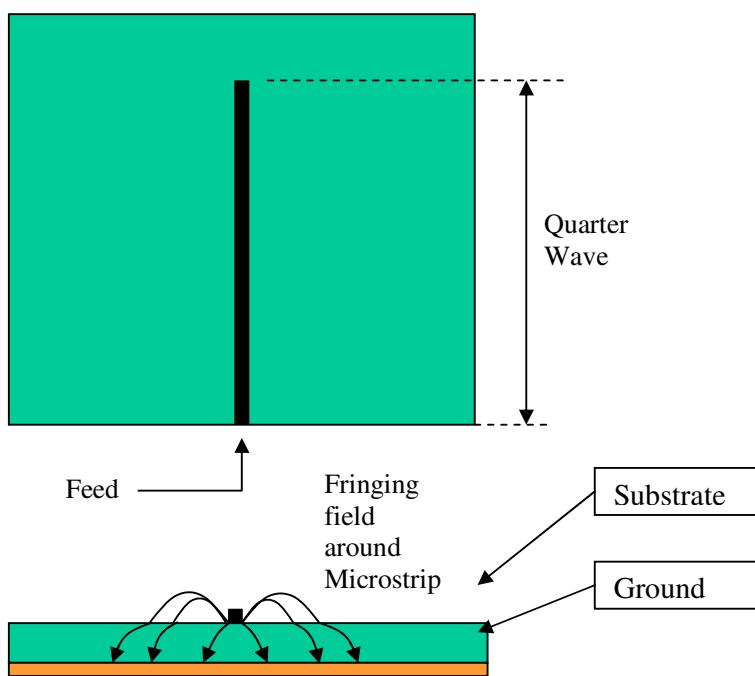


Printed and surface mount antennas have certain common properties. Area around and beneath the radiating element must be kept copper free. Ground plane must be provided on one side of the radiating element. Bandwidth $>100\text{MHz}$ with $\text{VSWR} < 2.5$ and efficiency $>60\%$.

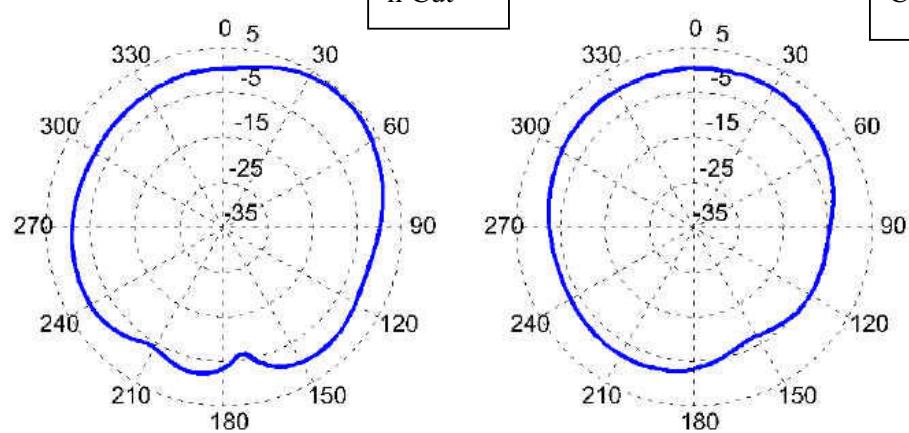
The antenna will de-tune if any object is placed close to it (in its near field). This has an effect of pulling the frequency, which must be retuned to 2.45GHz

An oscillating or constantly accelerating charge is critical in producing propagating waves, a static or non-accelerating charge will result in a non-propagating electric field. But this is not the only condition for radiation. Consider a printed $\lambda/4$ element on microstrip;

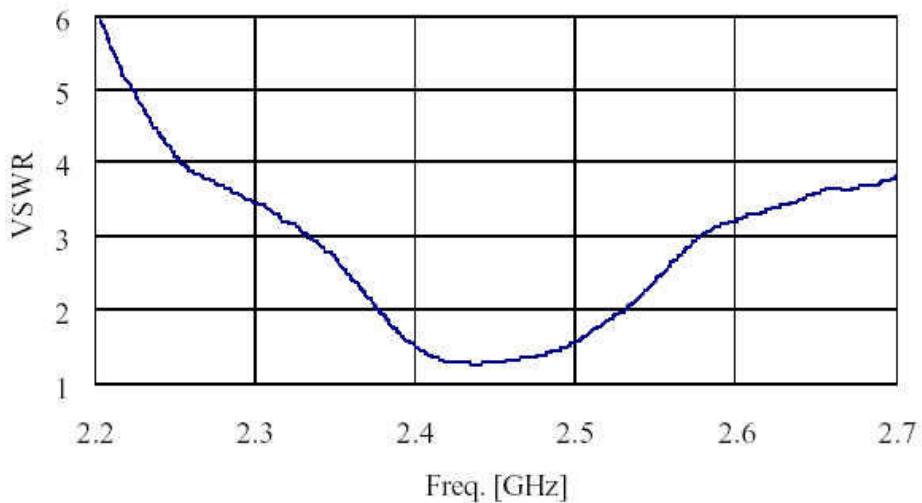


The fringing field around the microstrip due to the ground plane directly underneath the substrate will be confined to a small area. If a network analyzer is connected to the feed point, it would indicate a high VSWR and narrow bandwidth. This means very little radiation is being emitted from the microstrip element. To increase the radiation emission and achieve a better bandwidth, we have to move the ground plane away from the microstrip element, making the fringing field cover more distance. But it should be noted that if the ground plane is moved too far then the fringing field stops altogether, and there is no radiation. Therefore the position and size of the ground plane is vital in the design of a good radiator.

The antenna could be imagined as an impedance transformer, transforming the impedance of a microstrip line (50Ω) to that of free space (377Ω) allowing the power to be transferred from guided wave to free space wave.

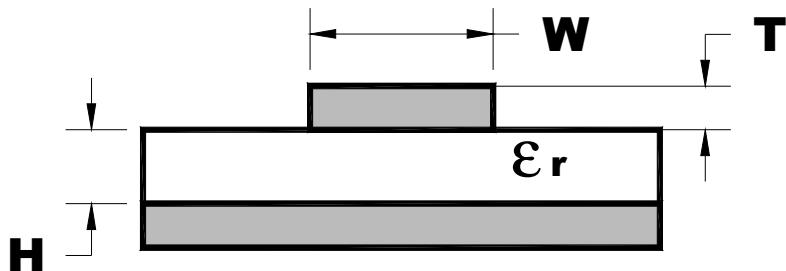
spirobank II antenna specification


The radiation pattern from such antennas where the physical size is much smaller then wavelength ($L \ll \lambda$) is almost symmetrical in all directions as shown above. Only when L is similar or greater then λ , can the pattern be controlled.



Input return loss when viewed on a network analyzer looks like as shown here with the full band covered with $VSWR < 2$. This gives very good matching into the antenna, however in real conditions when the antenna is detuned due to handling or placement of components close to it, the VSWR of 3 to 4 is normal.

For the MIR device, an SMD ceramic chip was chosen, for reasons of dimensions. The following microstrip model can be used to calculate the impedance of the trace which carries the signal to the antenna.:



The above diagram shows that the trace must have an impedance of 50Ω , then the dielectric and also the earthing system.

The impedance must be 50Ω in order to maintain the ROS "stationary waves" as close as possible to 1. Otherwise, there will be losses as the antenna is not suitable. These losses can then only be eliminated by calculating the length of the trace which must be equal to $\lambda/2$.

Dielectric Constant ϵ_r	4,6
Dielectric Thickness (mils) H	3,9
Trace Width (mils) W	5,4
Finished Copper Weight (mils) T	1,4
RESULTS	
Impedance Z_0 (Ohms)	50,03
Inductance/inch L_0 (nH/in)	7,149
Capacitance/inch C_0 (pF/in)	2,857
Propagation Delay T_{pd} (nS/in)	0,1430

These are the formulas used:

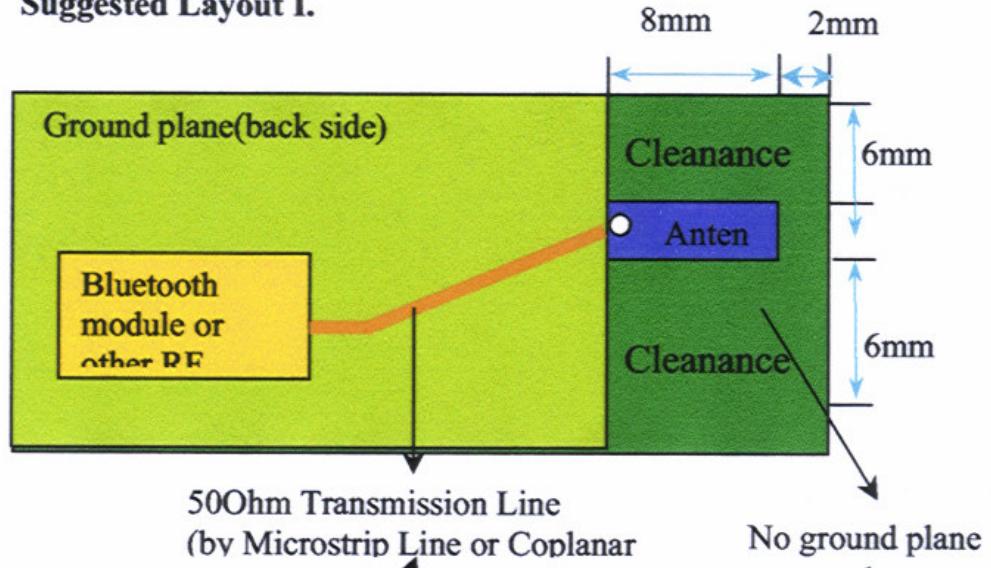
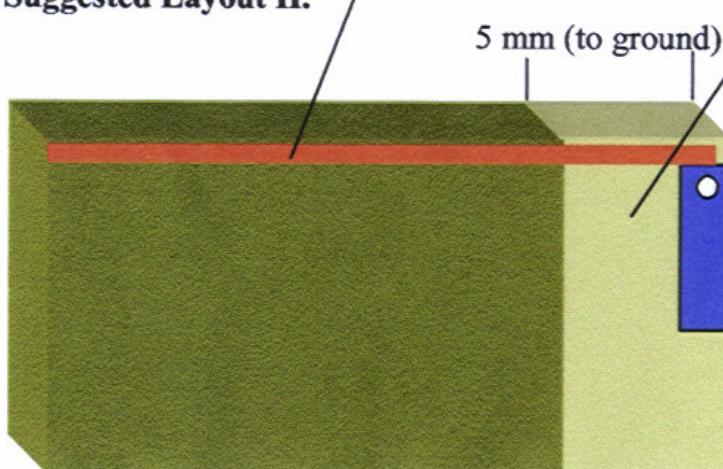
$$Z_0 = (87 / (\text{SQRT}(\epsilon_r + 1.41))) * \text{LN}((5.98 * H) / (0.8 * W + T))$$

$$L_0 = 0.001 * (C_0 * \text{SUMSQ}(Z_0))$$

$$C_0 = (0.67 * (\epsilon_r + 1.41)) / \text{LN}((5.98 * H) / (0.8 * W + T))$$

$$T_{pd} = 0.0833 * (1.016 * (\text{SQRT}(0.475 * \epsilon_r + 0.67)))$$

In the specific case of our ceramic chip, in order to have the maximum radiation, the antenna mounting specifications are as follows:

Suggested Layout I.**Suggested Layout II.**

Note: Optional matching network may be necessary
if 5mm isolation distance to ground is reduced.