9.71	3.44	22. 78	0.14	0.26	0.09	0.61	0.00
28	0	Path	147	19	19.68	4. 48	36.06	0.17	0.55	0.12	0.00	9.7	3.23	22.69	0.14	0.27	0.09	0.63	0.00
28	0	Path	148	20	19.08	4.07	36, 81	0.29	0.52	0.11	0.01	9.3	2.82	20.03	0.22	0.25	0.08	0.54	0.01

• QTMO N261 High channel SISO

										Max Ratio							Иол.	Ratio	
					4cm	2 PD(W/s	n2) at 2	2mm	0, 56	0.14	0, 06	4cm2	PD(W/m	2) at 1	Omm	0, 27	0. 09	0,63	0.04
Frequency	Module	Antenna	Boom 2	Beam 1	evalu	ation su	rfaces	06dBn	0.30	Ratio	0.00	evaluat	tion su	rfaces	@6dBm	0.21		tio	0.04
(GHz)	Module	type	DCum 2	DCum I					Front/worse		Left/worse					Danama /waman		Bottom/wor	Left/worse
					Front	Back	Bottom	Left	surface	surface	surface	Front	Back	Bottom	Left	surface		se surface	surface
28. 35	0	Path		0	1.23	0.23	3, 45	0, 05	0.36	0.07	0.01	0.41	0.14	1.48	0.04	0.12	0.04	0.43	0.01
28.35	0	Path		1	1.12	0.26	3, 31	0.05	0.34	0.08	0.02	0.36	0.15		0.04	0.11	0.05	0.40	0.01
28.35	0	Path		2		0. 22	3, 28	0.04	0.41	0.07	0.01	0.48	0.13		0.03	0.15	0.04	0.42	0.01
28. 35	0	Path		3	1.43	0.19	2, 93	0.04	0.49	0.06	0.01	0.53	0.12	1.32	0.03	0.18	0.04	0.45	0.01
28.35	0	Path		4	1.31	0.18	2.7	0.05	0.49	0.07	0.02	0.49	0.12	1.32	0.03	0.18	0.04	0.49	0.01
28.35	0	Path		5		0.52	6. 24	0.14	0.43	0.08	0.02	1.03	0.3		0.1	0.17	0.05	0.42	0.02
28.35	0	Path		6		0.63	7.37	0.05	0.49	0.09	0.01	1.45	0.37		0.04	0.20	0.05	0.56	0.01
28.35	0	Path		7		0.58	6, 76	0.04	0.55	0.09	0.01	1.58	0.37		0.03	0.23	0.05	0.59	0.00
28.35	0	Path		8		0.39	4.7	0.1	0.49	0.08	0.02	0.95	0.25		0.07	0.20	0.05	0.42	0.01
28.35	0	Path		9		0.59	6, 89	0.11	0.47	0.09	0.02	1.26	0.33		0.08	0.18	0.05	0.49	0.01
28.35	0	Path		10		0.82	7, 75	0.03	0.44	0.11	0.00	1.3	0.47		0.02	0.17	0.06	0.57	0.00
28.35	0	Path		11	2.54	0.62	6.32	0.08	0.40	0.10	0.01	0.92	0.4		0.07	0.15	0.06	0.49	0.01
28.35	0	Path		12		1.57	15, 17	0.84	0.53	0.10	0.06	3.82	1.02		0.6	0. 25	0.07	0.50	0.04
28.35	0	Path		13		1.99	17.48	0.05	0.54	0.11	0.00	4.71		10.62	0.04	0. 27	0.07	0.61	0.00
28.35	0	Path		14		2.3		0.03	0.52	0.13	0.00	4.57	1.34		0.02	0. 26	0.08	0.63	0.00
28.35	0	Path		15		1.58		0.04	0.56	0.10	0.00	4.07	1.17		0.03	0.27	0.08	0.60	0.00
28.35	0	Path Path		16 17		1.31	12.87 16.58	0.34	0.40	0.10	0.03	2. 29 4. 27	0.94		0.27	0.18	0.07	0.46 0.54	0.02
28.35 28.35	0	Path		18		2, 24	17.8	0. 37	0.53	0.11	0.02	4. 27	1.34		0.05	0.25	0.08	0.02	0.01
28, 35	0	Path		19		2.06		0.07	0.52	0.13	0.00	4, 35		10.67	0.03	0.25	0.08	0.62	0.00
28. 35	0	Path		20		1.58		0.03	0.56	0.12	0.00	3.6	1.18		0.03	0.26	0.09	0.56	0.00
28, 35	0	Path		128		0.12	3, 63	0.04	0.50	0.03	0.01	0.69	0.08		0.03	0.19	0.02	0.44	0.01
28. 35	0	Path		129		0.15	3. 2	0.03	0, 41	0.05	0. 01	0.47	0.09		0.03	0.15	0.03	0.42	0, 01
28.35	0	Path		130		0.32	3, 35	0, 04	0.33	0.10	0.01	0.34	0.2		0.03	0,10	0.06	0.41	0.01
28.35	0	Path		131	1.16	0.32	3, 28	0.05	0.35	0.10	0.02	0.38	0. 21	1.35	0.04	0.12	0.06	0.41	0.01
28.35	0	Path		132	1.1	0.35	2, 99	0.04	0.37	0.12	0.01	0.39	0.24	1.29	0.03	0.13	0.08	0.43	0.01
28. 35	0	Path		133	2.89	0.41	5. 9	0.14	0.49	0.07	0.02	1.23	0.18	2.66	0.1	0.21	0.03	0.45	0.02
28.35	0	Path		134		0.89	6, 61	0.08	0.44	0.13	0.01	1.11	0.57		0.05	0.17	0.09	0.58	0.01
28.35	0	Path		135	3.08	0.83	6, 76	0.06	0.46	0.12	0.01	1.2	0.54		0.05	0.18	0.08	0.51	0.01
28.35	0	Path		136	2.31	0.74	5, 48	0.15	0.42	0.14	0.03	0.88	0.48		0.11	0.16	0.09	0.39	0.02
28.35	0	Path		137	2. 91	0.59	6, 36	0.11	0.46	0.09	0.02	1.1	0.37		0.08	0.17	0.06	0.52	0.01
28.35	0	Path		138	3.41	0.69	7.47	0.04	0.46	0.09	0.01	1.32	0.43		0.03	0.18	0.06	0.56	0.00
28.35	0	Path		139	3.66	0.45	6.8	0.05	0.54	0.07	0.01	1.59	0.27		0.04	0.23	0.04	0.53	0.01
28.35	0	Path		140	6.9	1.78		0.65	0.49	0.13	0.05	3.36	1.31		0.47	0.24	0.09	0.51	0.03
28.35	0	Path		141	8.83	2.16		0.08	0.51	0.13	0.00	4.32		10.84	0.06	0. 25	0.08	0.63	0.00
28.35	0	Path		142	9.38	2.32	18, 23	0.02	0.51	0.13	0.00	4.77		11.11	0.02	0. 26	0.08	0.61	0.00
28.35	0	Path		143	8.97	2.39	16.41	0.11	0.55	0.15	0.01	4. 47	1.7		0.09	0. 27	0.10	0.59	0.01
28.35	0	Path		144	7. 26	1.59	15.7	0.23	0.46	0.10	0.01	3.17	1.06		0.18	0.20	0.07	0.42	0.01
28.35	0	Path		145	8.5	1. 91	16.31	0.2	0.52	0.12	0.01	4.15	1.45		0.13	0.25	0.09	0.59	0.01
28.35	0	Path		146	9.17	2. 37	17.9	0.05	0.51	0.13	0.00	4.57		11.07	0.04	0.26	0.08	0.62	0.00
28.35	0	Path		147	9. 21	2. 27		0.09	0.54	0.13	0.01	4.7	1.61		0.07	0.28	0.09	0.61	0.00
28.35	0	Path		148	8.4	2.13	16, 26	0.12	0.52	0.13	0.01	4.08	1.48	8.29	0.09	0.25	0.09	0.51	0.01

• QTMO N261 High channel MIMO

														Max Ratio					
TP.						4cm2 PD(W/m2) at 2mm			0.57	0.14	0.05	4cm2 PD(W/m2) at 10mm			0. 28	0.10	0.62	0.04	
Frequency (GHz)	Module	Antenna type	Beam 2	Beam 1	evaluation surfaces @6dBm			Ratio			evaluation surfaces @6dBm				Ratio				
(0112)		сурс			Front	Back	Bottom	Left	Front/worse	Back/worse	Left/worse	Front	Back	Bottom	Left	Front/worse	Back/worse	Bottom/wor	Left/worse
						Duon	Doocom	2010	surface	surface	surface		Duon		2010	surface	surface	se surface	surface
28.35	0	Path	128	0	3.7	0.5	7. 95	0.16	0.47	0.06	0.02	1.28	0.29		0.12	0.16	0.04	0.44	0.02
28.35	0	Path	129	1	2. 91	0.49	7, 52	0.15	0.39	0.07	0.02	0.99	0.31	2.89	0.11	0.13	0.04	0.38	0.01
28.35	0	Path	130	2	2.68	0.7	7. 28	0.1	0.37	0.10	0.01	0.98	0.44	2.89	0.08	0.13	0.06	0.40	0.01
28.35	0	Path	131	3	2.76	0.67	7, 22	0.12	0.38	0.09	0.02	1.02	0.48	2.89	0.1	0.14	0.07	0.40	0.01
28.35	0	Path	132	4	2.58	0.58	6.67	0.11	0.39	0.09	0.02	0.96	0.37	2.94	0.08	0.14	0.06	0.44	0.01
28.35	0	Path	133	5	6.38	1.18	14.38	0.37	0.44	0.08	0.03	2.54	0.78	6.45	0.26	0.18	0.05	0.45	0.02
28.35	0	Path	134	6	6.83	1.7	14.87	0.18	0.46	0.11	0.01	2.7	1.12	8.04	0.14	0.18	0.08	0.54	0.01
28.35	0	Path	135	7	7.12	1.97	14.67	0.14	0.49	0.13	0.01	2. 98	1.33	7.86	0.11	0.20	0.09	0.54	0.01
28.35	0	Path	136	8	5. 41	1.36	13.1	0.36	0.41	0.10	0.03	2.06	0.84	5.49	0.27	0.16	0.06	0.42	0.02
28.35	0	Path	137	9	6.54	1.36	15, 35	0.31	0.43	0.09	0.02	2.53	0.82	7.4	0.22	0.16	0.05	0.48	0.01
28.35	0	Path	138	10	7.15	2.04	15. 45	0.1	0.46	0.13	0.01	2.87	1.23	8.77	0.07	0.19	0.08	0.57	0.00
28.35	0	Path	139	11	7. 28	1.16	14. 45	0.24	0.50	0.08	0.02	2.93	0.72	7.4	0.19	0.20	0.05	0.51	0.01
28.35	0	Path	140	12	18.05	3.56	38. 88	2.01	0.46	0.09	0.05	8. 59	2. 78	20.11	1.46	0.22	0.07	0.52	0.04
28.35	0	Path	141	13	19.71	4.62	37.18	0.15	0.53	0.12	0.00	9.82	3.16	23.08	0.11	0.26	0.08	0.62	0.00
28. 35	0	Path	142	14	18.98	5.17	37.01	0.07	0.51	0.14	0.00	9.42	3.39	22.65	0.05	0.25	0.09	0.61	0.00
28.35	0	Path	143	15	20.14	4.76	35, 62	0.19	0.57	0.13	0.01	10.11	3. 41	22.05	0.16	0.28	0.10	0.62	0.00
28.35	0	Path	144	16	15. 29	3.08	38. 55	0.96	0.40	0.08	0.02	6.58	2. 01	16.87	0.74	0.17	0.05	0.44	0.02
28.35	0	Path	145	17	19.31	4.04	38.17	0.73	0.51	0.11	0.02	9.44	2. 71	22. 41	0.48	0.25	0.07	0.59	0.01
28. 35	0	Path	146	18	19.27	5. 23	37	0.17	0.52	0.14	0.00	9.3	3.46	22. 42	0.13	0.25	0.09	0.61	0.00
28. 35	0	Path	147	19	18.8	4.53	35. 54	0.16	0.53	0.13	0.00	9.13	3. 23	22.34	0.13	0.26	0.09	0.63	0.00
28.35	0	Path	148	20	19.18	4.05	36.88	0.36	0.52	0.11	0.01	9.36	2.8	20.31	0.27	0.25	0.08	0.55	0.01

Table 3.4-1: Max Ratio for SISO and MIMO per band per module

Band	module	Distance	Max Ratio for SISO	Max Ratio for MIMO		
N260	2mm		0.69	0.67		
N260	0	10mm	0.71	0.73		
NOC 1	0	2mm	0.59	0. 58		
N261	0	10mm	0.63	0.63		

PD design target

For Qualcomm SDX62/QTM545, the total device uncertainty for mmW radio is 2.0dB. To account for the total design related uncertainty, PD design target needs to be:

$$PD_design_target < PD_{regulatory_limit} \times 10^{\frac{-total\,uncertainty}{10}}$$

With FCC 4cm2-averaged PD requirement of 10 W/m2 and the declared 2.0 dB device design related uncertainty, the PD_design_target for the EUT is determined as:

$$PD_design_target = 6 W/m^2$$

Worst-case housing influence determination

For non-metal material, the material property cannot be accurately characterized at mmW frequencies to date. The estimated material property for the device housing is used in the simulation model, which could influence the accuracy in simulation for PD amplitude quantification. Since the housing influence on PD could vary from surface to surface where the EM field propagates through, the most underestimated surface is used to quantify the worst-case housing influence for conservative assessment.

Since the mmW antenna modules are placed at different location as shown in Figure 3.1-2, only material/housing surrounded has impact on EM field propagation, in turn impact on power density. Therefore, only adjacent surfaces for each QTM (as listed in Table 3-2) were used to evaluate the worst-case housing influence for each frequency band. For this EUT, when comparing a simulated 4cm2-avgeraged PD and measured 4 cm2-avgerated PD, the worst error introduced for each antenna module operating at each band when using the estimated material property in the simulation is highlighted yellow in Table 3.3-2. Thus, the worst-case housing influence, denoted as Δ min=Sim.PD-Meas.PD, is determined as:

Table 3.5-1: $\Delta \min$ for QTMO

Band	QTM	Δmin(db)				
N260	0	-0.31				
N261	0	2. 25				

 Δ min represents the worst case where RF exposure is underestimated the most in simulation when using the estimated material property for glass/plastics of the housing. For conservative assessment, the is used as the worst-case factor and applied to all the beams in the corresponding beam group to determine input power limits in PD char for compliance.

PD Char of the EUT

This section describes the PD Char generation that complies with the PD_design_target determined in Section 3.5.1 and is in compliance with the regulatory power density limit.

Scaling factor for SISO beams

Determine scaling factor for low, mid, high channel, S(i)low_or_mid_high by:

$$S(i)_{low\ or\ mid\ or\ high} = \frac{PD\ design\ target}{sim.PD_{surface(i)}} \quad , i \in SISO\ beams$$

Then finalize scaling factor, **S(i)**, by using equation below:

$$S(i) = min\{s_{low}(i), s_{mid}(i), s_{high}(i)\}, i \in SISO \ beams$$

and this scaling factor **S(i)**, is applied to the input power at each antenna port to determine input. power. limit for SISO beams.

scaling factor S(i) list

Scaling factor for MIMO beams

The relative phase between beam pair is not controlled in the EUT and could vary from run to run. Therefore, for beam pair, based on the simulation results, the worst-case scaling factor needs to be determined mathematically to ensure the compliance.

For beam pair, extract the E-fields and H-fields from the corresponding single beams at low, mid and high channel for each supported band and for all identified surfaces of the EUT.

For a given beam pair containing $beam_a$ and $beam_b$, and for a given channel, let relative phase between $beam_a$ and $beam_b = \varnothing$, and the total PD of the beam pair can be expressed as:

$$\begin{split} total \; PD \; (\emptyset) &= \frac{1}{2} \sqrt{Re\{PD_x(\emptyset)\}^2 + Re\{PD_y(\emptyset)\}^2 + Re\{PD_z(\emptyset)\}^2} \\ &= \frac{1}{2} Re\left\{ \left(\overrightarrow{E_a} + \overrightarrow{E_b e^{\jmath \omega \emptyset}}\right) \times \left(\overrightarrow{H_a} + \overrightarrow{H_b e^{\jmath \omega \emptyset}}\right)^* \right\} \; (4) \end{split}$$

where, $PDx(\varnothing)$, $PDy(\varnothing)$ and $PDz(\varnothing)$ are the three components of the total $PD(\varnothing)$; and are the extracted E-fields and H-fields of $beam_a$, while and are the extracted E-fields and H-fields of $beam_b$. Sweep \varnothing with a 5° step from 0° to 360° to determine the worst-case, \varnothing , which results in the highest total $PD(\varnothing)$ among all identified surfaces for this MIMO beam at this channel.

Follow the above procedure to determine \varnothing for all three channels of all bands supported, and obtain the scaling factor given by the below equation for low, mid and high channels:

$$s(i)_{low_or_mid_or_high} = \frac{\textit{PD design target}}{\textit{total PD }(\emptyset(i)_{\textit{worstcase}})}, i \in \textit{MIMO beams}$$

Similar to SISO beam, the worst-case scaling factor, S(i), for MIMO beam i is determined as:

 $s(i) = min\{slow(i), smid(i), shigh(i)\}, i \in MIMO beams$

and this scaling factor **S(i)**, is applied to the input power at each antenna port to determine input. power. limit for MIMO beams.

				Si	Si	Si	Si		_	l			Si	Si	Si	Si
Band	Module	Beam2	Beam1	Low	Mid	Hi gh	•in		Band	Module	Beam2	Beam1	Low	Mid	High	min
n260	0		0	2.07	2.03	2.03	2.03	Ц	n261	0		0	1.85	1.77	1.74	1.74
n260	0		1	2.11	2.13	2.14	2.11	Ц	n261	0		1	1.90	1.83	1.81	1.81
n260	0		2	1.73	1.80	1.85	1. 73	Н	n261	0		2	1.81	1.80	1.83	1.80
n260 n260	0		3 4	1.88	1.93	2.04 1.94	1.88	Н	n261 n261	0		3 4	2.11	2.07	2.05	2.05
n260	0		5	0.95	0.96	0.94	0.94	Н	n261	0		5	0.94	0.95	0.96	0.94
n260	0		6	0.98	1.05	1.10	0.98	H	n261	ő		6	0.86	0.82	0.81	0.81
n260	0		7	0.95	1.02	1.08	0.95	Ħ	n261	0		7	0.85	0.87	0.89	0.85
n260	0		8	0.87	0.87	0.92	0.87		n261	0		8	1.30	1.26	1.28	1.26
n260	0		9	0.96	1.00	1.03	0.96		n261	0		9	0.88	0.87	0.87	0.87
n260	0		10	0.96	1.00	1.10	0.96		n261	0		10	0.79	0.77	0.77	0.77
n260	0		11	0.92	0.91	0.93	0.91	Ц	n261	0		11	0.99	0.96	0.95	0.95
л260	0		12	0.57	0.54	0.53	0.53	Ц	n261	0		12	0.38	0.39	0.40	0.38
n260	0		13	0.48	0.54	0.57	0.48	Н	n261	0		13	0.37	0.35	0.34	0.34
n260	0		14	0.43	0.44	0.51	0.43	Н	n261	0		14	0.34	0.33	0.34	0.33
n260 n260	0		15 16	0. 44 0. 52	0.48 0.54	0.49	0. 44 0. 52	Н	n261 n261	0		15	0.41	0.40	0.40	0.40
n260	0		17	0.56	0.54	0.53 0.58	0.56	Н	n261	0		16 17	0.46	0.47	0.47	0.46
n260	0		18	0.45	0.49	0.55	0.45	Н	n261	0		18	0.35	0.33	0.34	0.33
n260	0		19	0.42	0.42	0.47	0.42	\forall	n261	0		19	0.36	0.34	0.35	0.34
n260	0		20	0.47	0.51	0.51	0.47		n261	0		20	0.45	0.44	0.44	0.44
n260	0		21	2.07	2.14	2.28	2.07		n261	0		21	1.71	1.65	1.65	1.65
n260	0		22	1.88	1.92	1.98	1.88		n261	0		22	2.01	1.89	1.88	1.88
n260	0		23	1.71	1.71	1.78	1.71		n261	0		23	1.76	1.76	1.79	1.76
n260	0		24	1.9	1.93	1.94	1.90	Ц	n261	0		24	1.88	1.83	1.83	1.83
n260	0		25	1. 79	1.80	1.89	1.79	Ц	n261	0		25	2.08	2.04	2.01	2.01
n260	0		26	0.96	0.94	0.97	0.94	Н	n261	0		26	1.06	1.02	1.02	1.02
n260	0		27	1.03	1.07	1.16	1.03	Н	n261	0		27	0.90	0.90	0.91	0.90
n260 n260	0		28 29	0.92 0.92	0.95 0.91	1.01 0.93	0. 92 0. 91	Н	n261 n261	0		28 29	0.93 1.10	0.89 1.10	0.89 1.09	0.89 1.09
n260	0		30	0.96	0.94	0.94	0.94	Н	n261	0		30	1.01	0.96	0.94	0.94
n260	0		31	0.95	1.00	1.05	0.95	H	n261	0		31	0.86	0.81	0.80	0.80
n260	0		32	0.94	0.92	0.94	0.92	H	n261	ō		32	0.95	0.90	0.88	0.88
n260	0		33	0.56	0.51	0.52	0.51	T	n261	0		33	0.44	0.43	0.43	0.43
n260	0		34	0.47	0.53	0.52	0.47		n261	0		34	0.36	0.35	0.35	0.35
n260	0		35	0.43	0.44	0.49	0.43		n261	0		35	0.34	0.33	0.33	0.33
n260	0		36	0.45	0.47	0.49	0.45	Ц	n261	0		36	0.39	0.37	0.37	0.37
n260	0		37	0.54	0.52	0.53	0.52	Ц	n261	0		37	0.36	0.37	0.38	0.36
п260	0		38	0.55	0.54	0.54	0.54	Ц	n261	0		38	0.40	0.37	0.37	0.37
n260	0		39	0.44	0.47	0.51	0.44	Н	n261	0		39	0.34	0.33	0.34	0.33
n260 n260	0		40 41	0.4	0. 44 0. 52	0.50 0.51	0. 40 0. 50	Н	n261 n261	0		40 41	0.37	0.35	0.35 0.37	0.35 0.36
n260	0		128	1.01	0.99	1.02	0.99	Н	n261	0		128	0. 76	0. 75	0. 75	0. 75
n260	0		129	0.93	0.93	0.91	0.91	\forall	n261	0		129	0. 82	0.15	0.80	0.80
n260	0				0.83	0.84	0.78	\forall	n261	0		130	0.83	0.82	0.82	0.82
n260	0		131	0.88	0.91	0.92	0.88	H	n261	0		131	0.85	0.82	0.83	0.82
n260	0		132	0.84	_	0.93	0.84		n261	0		132	0.91	0.89	0.90	0.89
n260	0		133	0.46	0.44	0.45	0.44		n261	0		133	0.41	0.41	0.42	0.41
n260	0		134	0.52	0.56	0.60	0.52	Ц	n261	0		134	0.42	0.40	0.40	0.40
n260	0		135	0.42	0.45	0.45	0.42	Ц	n261	0		135	0.42	0.41	0.41	0.41
n260	0		136	0.4	0.40	0.41	0.40	Ц	n261	0		136	0.48	0.45	0.46	0.45
n260	0		137	0.47		0.46	0.45	Н	n261	0		137	0.41	0.39	0.39	0.39 0.39
n260 n260	0		138 139	0.44	0. 44 0. 38	0.48	0. 44 0. 38	\dashv	n261 n261	0		138 139	0.40	0.39	0.39	0.39
n260	0		140	0.23	0.22	0.39	0. 22	Н	n261	0		140	0.44	0.42	0.42	0.42
n260	0		141	0.21	0.22	0.22	0.21	Н	n261	0		141	0.16	0.16	0.16	0.16
n260	0		142	0.21	0.21	0.24	0.21	H	n261	ő		142	0.17	0.16		0.16
n260	0		143	0.18	_	0.19	0.18	П	n261	0		143	0.17	0.17	0.17	0.17
n260	0		144	0.21	0.20	0.21	0.20		n261	0		144	0.16	0.15	0.16	0.15
n260	0		145	0.25	0.25	0.25	0.25		n261	0		145	0.16	0.16	0.16	0.16
n260	0		146	0.21	0.20	0.22	0.20		n261	0		146	0.16	0.16	0.16	0.16
n260	0					0.21	0.18	Ц	n261	0		147	0.17	0.17	0.17	0.17
n260	0		148	0.19	0.20	0.19	0.19	Ц	n261	0		148	0.17	0.16	0.16	0.16

Input power limit when only $mm\mathbb{W}$ radio is ON

When only $mm\mathbb{W}$ radio is on, the power limit specifies the power level (denoted as

input. power. limit) at antenna port that corresponds to PD_design_target for all the beams. The reference power used in simulation is 6dBm and denoted as *Pref.*

The logic to determine *input.power.limit* is as shown below:

If -TxAGC uncertainty at reference power level < Δ min < TxAGC uncertainty at reference power level, then

input. power. $limit(i) = Pref + 10 * log(S(i)), i \in all beams(1)$

else if Δ min < -TxAGC uncertainty at reference power level,

input. power. limit(i)=Pref+10*log(S(i))+(Δmin +TxAGC uncertanity at reference power level) (2) $I \in all \ beams$

else if Δ min > TxAGC uncertainty at reference power level,

input. power. $limit(i) = Pref + 10 * log(S(i)) + (\Delta min - TxAGC uncertanity at reference power level)$ (3) $I \in all \ beams$

Following above logic, the *input. power. limit* for this EUT can be calculated as:

Table 3.5-2: power.limit calculation

Band	Module	Δmin(db)	Input.power.limit(dbm)	Notes
N260	0	-0.31	6dbm+10*log(S(i))	Using Eq.1
N261	0	2. 25	6dbm+10*log(S(i))+(2.25-0.63)	Using Eq.3

Note the $\Delta \min$ (dB) used is the minimum of Hpol and Vpol per QTM per band (see Table 3.3-2). Resulted *input.power.limit* for all beams is listed in Table below

				Si	Δ	P	input.					Si	Δ	,	input.
Band	Module	Beam2	Beam1	min	min	Equa tion	power.	Band	Module	Beam2	Beam1	min	min	Equa tion	power.
n260	0		0	2.03	-0.31	Eq. 1	1imit 9.08	n261	0		0	1.74	2.25	Eq. 3	limit 10.02
n260	0		1	2.11		Eq. 1	9.23	n261	0		1	1.81	2.25	Eq. 3	
n260	0		2	1.73	- 0.31	Eq. 1	8.38	n261	0		2	1.80	2.25	Eq. 3	10.16
n260	0		3	1.88	-0.31	Eq. 1	8.74	n261	0		3	2.05	2.25	Eq. 3	10. 73
n260 n260	0		4 5	1.73 0.94	-0.31 -0.31	Eq. 1	8.39 5.73	n261 n261	0		4 5	2.21 0.94	2.25	Eq. 3	11.06 7.36
n260	0		6	0.98	-0.31	Eq. 1	5. 93	n261	0		6	0.81	2.25	Eq. 3	6.73
n260	0		7	0.95	-0.31	Eq. 1	5.77	n261	0		7	0.85	2.25	Eq. 3	6.93
n260	0		8	0.87	- 0.31	Eq. 1	5.39	n261	0		8	1.26	2.25	Eq. 3	8.63
n260	0		9	0.96	-0.31	Eq. 1	5.83	n261	0		9	0.87	2.25	Eq. 3	6.99
n260 n260	0		10 11	0.96	-0.31 -0.31	Eq. 1	5.82 5.59	n261 n261	0		10 11	0. 77 0. 95	2.25	Eq. 3	6.49 7.39
n260	0		12	0.53		Eq. 1	3.25	n261	0		12	0.38	2.25	Eq. 3	3.42
n260	0		13	0.48	-0.31	Eq. 1	2.83	n261	0		13	0.34	2.25	Eq. 3	2.98
n260	0		14	0.43	-0.31	Eq. 1	2.31	n261	0		14	0.33	2.25	Eq. 3	2.82
n260	0		15	0.44		Eq. 1	2.43	n261	0		15	0.40	2.25	Eq. 3	3.59
n260 n260	0		16 17	0.52 0.56	-0.31 -0.31	Eq. 1	3. 19 3. 48	n261 n261	0		16 17	0.46	2.25	Eq. 3	4.23 3.16
n260	0		18	0.45	-0.31	Eq. 1	2.58	n261	0		18	0.38	2.25	Eq. 3	2.87
n260	0		19	0.42	-0.31	Eq. 1	2.24	n261	0		19	0.34	2.25	Eq. 3	2.99
n260	0		20	0.47	-0.31	Eq. 1	2.74	n261	0		20	0.44	2.25	Eq. 3	4.06
n260	0		128	2.07	-0.31	Eq. 1	9.16	n261	0		128	1.65	2.25	Eq. 3	9.80
n260 n260	0		129 130	1.88		Eq. 1	8. 74 8. 33	n261 n261	0		129 130	1.88	2.25	Eq. 3	
n260	0		131	1.90	-0.31	Eq. 1	8.80	n261	0		131	1.83	2.25	Eq. 3	10.24
n260	0		132	1.79	-0.31	Eq. 1	8.53	n261	0		132	2.01	2.25	Eq. 3	10.64
n260	0		133	0.94	-0.31	Eq. 1	5. 72	n261	0		133	1.02	2.25	Eq. 3	7.69
n260	0		134	1.03	-0.31	Eq. 1	6.13	n261	0		134	0.90	2.25	Eq. 3	7.14
n260 n260	0		135 136	0.92	-0.31 -0.31	Eq. 1	5.66 5.59	n261 n261	0		135 136	0.89 1.09	2.25	Eq. 3	7. 10 8. 01
n260	0		137	0.94	-0.31	Eq. 1	5. 71	n261	0		137	0.94	2.25	Eq. 3	7.37
n260	0		138	0.95	-0.31	Eq. 1	5. 76	n261	ō		138	0.80	2.25	Eq. 3	6.67
n260	0		139	0.92	- 0.31	Eq. 1	5.66	n261	0		139	0.88	2.25	Eq. 3	7.08
n260	0		140	0.51	-0.31	Eq. 1	3.11	n261	0		140	0.43	2.25	Eq. 3	3.95
n260 n260	0		141 142	0.47	-0.31 -0.31	Eq. 1	2.76	n261 n261	0		141 142	0.35	2.25	Eq. 3	3.05 2.75
n260	0		143	0.45	-0.31	Eq. 1	2.49	n261	0		143	0.33	2.25	Eq. 3	3.25
n260	0		144	0.52	-0.31	Eq. 1	3.16	n261	0		144	0.36	2.25	Eq. 3	3.19
n260	0		145	0.54		Eq. 1	3.29	n261	0		145	0.37	2.25	Eq. 3	3.28
n260	0		146	0.44	-0.31			n261	0		146			Eq. 3	
n260 n260	0		147 148	0.40	-0.31 -0.31			n261 n261	0		147 148	0.35	2, 25	Eq. 3	
n260	0	128	0	0.99	-0.31			n261	0	128	0	0. 75	2.25	Eq. 3	
n260	0	129	1	0.91	-0.31	Eq. 1	5.59	n261	0	129	1	0.80	2.25	Eq. 3	6.64
п260	0	130	2	0. 78	-0.31		_	n261	0	130	2	0.82	2.25	Eq. 3	
n260	0	131	3		-0.31			n261	0	131	3	0.82	2.25	Eq. 3	
n260 n260	0	132 133	4 5	0.84	-0.31 -0.31			n261 n261	0	132 133	4 5	0.89	2, 25	Eq. 3	
n260	0	134	6		-0.31			n261	0	134	6	0.40	2.25	Eq. 3	
n260	0	135	7	0.42	-0.31			n261	0	135	7	0.41	2.25	Eq. 3	
n260	0	136	8	0.40	-0.31			n261	0	136	8	0.45	2.25	Eq. 3	
n260	0	137	9	0.45	-0.31			n261	0	137	9	0.39	2.25	Eq. 3	
n260 n260	0	138 139	10 11	0.44	-0.31 -0.31			n261 n261	0	138 139	10 11	0.39 0.42	2.25	Eq. 3	
n260	0	140	12	0.22	-0.31			n261	0	140	12	0.42	2.25		-0.50
n260	0	141	13	0.21			-0.75	n261	0	141	13		2.25		-0.35
n260	0	142	14		-0.31	Eq. 1	-0.87	n261	0	142	14		2.25	Eq. 3	-0.33
n260	0	143	15	0.18	-0.31			n261	0	143	15	0.17	2.25		-0.16
n260 n260	0	144 145	16 17	0.20	-0.31 -0.31			n261 n261	0	144 145	16 17	0.15 0.16	2.25	_	-0.48 -0.42
n260	0	146	18	0.26			-0. 95	n261	0	146	18	0.16	2.25		-0.32
n260	0	147	19				-1.35	n261	0	147	19		2.25		-0.17
n260	0	148	20	0.19			-1.19	n261	0	148	20	0.16	2.25	Eq. 3	- 0.27