



**Hearing Aid Compatibility (HAC)
RF Emissions Test Report
for
Nokia Inc.
on the
CDMA 2000 1xRTT Mobile Phone**

Report No. : HA820515-A
Trade Name : Nokia
Model Name : RH-109
FCC ID : QMNRH-109
Date of Testing : Mar. 31, 2008
Date of Report : Apr. 22, 2008
Date of Review : Apr. 22, 2008

- **Results Summary : M Category = M3**
- The test results refer exclusively to the presented test model/sample only.
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- Report Version: Rev.03

SPORTON International Inc.

No.52, Hwa-Ya 1st RD., Hwa Ya Technology Park, Kwei-Shan Hsiang, TaoYuan Hsien, Taiwan, R.O.C.



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1. Statement of Compliance

The Hearing Aid Compliance (HAC) maximum results found during testing for the Nokia Inc. CDMA 2000 1xRTT Mobile Phone Nokia RH-109 are as follows (with expanded uncertainty $\pm 29.4\%$ for E-field and $\pm 21.8\%$ for H-field):

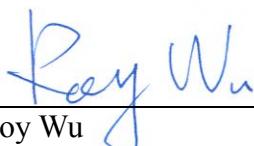
Band	E-Field (V/m)	M Rating	H-Field (A/m)	M Rating
CDMA2000 Cellular	127.4	M4	0.12	M4
CDMA2000 AWS	66.1	M3	0.157	M4
CDMA2000 PCS	59.6	M4	0.167	M4

Remark :
HAC test data for part 27 AWS band are provided for reference only, that they are not part of requirements for equipment authorization under part 20.19.

They are in compliance with HAC limits specified in guidelines FCC 47CFR §20.19 and ANSI Standard ANSI C63.19 for HAC Rated category M3.

Results Summary : M Category = M3

Approved by



Roy Wu
Manager



2. Administration Data

2.1 Testing Laboratory

Company Name : Sporton International Inc.
Department : Antenna Design/SAR
Address : No.52, Hwa-Ya 1st RD., Hwa Ya Technology Park, Kwei-Shan Hsiang, TaoYuan Hsien, Taiwan, R.O.C.
Telephone Number : 886-3-327-3456
Fax Number : 886-3-327-0973

2.2 Detail of Applicant

Company Name : Nokia Inc.
Address : 12278 Scripps Summit Dr. San Diego CA92131 USA

2.3 Detail of Manufacturer

Company Name : Compal Communications(Nanjing) Co., Ltd.
Address: Nanjing Jiangning Export Processing Zone (South Area) No.68-2 Suyuan Street

2.4 Application Details

Date of reception of application: Mar. 21, 2008
Start of test : Mar. 31, 2008
End of test : Mar. 31, 2008



3. General Information

3.1 Description of Device Under Test (DUT)

DUT Type	CDMA 2000 1xRTT Mobile Phone
Trade Name	Nokia
Model Name	RH-109
FCC ID	QMNRH-109
MEID	268435456102522603
Tx Frequency	CDMA2000 Cellular : 824 ~ 849 MHz CDMA2000 AWS : 1710 ~ 1755 MHz CDMA2000 PCS : 1850 ~ 1910 MHz
Rx Frequency	CDMA2000 Cellular : 869 ~ 894 MHz CDMA2000 AWS : 2110 ~ 2155 MHz CDMA2000 PCS : 1930 ~ 1990 MHz
Antenna Type	Fixed Internal
HW Version	3200
SW Version	PL_2100T_GEN
Maximum Output Power to Antenna	CDMA2000 Cellular : 25.08 dBm CDMA2000 AWS : 24.87 dBm CDMA2000 PCS : 24.45 dBm
Type of Modulation	QPSK



3.2 Applied Standards:

The ANSI Standard ANSI C63.19:2006 represents performance requirements for acceptable interoperability of hearing aids with wireless communications devices. When these parameters are met, a hearing aid operates acceptably in close proximity to a wireless communications device.

The following AWF factors shall be used for the standard transmission protocols:

Standard	Technology	AWF (dB)
TIA/EIA/IS-2000	CDMA	0
TIA/EIA-136	TDMA (50 Hz)	0
J-STD-007	GSM (217)	-5
T1/T1P1/3GPP	UMTS (WCDMA)	0
iDENTM	TDMA (22 and 11 Hz)	0

Table 3.1 Articulation Weighting Factor (AWF)

Category	Telephone RF Parameters				
	Near Field	AWF	E-Field Emissions	H-Field Emissions	
< 960 MHz					
Category M1	0	631.0 – 1122.0	V/m	1.91 – 3.39	A/m
	-5	473.2 – 841.4	V/m	1.43 – 2.54	A/m
Category M2	0	354.8 – 631.0	V/m	1.07 – 1.91	A/m
	-5	266.1 – 473.2	V/m	0.80 – 1.43	A/m
Category M3	0	199.5 – 354.8	V/m	0.6 – 1.07	A/m
	-5	149.6 – 266.1	V/m	0.45 – 0.80	A/m
Category M4	0	< 199.5	V/m	< 0.60	A/m
	-5	< 149.6	V/m	< 0.45	A/m
> 960 MHz					
Category M1	0	199.5 – 354.8	V/m	0.60 – 1.07	A/m
	-5	149.6 – 266.1	V/m	0.45 – 0.80	A/m
Category M2	0	112.2 – 199.5	V/m	0.34 – 0.60	A/m
	-5	84.1 – 149.6	V/m	0.25 – 0.45	A/m
Category M3	0	63.1 – 112.2	V/m	0.19 – 0.34	A/m
	-5	47.3 – 84.1	V/m	0.14 – 0.25	A/m
Category M4	0	< 63.1	V/m	< 0.19	A/m
	-5	< 47.3	V/m	< 0.14	A/m

Table 3.2 Telephone near-field categories in linear units



3.4 Test Conditions:

3.4.1 Ambient Condition

Ambient Temperature (°C)	20-24°C
Humidity (%)	<60%

3.4.2 Test Configuration

The device was controlled by using a base station emulator R&S CMU200. Communication between the device and the emulator was established by air link.

Measurements were performed on the low, middle and high channels of all bands.

The DUT was set from the emulator to radiate maximum output power during all testings.

The worst case for CDMA2000 test modes please refer to Appendix D.



4. Hearing Aid Compliance (HAC)

4.1 Introduction

The federal communication commission (FCC) adopted ANSI C63.19 as HAC test standard.

5. HAC Measurement Setup

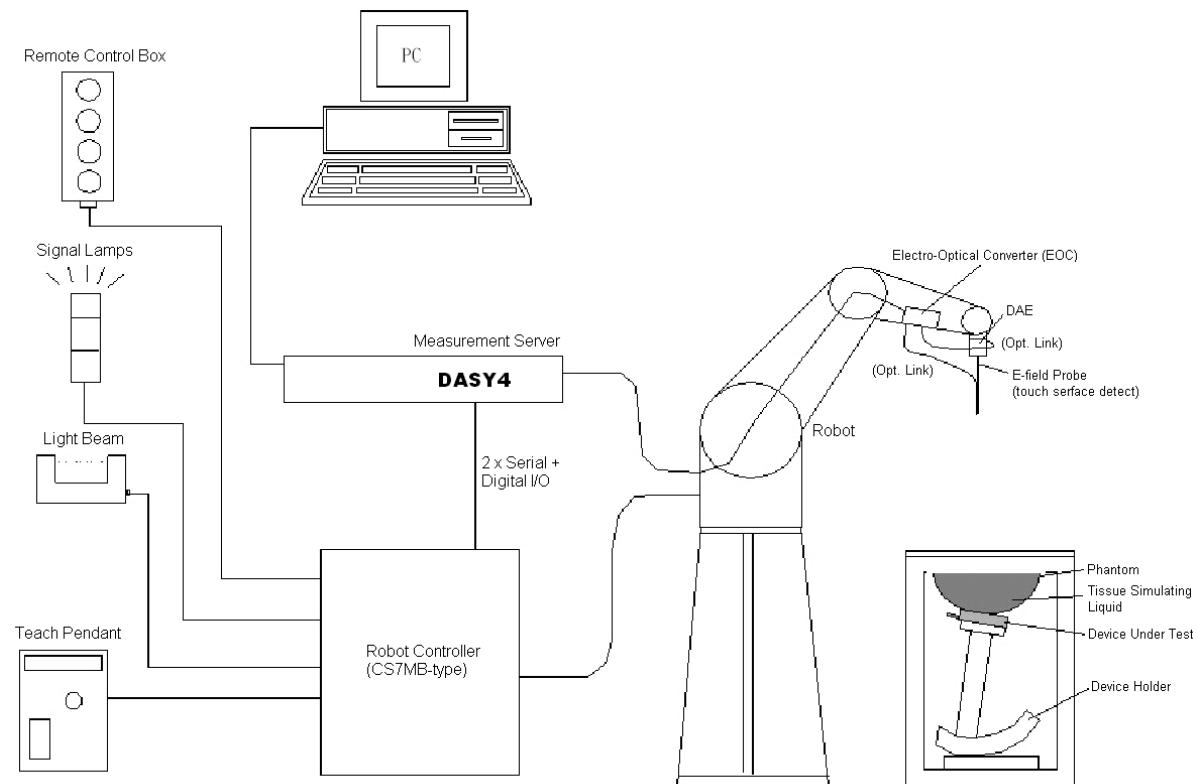


Fig. 5.1 DASY4 system



The DASY4 system for performance compliance tests is illustrated above graphically. This system consists of the following items:

- A standard high precision 6-axis robot with controller, a teach pendant and software
- A data acquisition electronic (DAE) attached to the robot arm extension
- A dosimetric probe equipped with an optical surface detector system
- The electro-optical converter (EOC) performs the conversion between optical and electrical signals
- A measurement server performs the time critical tasks such as signal filtering, control of the robot operation and fast movement interrupts.
- A probe alignment unit which improves the accuracy of the probe positioning
- A computer operating Windows XP
- DASY4 software
- Remote control with teach pendant and additional circuitry for robot safety such as warming lamps, etc.
- The SAM twin phantom
- A device holder
- Dipole for evaluating the proper functioning of the system
- Arch Phantom

Some of the components are described in details in the following sub-sections.

5.1 DASY4 E-Field and H-Field Probe System

The HAC measurement is conducted with the dosimetric probe ER3DV6 and H3DV6 (manufactured by SPEAG). The probe is specially designed and calibrated. This probe has a built in optical surface detection system to prevent from collision with DUT.

5.2 System Specification

5.2.1 ER3DV6 E-Field Probe Description

Construction	One dipole parallel, two dipoles normal to probe axis Built-in shielding against static charges
Calibration	In air from 100 MHz to 3.0 GHz (absolute accuracy $\pm 6.0\%$, $k=2$)
Frequency	100 MHz to 6 GHz;
Directivity	Linearity: ± 2.0 dB (100 MHz to 3 GHz) ± 0.2 dB in air (rotation around probe axis) ± 0.4 dB in air (rotation normal to probe axis)
Dynamic Range	2 V/m to 1000 V/m (M3 or better device readings fall well below diode compression point)
Linearity	± 0.2 dB
Dimensions	Overall length: 330 mm (Tip: 16 mm) Tip diameter: 8 mm (Body: 12 mm) Distance from probe tip to dipole centers: 2.5 mm



Fig. 5.2
E-field Free-space Probe

5.2.2 H3DV6 H-Field Probe Description

Construction	Three concentric loop sensors with 3.8 mm loop diameters Resistively loaded detector diodes for linear response Built-in shielding against static charges
Frequency	200 MHz to 3 GHz (absolute accuracy $\pm 6.0\%$, $k=2$); Output linearized
Directivity	± 0.25 dB (spherical isotropy error)
Dynamic Range	10 m A/m to 2 A/m at 1 GHz (M3 or better device readings fall well below diode compression point)
Dimensions	Overall length: 330 mm (Tip: 40 mm) Tip diameter: 6 mm (Body: 12 mm) Distance from probe tip to dipole centers: 3 mm
E-Field Interference	$< 10\%$ at 3 GHz (for plane wave)



Fig. 5.3
H-field Free-space Probe

5.2.3 Probe Tip Description

HAC field measurements take place in the close near field with high gradients. Increasing the measuring distance from the source will generally decrease the measured field values (in case of the validation dipole approx. 10% per mm).

Magnetic field sensors are measuring the integral of the H-field across their sensor area surrounded by the loop. They are calibrated in a precise, homogeneous field. When measuring a gradient field, the result will be very close to the field in the center of the loop which is equivalent to the value of a homogeneous field equivalent to the center value. But it will be different from the field at the field at the border of the loop.

Consequently, two sensors with different loop diameters – both calibrated ideally – would give different results when measuring from the edge of the probe sensor elements. The behavior for electrically small E-field sensors is equivalent. See below for distance plots from a WD which show the conservative nature of field readings at the probe element center vs. measurements at the sensor end:

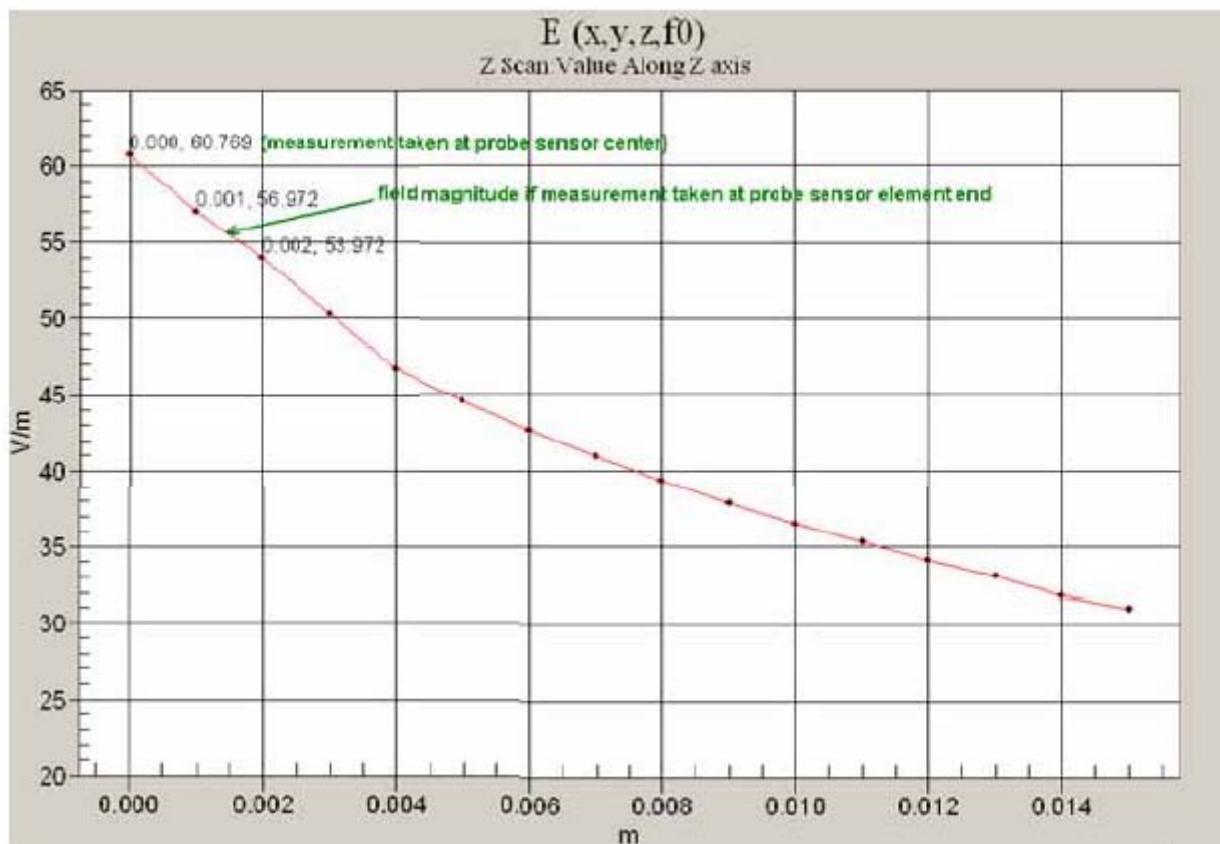


Fig. 5.4 Z-Axis Scan at maximum point above a typical wireless device for E-field

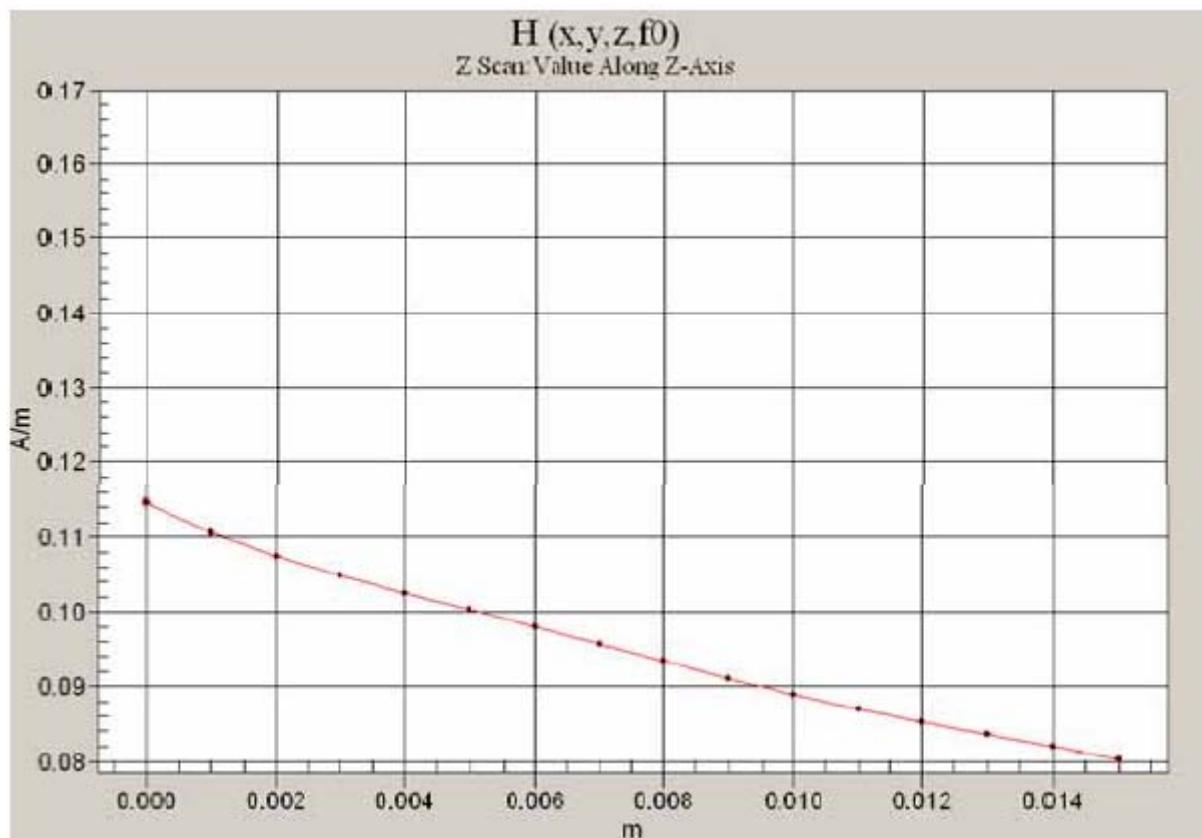


Fig. 5.5 Z-Axis Scan at maximum point above a typical wireless device for H-field

The magnetic field loops of the H3D probes are concentric, with the center 3mm from the tip for H3DV6. Their radius is 1.9 mm.

The electric field probes have a more irregular internal geometry because it is physically not possible to have the 3 orthogonal sensors situated with the same center. The effect of the different sensor centers is accounted for in the HAC uncertainty budget (“sensor displacement”). Their geometric center is at 2.5 mm from the tip, and the element ends are 1.1 mm closer to the tip.

Where:

Peak Field = Peak field (in dB V/m or dB A/m)

Raw = Raw field measurement from the measurement system (in V/m or A/m).

PMF = Probe Modulation Factor (in Linear units). See Chapter 8 of test report.



5.3 DATA Acquisition Electronics (DAE)

The data acquisition electronics (DAE4) consists of a highly sensitive electrometer-grade preamplifier with auto-zeroing, a channel and gain-switching multiplexer, a fast 16 bit AD-converter and a command decoder and control logic unit. Transmission to the measurement server is accomplished through an optical downlink for data and status information as well as an optical uplink for commands and the clock.

The mechanical probe mounting device includes two different sensor systems for frontal and sideways probe contacts. They are used for mechanical surface detection and probe collision detection.

The input impedance of the DAE4 is 200M Ohm; the inputs are symmetrical and floating. Common mode rejection is above 80dB.

5.4 Robot

The DASY4 system uses the high precision robots RX90BL type out of the newer series from Stäubli SA (France). For the 6-axis controller DASY4 system, the CS7MB robot controller version from Stäubli is used. The TX robot series have many features that are important for our application:

- High precision (repeatability 0.02 mm)
- High reliability (industrial design)
- Jerk-free straight movements
- Low ELF interference (the closed metallic construction shields against motor control fields)
- 6-axis controller

5.5 Measurement Server

The DASY4 measurement server is based on a PC/104 CPU board with 166 MHz CPU, 32 MB chipset and 64 MB RAM.

Communication with the DAE4 electronic box, the 16-bit AD-converter system for optical detection and digital I/O interface.

The measurement server performs all the real-time data evaluation for field measurements and surface detection, controls robot movements and handles safety operations.



5.6 Phone Positioner

The phone positioner shown in Fig. 5.8 is used to adjust DUT to the suitable position.



Fig. 5.6 Phone Positioner

5.6.1 Test Arch Phantom

Construction	Enables easy and well defined positioning of the phone and validation dipoles as well as simple teaching of the robot.
Dimensions	370 x 370 x 370 mm

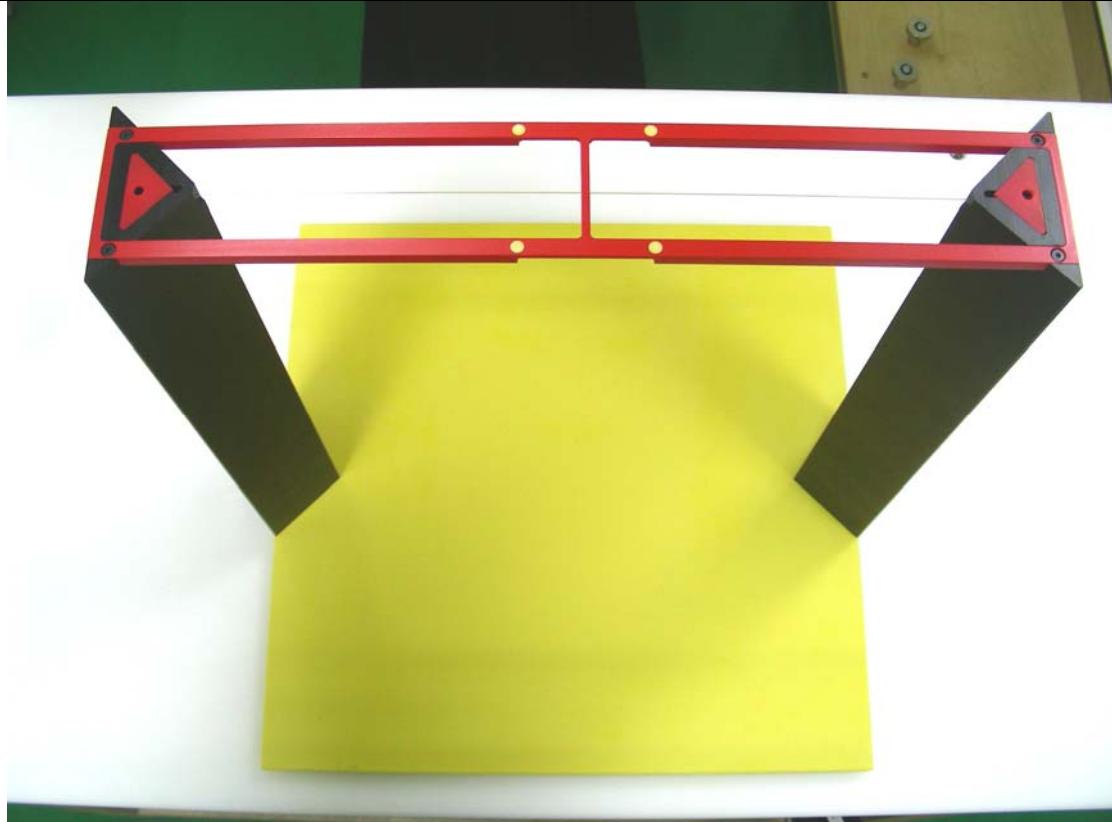


Fig. 5.7 Test Arch Phantom



5.7 Data Storage and Evaluation

5.7.1 Data Storage

The DASY4 software stores the assessed data from the data acquisition electronics as raw data (in microvolt readings from the probe sensors), together with all the necessary software parameters for the data evaluation (probe calibration data, and device frequency and modulation data) in measurement files with the extension .DA4. The postprocessing software evaluates the desired unit and format for output each time the data is visualized or exported. This allows verification of the complete software setup even after the measurement and allows correction of erroneous parameter settings.

5.7.2 Data Evaluation

The DASY4 postprocessing software (SEMCAD) automatically executes the following procedures to calculate the field units from the microvolt readings at the probe connector. The parameters used in the evaluation are stored in the configuration modules of the software :

Probe parameters :	- Sensitivity	Norm i , a $_{i0}$, a $_{i1}$, a $_{i2}$
	- Conversion factor	ConvF i
	- Diode compression point	dcp i
Device parameters :	- Frequency	f
	- Crest factor	cf
Media parameters :	- Conductivity	σ
	- Density	ρ

These parameters must be set correctly in the software. They can be found in the component documents or they can be imported into the software from the configuration files issued for the DASY4 components. In the direct measuring mode of the multimeter option, the parameters of the actual system setup are used. In the scan visualization and export modes, the parameters stored in the corresponding document files are used.

The first step of the evaluation is a linearization of the filtered input signal to account for the compression characteristics of the detector diode. The compensation depends on the input signal, the diode type and the DC-transmission factor from the diode to the evaluation electronics. If the exciting field is pulsed, the crest factor of the signal must be known to correctly compensate for peak power. The formula for each channel can be given as :

$$V_i = U_i + U_i^2 \cdot \frac{cf}{dcp_i}$$

with

V_i = compensated signal of channel i ($i = x, y, z$)

U_i = input signal of channel i ($i = x, y, z$)

cf = crest factor of exciting field (DASY parameter)

dcp_i = diode compression point (DASY parameter)

From the compensated input signals, the primary field data for each channel can be evaluated :



$$\text{E-field probes : } E_i = \sqrt{\frac{V_i}{Norm_i ConvF}}$$

$$\text{H-field probes : } H_i = \sqrt{V_i} \frac{a_{i0} + a_{i1}f + a_{i2}f^2}{f}$$

with V_i = compensated signal of channel i ($i = x, y, z$)

$Norm_i$ = sensor sensitivity of channel i ($i = x, y, z$)

μ V/(V/m)2 for E-field Probes

$ConvF$ = sensitivity enhancement in solution

a_{ij} = sensor sensitivity factors for H-field probes

f = carrier frequency [GHz]

E_i = electric field strength of channel i in V/m

H_i = magnetic field strength of channel i in A/m

The RSS value of the field components gives the total field strength (Hermitian magnitude) :

$$E_{tot} = \sqrt{E_x^2 + E_y^2 + E_z^2}$$

The primary field data are used to calculate the derived field units.

The power flow density is calculated assuming the excitation field to be a free space field.

$$P_{pwe} = \frac{E_{tot}^2}{3770} \quad \text{or} \quad P_{pwe} = H_{tot}^2 \cdot 37.7$$

with P_{pwe} = equivalent power density of a plane wave in mW/cm²

E_{tot} = total electric field strength in V/m

H_{tot} = total magnetic field strength in A/m

The measurement/integration time per point, as specified by the system manufacturer is >500 ms.

The signal response time is evaluated as the time required by the system to reach 90% of the expected final value after an on/off switch of the power source with an integration time of 500 ms and a probe response time of <5 ms. In the current implementation, DASY4 waits longer than 100 ms after having reached the grid point before starting a measurement, i.e., the response time uncertainty is negligible.

If the device under test does not emit a CW signal, the integration time applied to measure the electric field at a specific point may introduce additional uncertainties due to the discretization. The tolerances for the different systems had the worst-case of 2.6%.



5.8 Test Equipment List

Manufacturer	Name of Equipment	Type/Model	Serial Number	Calibration	
				Last Cal.	Due Date
SPEAG	Isotropic E-Filed Probe	ER3DV6	2358	Jan. 28, 2008	Jan. 27, 2009
SPEAG	Isotropic H-Filed Probe	H3DV6	6184	Jan. 28, 2008	Jan. 27, 2009
SPEAG	835MHz Calibration Dipole	CD835V3	1017	Jul. 12, 2007	Jul. 12, 2008
SPEAG	1880MHz Calibration Dipole	CD1880V3	1036	Jul. 12, 2007	Jul. 12, 2008
SPEAG	Data Acquisition Electronics	DAE3	577	Nov. 16, 2007	Nov. 16, 2008
SPEAG	Phone Positoiner	N/A	N/A	NCR	NCR
SPEAG	Test Arch Phantom	N/A	N/A	NCR	NCR
SPEAG	Phantom	QD 000 P40 C	TP-1150	NCR	NCR
SPEAG	Robot	Staubli RX90BL	F03/5W15A1/A/01	NCR	NCR
SPEAG	Software	DASY4 V4.7 Build 55	N/A	NCR	NCR
SPEAG	Software	SEMCAD V1.8 Build 176	N/A	NCR	NCR
SPEAG	Measurement Server	SE UMS 001 BA	1021	NCR	NCR
Agilent	Dual Directional Coupler	778D	50422	NCR	NCR
Agilent	Power Amplifier	8449B	3008A01917	NCR	NCR
Agilent	Power Meter	E4416A	GB41292344	Feb. 21, 2008	Feb. 20, 2009
Agilent	Power Sensor	E9327A	US40441548	Feb. 21, 2008	Feb. 20, 2009
Agilent	Wireless COM. Test Set	E5515C	GB46311322	Dec. 22, 2006	Dec. 22, 2008
R&S	Universal Radio Communication Tester	CMU200	103937	Oct. 19, 2007	Oct. 19, 2008

Table 5.6 Test Equipment List



6. Uncertainty Assessment

The component of uncertainty may generally be categorized according to the methods used to evaluate them. The evaluation of uncertainty by the statistical analysis of a series of observations is termed a Type A evaluation of uncertainty. The evaluation of uncertainty by means other than the statistical analysis of a series of observation is termed a Type B evaluation of uncertainty. Each component of uncertainty, however evaluated, is represented by an estimated standard deviation, termed standard uncertainty, which is determined by the positive square root of the estimated variance.

A Type A evaluation of standard uncertainty may be based on any valid statistical method for treating data. This includes calculating the standard deviation of the mean of a series of independent observations; using the method of least squares to fit a curve to the data in order to estimate the parameter of the curve and their standard deviations; or carrying out an analysis of variance in order to identify and quantify random effects in certain kinds of measurement.

A type B evaluation of standard uncertainty is typically based on scientific judgment using all of the relevant information available. These may include previous measurement data, experience and knowledge of the behavior and properties of relevant materials and instruments, manufacturer's specification, data provided in calibration reports and uncertainties assigned to reference data taken from handbooks. Broadly speaking, the uncertainty is either obtained from an outdoor source or obtained from an assumed distribution, such as the normal distribution, rectangular or triangular distributions indicated in Table 7.1

Uncertainty Distributions	Normal	Rectangular	Triangular	U-shape
Multiplying factor ^(a)	$1/k$ (b)	$1/\sqrt{3}$	$1/\sqrt{6}$	$1/\sqrt{2}$

(a) standard uncertainty is determined as the product of the multiplying factor and the estimated range of variations in the measured quantity

(b) k is the coverage factor

Table 6.1

The combined standard uncertainty of the measurement result represents the estimated standard deviation of the result. It is obtained by combining the individual standard uncertainties of both Type A and Type B evaluation using the usual "root-sum-squares" (RSS) methods of combining standard deviations by taking the positive square root of the estimated variances.

Expanded uncertainty is a measure of uncertainty that defines an interval about the measurement result within which the measured value is confidently believed to lie. It is obtained by multiplying the combined standard uncertainty by a coverage factor. Typically, the coverage factor ranges from 2 to 3. Using a coverage factor allows the true value of a measured quantity to be specified with a defined probability within the specified uncertainty range. For purpose of this document, a coverage factor two is used, which corresponds to confidence interval of about 95 %. The DASY4 uncertainty Budget is showed in Table 6.2.



Error Description	Uncertainty Value (\pm %)	Probability Distribution	Divisor	(Ci) E	(Ci) H	Std. Unc. E	Std. Unc. H
Measurement System							
Probe Calibration	± 5.1	Normal	1	1	1	± 5.1	± 5.1
Axial Isotropy	± 4.7	Rectangular	$\sqrt{3}$	1	1	± 2.7	± 2.7
Sensor Displacement	± 16.5	Rectangular	$\sqrt{3}$	1	0.145	± 9.5	± 1.4
Boundary Effect	± 2.4	Rectangular	$\sqrt{3}$	1	1	± 1.4	± 1.4
Linearity	± 4.7	Rectangular	$\sqrt{3}$	1	1	± 2.7	± 2.7
Scaling to Peak Envelope Power	± 2.0	Rectangular	$\sqrt{3}$	1	1	± 1.2	± 1.2
System Detection Limit	± 1.0	Rectangular	$\sqrt{3}$	1	1	± 0.6	± 0.6
Readout Electronics	± 0.3	Normal	1	1	1	± 0.3	± 0.3
Response Time	± 0.8	Rectangular	$\sqrt{3}$	1	1	± 0.5	± 0.5
Integration Time	± 2.6	Rectangular	$\sqrt{3}$	1	1	± 1.5	± 1.5
RF Ambient Conditions	± 3.0	Rectangular	$\sqrt{3}$	1	1	± 1.7	± 1.7
RF Reflections	± 12.0	Rectangular	$\sqrt{3}$	1	1	± 6.9	± 6.9
Probe Positioner	± 1.2	Rectangular	$\sqrt{3}$	1	0.67	± 0.7	± 0.5
Probe Positioning	± 4.7	Rectangular	$\sqrt{3}$	1	0.67	± 2.7	± 1.8
Extrap. and Interpolation	± 1.0	Rectangular	$\sqrt{3}$	1	1	± 0.6	± 0.6
Test Sample Related							
Device Positioning Vertical	± 4.7	Rectangular	$\sqrt{3}$	1	0.67	± 2.7	± 1.8
Device Positioning Lateral	± 1.0	Rectangular	$\sqrt{3}$	1	1	± 0.6	± 0.6
Device Holder and Phantom	± 2.4	Rectangular	$\sqrt{3}$	1	1	± 1.4	± 1.4
Power Drift	± 5.0	Rectangular	$\sqrt{3}$	1	1	± 2.9	± 2.9
Phantom and Setup Related							
Phantom Thickness	± 2.4	Rectangular	$\sqrt{3}$	1	0.67	± 1.4	± 0.9
Combined Standard Uncertainty							
Coverage Factor for 95 %		K=2				± 14.7	± 10.9
Expanded uncertainty (Coverage factor = 2)						± 29.4	± 21.8

Table 6.2 Uncertainty Budget of DASY4

7. HAC Measurement Evaluation

Each DASY4 system is equipped with one or more system validation kits. These units, together with the predefined measurement procedures within the DASY4 software, enable the user to conduct the system performance check and system validation. System validation kit includes a dipole, tripod holder to fix it underneath the test Arch and a corresponding distance holder.

7.1 Purpose of System Performance check

The system performance check verifies that the system operates within its specifications. System and operator errors can be detected and corrected. It is recommended that the system performance check be performed prior to any usage of the system in order to guarantee reproducible results. The system performance check uses normal HAC measurements in a simplified setup with a well characterized source. This setup was selected to give a high sensitivity to all parameters that might fail or vary over time. The system check does not intend to replace the calibration of the components, but indicates situations where the system uncertainty is exceeded due to drift or failure.

7.2 System Setup

In the simplified setup for system evaluation, the DUT is replaced by a calibrated dipole and the power source is replaced by a continuous wave which comes from a signal generator at frequency 835 and 1880 MHz. The calibrated dipole must be placed beneath the flat phantom section of the ARC with the correct distance holder. The equipment setup is shown below:

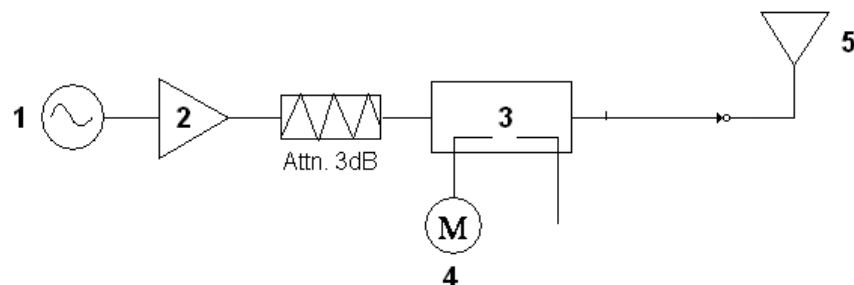


Fig. 7.1 System Setup of System Evaluation

1. Signal Generator
2. Amplifier
3. Directional Coupler
4. Power Meter
5. 835 or 1880 MHz Dipole

The output power on dipole port must be calibrated to 20dBm (100mW) before dipole is connected.

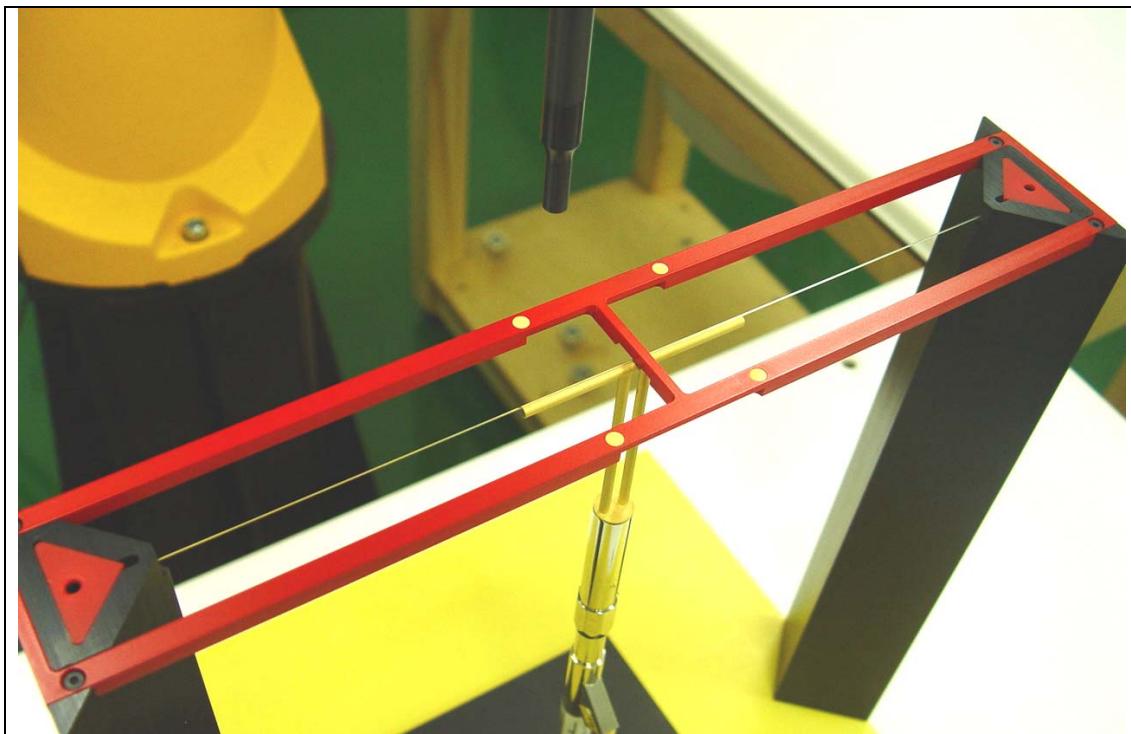


Fig 7.2 Dipole Setup



7.3 Validation Results

Frequency (MHz)	Input Power (dBm)	E-field Result (V/m)	Target Field (V/m)	Deviation (%)
835	20.0	175.55	167.1	5.06
1880	20.0	148.10	138.9	6.62
<hr/>				
Frequency (MHz)	Input Power (dBm)	H-field Result (A/m)	Target Field (A/m)	Deviation (%)
835	20.0	0.455	0.453	0.44
1880	20.0	0.500	0.471	6.16

Table 7.1 System Validation

Remark: Deviation = ((E or H-field Result) - (Target field)) / (Target field) * 100%

The table above indicates the system performance check can meet the variation criterion, $\pm 25\%$.

8. RF Field Probe Modulation Factor

A calibration shall be made of the modulation response of the probe and its instrumentation chain. This calibration shall be performed with the field probe, attached to the instrumentation that is to be used with it during the measurement. The response of the probe system to a CW field at the frequency(s) of interest is compared to its response to a modulated signal with equal peak amplitude. The field level of the test signals shall be more than 10 dB above the ambient level and the noise floor of the instrumentation being used. The ratio of the CW reading to that taken with a modulated field shall be applied to the readings taken of modulated fields of the specified type.

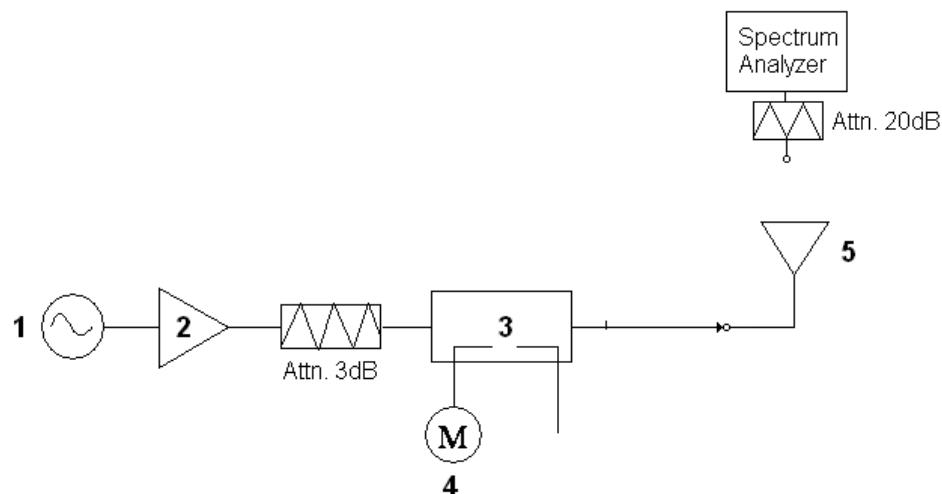


Fig. 8.1 System Calibration

This was done using the following procedure:

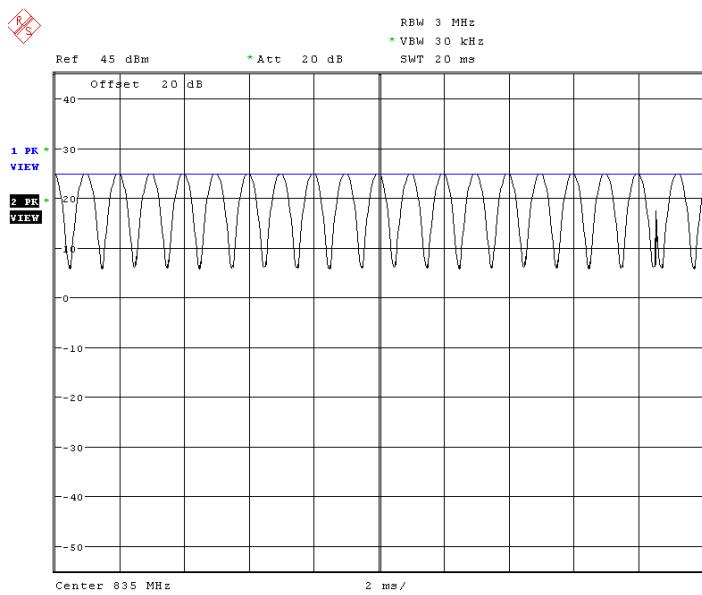
1. Fixing the probe in a set location relative to a field generating device.
2. Illuminate the probe with a CW signal at the intended measurement frequency.
3. Record the reading of the probe measurement system of the CW signal.
4. Determine the level of the CW signal being used to drive the field generating device.
5. Substitute a signal using the same modulation as that used by the intended WD for the CW signal.
6. Set the peak amplitude during transmission of the modulated signal to equal the amplitude of the CW signal.
7. Record the reading of the probe measurement system of the modulated signal.
8. The ratio of the CW to modulated signal reading is the modulation factor.
9. Repeat 2~8 steps at intended measurement frequency for both E and H field probe.



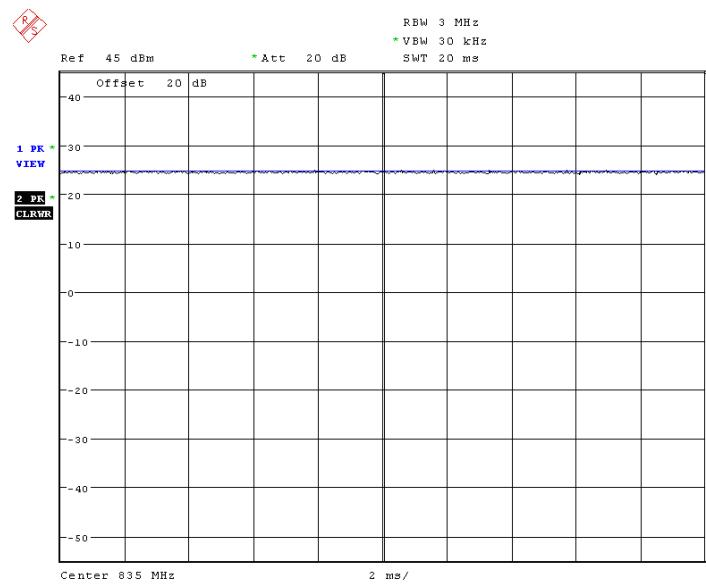
PMF Measurement Summary:

Frequency	Functions	E-field	H-field	PMF	
		V/m	A/m	E-field	H-field
835MHz	CW	185.5	0.802	-	-
835MHz	AM	117.8	0.515	1.57	1.56
835MHz	CDMA	191.4	0.817	0.97	0.98
835MHz	CMDA 1/8	66.3	0.287	2.80	2.79
1880MHz	CW	176.4	0.793	-	-
1880MHz	AM	114.5	0.487	1.54	1.63
1880MHz	CDMA	179.9	0.801	0.98	0.99
1880MHz	CMDA 1/8	63.2	0.283	2.79	2.80

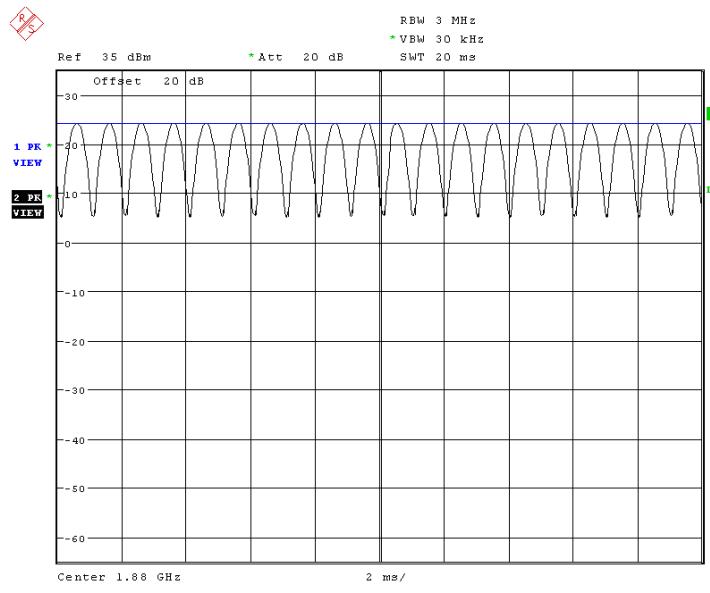
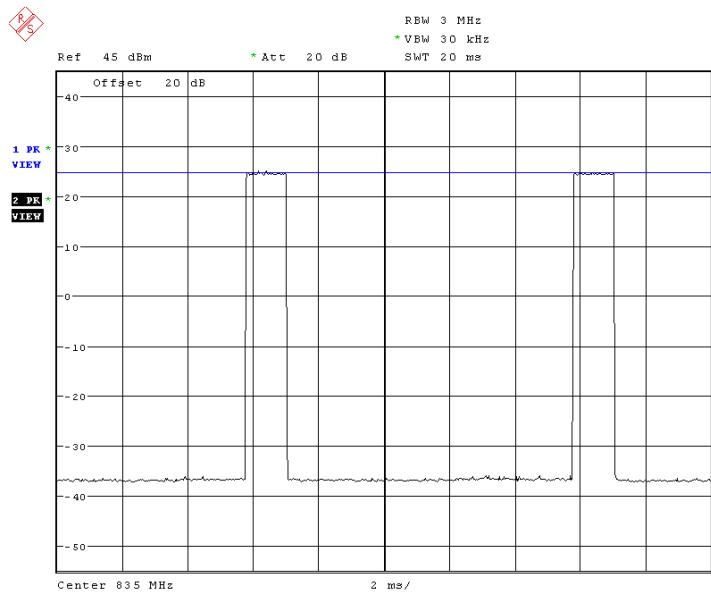
Zero span Spectrum Plots for RF Field Probe Modulation Factor



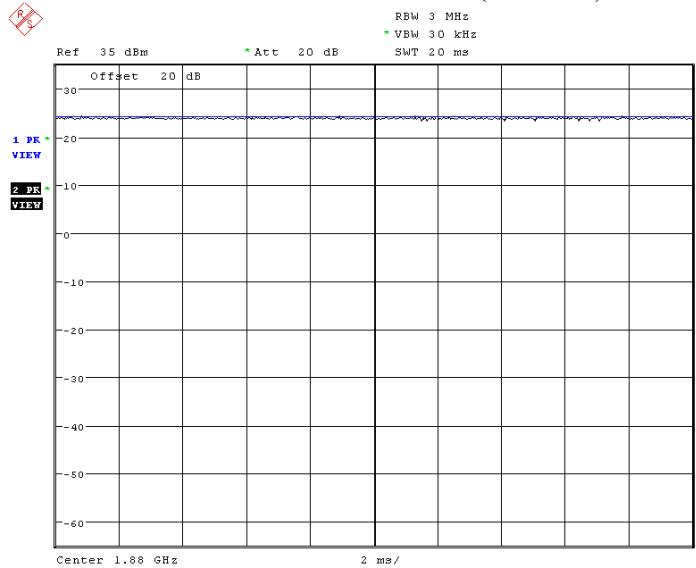
835MHz - CW and 80% AM



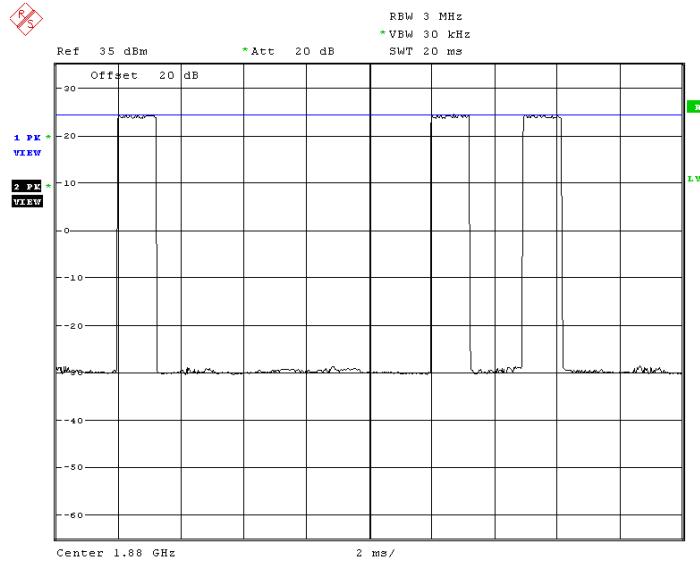
835MHz - CW and CDMA (Full Rate)



835MHz - CW and CDMA (1/8 Rate)



1880MHz - CW and 80% AM



1880MHz - CW and CDMA (Full Rate)

1880MHz - CW and CDMA (1/8 Rate)

9. Description for DUT Testing Position

The DUT was put on device holder and adjusted to the accurate and reliable position.

Figure 9.1 illustrate the references and reference plane that shall be used in a typical DUT emissions measurement. The principle of this section is applied to DUT with similar geometry.

- The grid is 5 cm by 5 cm area that is divided into 9 evenly sized blocks or sub-grids.
- The grid is centered on the audio frequency output transducer of the DUT.
- The grid is in a reference plane, which is defined as the planar area that contains the highest point in the area of the phone that normally rests against the user's ear. It is parallel to the centerline of the receiver area of the phone and is defined by the points of the receiver-end of the DUT handset, which, in normal handset use, rest against the ear.
- The measurement plane is parallel to, and 1.0 cm in front of, the reference plane.



Figure 9.1: A typical DUT reference and plane for HAC measurements

Setup photographs please refer to Appendix E.



10. RF Emissions Test Procedure

The following illustrate a typical RF emissions test scan over a wireless communications device:

1. Proper operation of the field probe, probe measurement system, other instrumentation, and the positioning system was confirmed.
2. DUT is positioned in its intended test position, acoustic output point of the device perpendicular to the field probe.
3. The DUT operation for maximum rated RF output power was configured and confirmed with the base station simulator, at the test channel and other normal operating parameters as intended for the test. The battery was ensured to be fully charged before each test.
4. The center sub-grid was centered over the center of the acoustic output (also audio band magnetic output, if applicable). The DUT audio output was positioned tangent (as physically possible) to the measurement plane.
5. A surface calibration was performed before each setup change to ensure repeatable spacing and proper maintenance of the measurement plane using the test Arch.
6. The measurement system measured the field strength at the reference location.
7. Measurements at 5 mm increments in the 5 x 5 cm region were performed and recorded. A 360°C rotation about the azimuth axis at the maximum interpolated position was measured. For the worst-case condition, the peak reading from this rotation was used in re-evaluating the HAC category.
8. The system performed a drift evaluation by measuring the field at the reference location.
9. Steps 1-8 were done for both the E and H-Field measurements.



11. HAC Test Results

11.1 E-Field Emission

Mode	Chan.	Freq. (MHz)	Modulation type	PMF	Conducted Power (dBm)	Power Drift (dB)	Peak Field (V/m)	Backlight	M-Rating
CDMA2000 Cellular	1013	824.70	QPSK	0.97	24.85	-0.014	121.6	Off	M4
	384	836.52	QPSK	0.97	24.75	-0.138	123.7	Off	M4
	777	848.31	QPSK	0.97	24.85	-0.014	126.1	Off	M4
	777	848.31	QPSK	0.97	24.85	-0.011	127.4	On	M4
CDMA2000 AWS	25	1711.25	QPSK	0.98	24.76	0.209	65.5	Off	M3
	25	1711.25	QPSK	0.98	24.76	0.106	66.1	On	M3
	425	1731.25	QPSK	0.98	24.56	-0.106	62.4	Off	M4
	875	1753.75	QPSK	0.98	24.45	-0.104	63.6	Off	M3
CDMA2000 PCS	25	1851.25	QPSK	0.98	23.74	-0.107	59.2	Off	M4
	600	1880.00	QPSK	0.98	24.20	0.059	59.6	Off	M4
	600	1880.00	QPSK	0.98	24.20	-0.146	58.9	On	M4
	1175	1908.75	QPSK	0.98	24.14	0.088	57.2	Off	M4

11.2 H-Field Emission

Mode	Chan.	Freq. (MHz)	Modulation type	PMF	Conducted Power (dBm)	Power Drift (dB)	Peak Field (A/m)	Backlight	M-Rating
CDMA2000 Cellular	1013	824.70	QPSK	0.98	24.85	0.089	0.107	Off	M4
	384	836.52	QPSK	0.98	24.75	0.036	0.112	Off	M4
	777	848.31	QPSK	0.98	24.85	0.005	0.118	Off	M4
	777	848.31	QPSK	0.98	24.85	0.087	0.12	On	M4
CDMA2000 AWS	25	1711.25	QPSK	0.99	24.76	0.228	0.156	Off	M4
	425	1731.25	QPSK	0.99	24.56	-0.182	0.157	Off	M4
	425	1731.25	QPSK	0.99	24.56	-0.172	0.139	On	M4
	875	1753.75	QPSK	0.99	24.45	-0.011	0.156	Off	M4
CDMA2000 PCS	25	1851.25	QPSK	0.99	23.74	0.043	0.153	Off	M4
	600	1880.00	QPSK	0.99	24.20	-0.041	0.157	Off	M4
	600	1880.00	QPSK	0.99	24.20	-0.045	0.167	On	M4
	1175	1908.75	QPSK	0.99	24.14	0.125	0.141	Off	M4

Remark :

1. The device was chosen to be tested in the worst case peak E-Field condition under RC3/SO55 Full Rate.
2. The HAC mode of EUT is turn on and output power is adjusted to maximum level during RF Emission testing.
3. Test Engineer : Jason Wang and Eric Huang



12. References

- [1] ANSI C63.19 2006, "American National Standard for Methods of Measurement of Compatibility between Wireless Communications Devices and Hearing Aids"
- [2] DASY4 System Hand book.