


Power Density Evaluation Report

FCC ID : PU5-TP00139AM
Equipment : Notebook Computer
Model Name : TP00139A
Applicant : Wistron Corporation
21F, No. 88, Sec. 1, Hsin Tai Wu Rd.,
Hsichih Dist, New Taipei City 221, Taiwan
Standard : FCC 47 CFR Part 2 (2.1093)

We, SPORTON INTERNATIONAL INC have been evaluated in accordance with 47 CFR Part 2.1093 for the device and pass the limit.

The product was received on Jan. 06, 2022 and testing was started from Jan. 31, 2022 and completed on Mar. 11, 2022. We, SPORTON INTERNATIONAL INC have been evaluated in accordance with 47 CFR Part 2.1093 for the device and pass the limit.

The test results in this report apply exclusively to the tested model / sample. Without written approval of SPORTON INTERNATIONAL INC. Laboratory, the test report shall not be reproduced except in full.



Approved by: Cona Huang / Deputy Manager



Sporton International Inc. EMC & Wireless Communications Laboratory



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History of this test report

Report No.	Version	Description	Issued Date
FA1D1645	01	Initial issue of report	Mar. 13, 2022



1. Summary

The maximum measured average power density found during testing for Wistron Corporation, Notebook Computer, are as follows.

Standalone transmission				Simultaneous transmission with other transmitters
RF Transmitter		Measured PD (mW/cm ²)	Reported PD (mW/cm ²)	Summation of Exposure Ratio
5G FR2	n260	6.82	9.0	0.961
	n261	7.61	9.0	
Result		PASS		

Reviewed by: Jason Wang

Report Producer: Carlie Tsai

2. Guidance Applied

The Power Density testing specification, method, and procedure for this device is in accordance with the following standards:

- FCC 47 CFR Part 2.1091
- FCC 47 CFR Part 2.1093
- FCC KDB 865664 D02 SAR Reporting v01r02
- FCC KDB 447498 D01 General RF Exposure Guidance v06
- FCC KDB 648474 D04 SAR Evaluation Considerations for Wireless Handsets v01r03
- TCBC workshop notes
- IEC Draft TR 63170



3. Equipment Under Test (EUT) Information

3.1 General Information

Product Feature & Specification	
Equipment Name	Notebook Computer
FCC ID	PU5-TP00139AM
Wireless Technology and Frequency Range	WCDMA Band II: 1850 MHz ~ 1910 MHz WCDMA Band IV: 1710 MHz ~ 1755 MHz WCDMA Band V: 824 MHz ~ 849 MHz LTE Band 2: 1850 MHz ~ 1910 MHz LTE Band 4: 1710 MHz ~ 1755 MHz LTE Band 5: 824 MHz ~ 849 MHz LTE Band 7: 2500 MHz ~ 2570 MHz LTE Band 12: 699 MHz ~ 716 MHz LTE Band 13: 777 MHz ~ 787 MHz LTE Band 14: 788 MHz ~ 798 MHz LTE Band 17: 704 MHz ~ 716 MHz LTE Band 25: 1850 MHz ~ 1915 MHz LTE Band 26: 814 MHz ~ 849 MHz LTE Band 30: 2305 MHz ~ 2315 MHz LTE Band 38: 2570 MHz ~ 2620 MHz LTE Band 41: 2496 MHz ~ 2690 MHz LTE Band 42: 3550 MHz ~ 3600 MHz LTE Band 48: 3550 MHz ~ 3700 MHz LTE Band 66: 1710 MHz ~ 1780 MHz LTE Band 71: 663 MHz ~ 698 MHz 5G NR n2 : 1850 MHz ~ 1910 MHz 5G NR n5 : 824 MHz ~ 849 MHz 5G NR n7 : 2500 MHz ~ 2570 MHz 5G NR n12 : 699 MHz ~ 716 MHz 5G NR n25 : 1850 MHz ~ 1915 MHz 5G NR n38 : 2570 MHz ~ 2620 MHz 5G NR n41 : 2496 MHz ~ 2690 MHz 5G NR n66 : 1710 MHz ~ 1780 MHz 5G NR n71 : 663 MHz ~ 698 MHz 5G NR n77: 3700 MHz ~ 3980 MHz 5G NR n260 : 37 GHz~40 GHz 5G NR n261 : 27.5 GHz~28.35 GHz WLAN 2.4 GHz Band: 2400 MHz ~ 2483.5 MHz WLAN 5.2 GHz Band: 5150 MHz ~ 5250 MHz WLAN 5.3 GHz Band: 5250 MHz ~ 5350 MHz WLAN 5.6 GHz Band: 5470 MHz ~ 5725 MHz WLAN 5.8 GHz Band: 5725 MHz ~ 5850 MHz WLAN 6E: 5925 MHz ~ 6425 MHz, 6425 MHz ~ 6525 MHz, 6525 MHz ~ 6875 MHz, 6875 MHz ~ 7125 MHz Bluetooth: 2400 MHz ~ 2483.5 MHz
Mode	RMC 12.2Kbps HSDPA HSUPA DC-HSDPA LTE: QPSK, 16QAM, 64QAM, 256QAM 5G NR: DFT-s-OFDM/CP-OFDM, Pi/2 BPSK/QPSK/16QAM/64QAM/256QAM WLAN: 802.11a/b/g/n/ac/ax HT20/HT40/VHT20/VHT40/VHT80/VHT160/HE20/HE40/HE80/HE160 Bluetooth BR/EDR/LE

4. RF Exposure Limits

4.1 Uncontrolled Environment

Uncontrolled Environments are defined as locations where there is the exposure of individuals who have no knowledge or control of their exposure. The general population/uncontrolled exposure limits are applicable to situations in which the general public may be exposed or in which persons who are exposed as a consequence of their employment may not be made fully aware of the potential for exposure or cannot exercise control over their exposure. Members of the general public would come under this category when exposure is not employment-related; for example, in the case of a wireless transmitter that exposes persons in its vicinity.

4.2 Controlled Environment

Controlled Environments are defined as locations where there is exposure that may be incurred by persons who are aware of the potential for exposure, (i.e. as a result of employment or occupation). In general, occupational/controlled exposure limits are applicable to situations in which persons are exposed as a consequence of their employment, who have been made fully aware of the potential for exposure and can exercise control over their exposure. The exposure category is also applicable when the exposure is of a transient nature due to incidental passage through a location where the exposure levels may be higher than the general population/uncontrolled limits, but the exposed person is fully aware of the potential for exposure and can exercise control over his or her exposure by leaving the area or by some other appropriate means.

The criteria listed in Table 1 shall be used to evaluate the environmental impact of human exposure above 6GHz to radio frequency (RF) radiation as specified in §1.1310.

General Population Basic restriction for power density for frequencies between 1.5GHz and 100 GHz is $1.0 \text{ mW/cm}^2 = 10 \text{ W/m}^2$

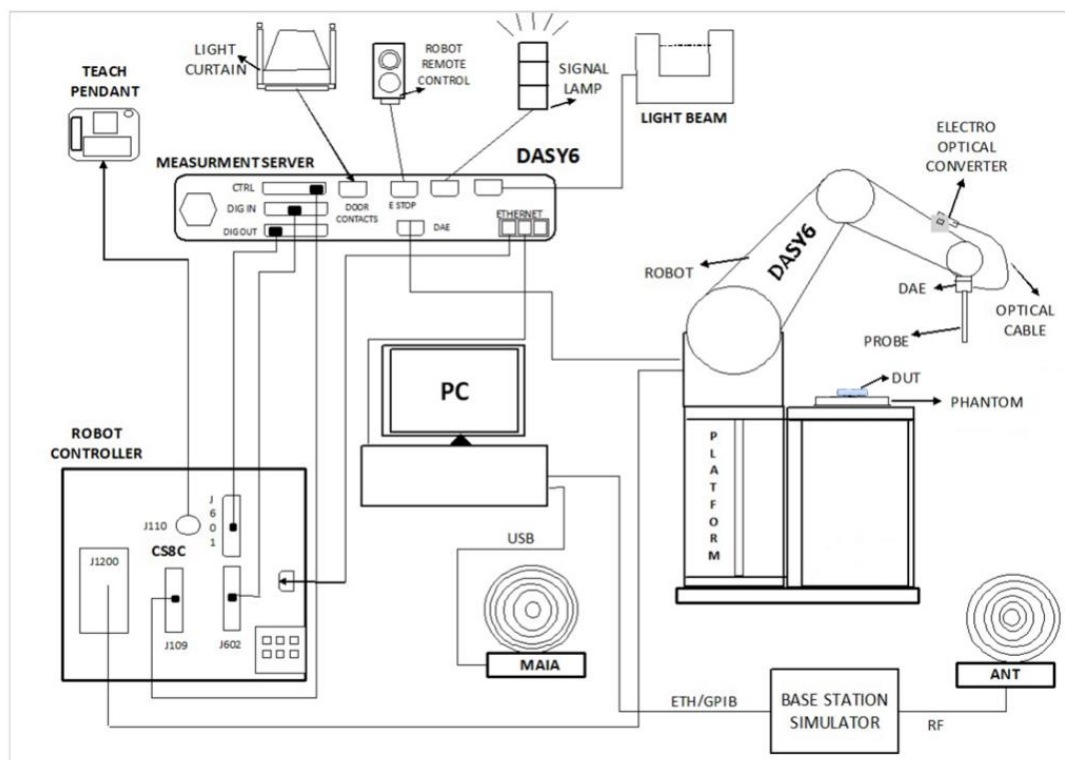
Frequency range (MHz)	Electric field strength (V/m)	Magnetic field strength (A/m)	Power density (mW/cm ²)	Averaging time (minutes)
(A) Limits for Occupational/Controlled Exposures				
0.3-3.0	614	1.63	*(100)	6
3.0-30	1842/f	4.89/f	*(900/f ²)	6
30-300	61.4	0.163	1.0	6
300-1500			f/300	6
1500-100,000			5	6
(B) Limits for General Population/Uncontrolled Exposure				
0.3-1.34	614	1.63	*(100)	30
1.34-30	824/f	2.19/f	*(180/f ²)	30
30-300	27.5	0.073	0.2	30
300-1500			f/1500	30
1500-100,000			1.0	30

Table 1

5. System Description and Setup

The system to be used for the near field power density measurement

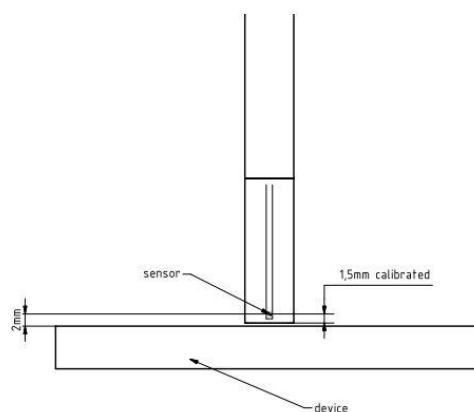
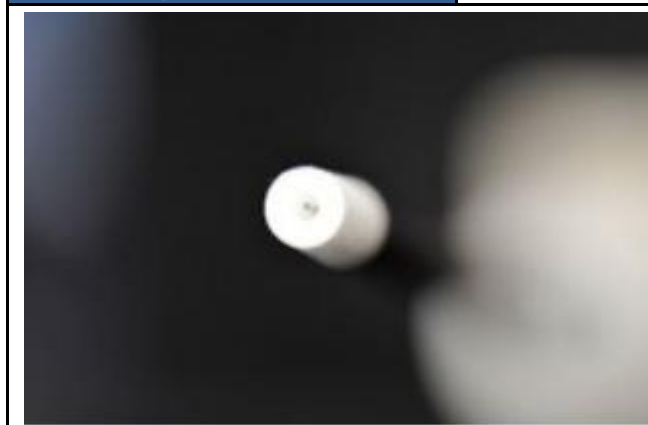
- SPEAG DASY6 system
- SPEAG cDASY6 5G module software
- EUmWVx probe
- 5G Phantom cover



5.1 EUmmWave Probe / E-Field 5G Probe

The probe design allows measurements at distances as small as 2 mm from the sensors to the surface of the device under test (DUT). The typical sensor to probe tip distance is 1.5 mm.

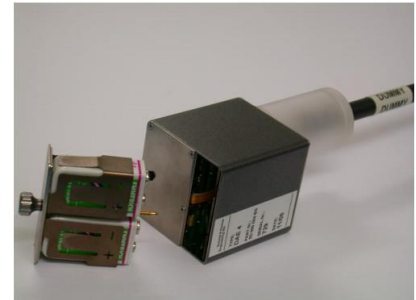
Frequency	750 MHz – 110 GHz
Probe Overall Length	320 mm
Probe Body Diameter	8.0 mm
Tip Length	23.0 mm
Tip Diameter	8.0 mm
Probe's two dipoles length	0.9 mm – Diode loaded
Dynamic Range	< 20 V/m - 10000 V/m with PRE-10 (min < 50 V/m - 3000 V/m)
Position Precision	< 0.2 mm
Distance between diode sensors and probe's tip	1.5 mm
Minimum Mechanical separation between probe tip and a Surface	0.5 mm
Applications	E-field measurements of 5G devices and other mm-wave transmitters operating above 10GHz in < 2 mm distance from device (free-space) Power density, H-field and far-field analysis using total field reconstruction.
Compatibility	cDASY6 + 5G-Module SW1.0 and higher



5.2 Data Acquisition Electronics (DAE)

The data acquisition electronics (DAE) consists of a highly sensitive electrometer-grade preamplifier with auto-zeroing, a channel and gain-switching multiplexer, a fast 16 bit AD-converter and a command decoder and control logic unit. Transmission to the measurement server is accomplished through an optical downlink for data and status information as well as an optical uplink for commands and the clock.

The input impedance of the DAE is 200 MOhm; the inputs are symmetrical and floating. Common mode rejection is above 80 dB.



5.3 Scan configuration

Fine-resolution scans on 2 different planes are performed to reconstruct the E- and H-fields as well as the power density; the z-distance between the 2 planes is set to $\lambda/4$.

The (x, y) grid step is also set $\lambda/4$, the grid extent is set to sufficiently large to identify the field pattern and the peak.

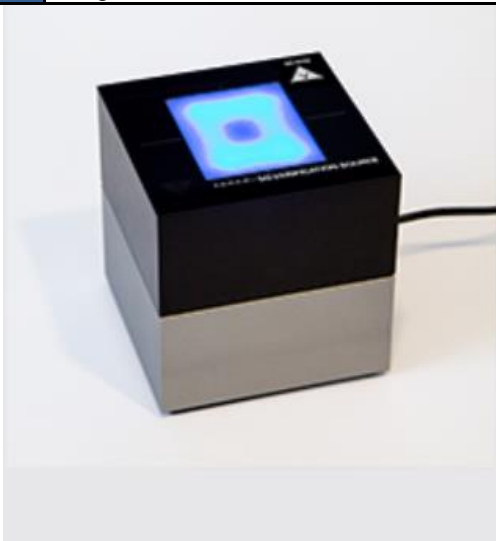
6. Test Equipment List

Manufacturer	Name of Equipment	Type/Model	Serial Number	Calibration	
				Last Cal.	Due Date
SPEAG	5G Verification Source	30GHz	1007	Nov. 15, 2021	Nov. 14, 2022
SPEAG	EUmmWV Probe Tip Protection	EUmmWV4	9441	Nov. 24, 2021	Nov. 23, 2022
SPEAG	Data Acquisition Electronics	DAE4	778	May. 21, 2021	May. 20, 2022
TESTO	Hygro meter	608-H1	45207528	Oct. 22, 2021	Oct. 21, 2022
Aglient	Spectrum Analyzer	E4408B	MY44211028	Aug. 19, 2021	Aug. 18, 2022
Custom Microwave	Standard Horn antenna	M15RH	V91113-A	NCR	NCR

7. System Verification Source

The System Verification sources at 30 GHz and above comprise horn-antennas and very stable signal generators.

Model	Ka-band horn antenna
Calibrated frequency:	30 GHz at 10mm from the case surface
Frequency accuracy	± 100 MHz
E-field polarization	linear
Harmonics	-20 dBc
Total radiated power	14 dBm
Power stability	0.05 dB
Power consumption	5 W
Size	00 x 100 x 100 mm
Weight	1 kg



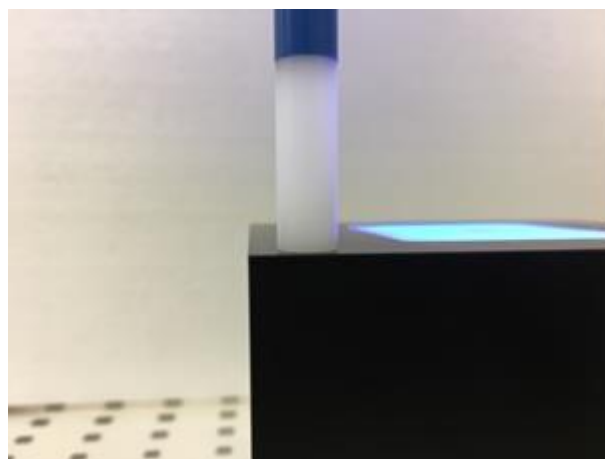
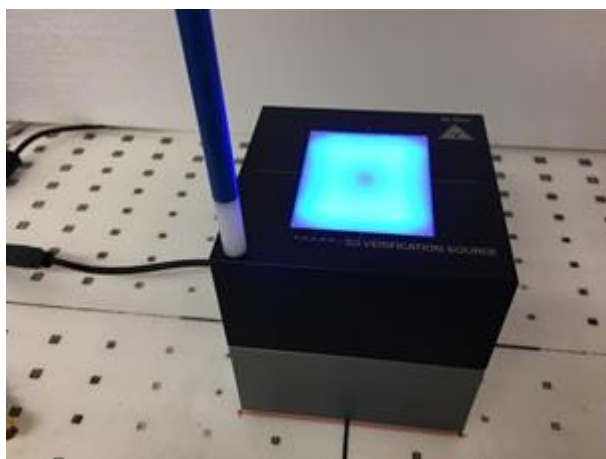
8. Power Density System Verification

The system performance check verifies that the system operates within its specifications.

The EUT is replaced by a calibrated source, the same spatial resolution, measurement region and the test separation used in the calibration was applied to system check. Through visual inspection into the measured power density distribution, both spatially (shape) and numerically (level) have no noticeable difference. The measured results should be within 0.66dB of the calibrated targets.

Frequency [GHz]	Grid step	Grid extent X/Y [mm]	Measurement points
10	$0.25 \left(\frac{\lambda}{4}\right)$	120/120	16×16
30	$0.25 \left(\frac{\lambda}{4}\right)$	60/60	24×24
60	$0.25 \left(\frac{\lambda}{4}\right)$	32.5/32.5	26×26
90	$0.25 \left(\frac{\lambda}{4}\right)$	30/30	36×36

Settings for measurement of verification sources



Verification Setup photo

9. System Verification Results

Frequency (GHz)	5G Verification Source	Probe S/N	DAE S/N	Distance (mm)	Measured 4 cm ² (W/m ²)	Targeted 4 cm ² (W/m ²)	Deviation (dB)	Date	Test Site
30G	30GHz_1007	9441	778	10	32.6	35.8	-0.41	2022/1/31	SAR06-HY
30G	30GHz_1007	9441	778	10	32.8	35.8	-0.38	2022/3/10	SAR06-HY

9.1 Computation of the Electric Field Polarization Ellipse

For the numerical description of an arbitrarily oriented ellipse in three-dimensional space, five parameters are needed: the semi-major axis (a), the semi-minor axis (b), two angles describing the orientation of the normal vector of the ellipse (ϕ , θ), and one angle describing the tilt of the semi-major axis (ψ). For the two extreme cases, i.e., circular and linear polarizations, three parameters only (a , ϕ and θ) are sufficient for the description of the incident field.

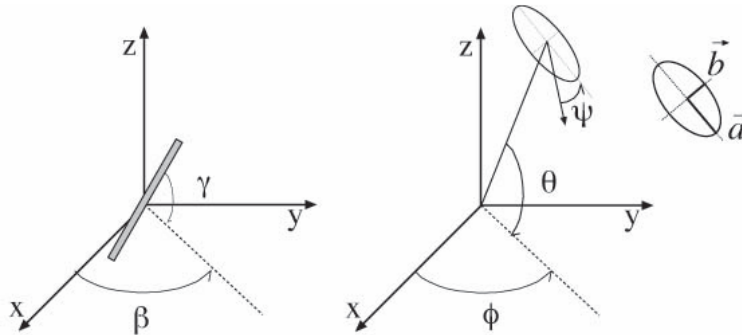


Illustration of the angles used for the numerical description of the sensor and the orientation of an ellipse in 3-D space.

For the reconstruction of the ellipse parameters from measured data, the problem can be reformulated as a nonlinear search problem. The semi-major and semi-minor axes of an elliptical field can be expressed as functions of the three angles (ϕ , θ and ψ). The parameters can be uniquely determined towards minimizing the error based on least-squares for the given set of angles and the measured data. In this way, the number of free parameters is reduced from five to three, which means that at least three sensor readings are necessary to gain sufficient information for the reconstruction of the ellipse parameters. However, to suppress the noise and increase the reconstruction accuracy, it is desirable that the system of equations be over determined. The solution to use a probe consisting of two sensors angled by r_1 and r_2 toward the probe axis and to perform measurements at three angular positions of the probe, i.e., at β_1 , β_2 and β_3 , results in over-determinations by a factor of two. If there is a need for more information or increased accuracy, more rotation angles can be added. The reconstruction of the ellipse parameters can be separated into linear and non-linear parts that are best solved by the Givens algorithm combined with a downhill simplex algorithm. To minimize the mutual coupling, sensor angles are set with a shift of 90 degree ($r_2 = r_1 + 90$ degree), and to simplify, the first rotation angle of the probe (β_1) can be set to 0 degree.

9.2 Total Field and Power Flux Density Reconstruction

Computation of the power density in general requires knowledge of the electric and magnetic field amplitudes and phases in the plane of incidence. Reconstruction of these quantities from pseudo-vector E-field measurements is feasible, as they are constrained by Maxwell's equations. SPEAG have developed a reconstruction approach based on the Gerchberg-Saxton algorithm, which benefits from the availability of the E-field polarization ellipse information obtained with the EUmWV2 probe.

The average of the reconstructed power density is evaluated over a circular area in each measurement plane. Two average power density values can be computed, the average total power density and the average incident power density, and the average total power density is used to determine compliance.

- $|Re\{S\}|$ is the total Poynting vector
- $\mathbf{n} \cdot Re\{S\}$ is the normal Poynting vector

The software post-processing reports to values, "S avg tot" and "S avg inc". "S avg tot" represents average total power density (all three xyz components included), and "S avg inc" represents average normal power density. The average total power density "S avg tot" is reported to determine the device compliance.

10. RF Exposure Evaluation Results

1. The PD test was performed of a 2mm separation between sensor and EUT surface (the probe tip is 0.5mm to the EUT surface).
2. According to TCBC Workshop in October 2018, 4 cm² averaging area are used.
3. This device is enabled with Qualcomm® Smart Transmit feature, smart transmit will manage and ensure LTE and 5G simultaneous transmission is compliant. The validation of the time-averaging algorithm and compliance under the Tx varying transmission scenario for WWAN technologies are reported in Part 2 report.
4. Input power limit parameter for 5G mmW NR radio was calculated in RF Exposure Part 0 test report.
5. The device was configured to transmit CW wave signal for testing, due to Qualcomm® Smart Transmit feature, additional testing was not required for different modulations (CP-OFDM QPSK, CP-OFDM 16QAM, CP-OFDM 64QAM), RB configurations, component carriers, channel configurations (low channel, mid channel, high channel).
6. It's illustrated in Part 0 report that , for 5G mmW NR since there is total design-related uncertainty arising from TxAGC and device-to-device variation, the worst-case RF exposure should be determined by accounting for this device uncertainty of 2.1 dB, as well as PD design target of 5.55W/m². Therefore, 5G mmW NR RF exposure for this DUT is evaluated by reported PD calculated as:

$$\text{Reported PD} = \text{PD design target} + 2.1 \text{ dB} = 9 \text{ W/cm}^2 = 0.9 \text{ mW/cm}^2$$

Plot No.	Band	Antenna Module	Beam ID 1	Beam ID 2	Frequency (GHz)	Exposure Surface	Input Power limit	Test Separation (mm)	Modulation	Epeak [V/m]	Hpeak [A/m]	Measured results Savg inc 4cm ² (W/m ²)	Measured results Savg tot 4cm ² (W/m ²)
	n260	AiP_0	30	-	38.5	Bottom of Laptop	12.45	2mm	CW	73.7	0.18	5.02	5.67
	n260	AiP_0	44	-	38.5	Bottom of Laptop	12.56	2mm	CW	71.7	0.188	2.84	3.43
	n260	AiP_0	0	-	38.5	Bottom of Laptop	17.84	2mm	CW	30.3	0.09	0.921	1.2
	n260	AiP_0	-	171	38.5	Bottom of Laptop	12.08	2mm	CW	64	0.17	4.89	5.62
	n260	AiP_0	29	157	38.5	Bottom of Laptop	8.37	2mm	CW	65.9	0.17	3.25	3.88
	n260	AiP_1	33	-	38.5	Bottom of Laptop	11.19	2mm	CW	58.6	0.172	2.42	2.88
	n260	AiP_1	-	164	37	Bottom of Laptop	10.91	2mm	CW	73.5	0.164	1.99	2.22
	n260	AiP_1	33	161	38.5	Bottom of Laptop	7.01	2mm	CW	50.2	0.148	0.903	1.1
	n260	AiP_2	51	-	38.5	Bottom of Laptop	11.15	2mm	CW	59.2	0.186	4.42	4.71
1	n260	AiP_2	-	166	38.5	Bottom of Laptop	9.36	2mm	CW	76.1	0.202	5.18	6.82
	n260	AiP_2	40	168	38.5	Bottom of Laptop	6.92	2mm	CW	50	0.13	2.37	2.98
	n261	AiP_0	29	-	27.925	Bottom of Laptop	9.1	2mm	CW	64.4	0.18	4.65	5.36
2	n261	AiP_0	30	-	27.5	Bottom of Laptop	10.31	2mm	CW	74.4	0.192	7.18	7.61
	n261	AiP_0	3	-	28.35	Bottom of Laptop	15.1	2mm	CW	60.2	0.151	3.38	3.67
	n261	AiP_0	-	158	27.925	Bottom of Laptop	9.07	2mm	CW	59.5	0.17	4.13	4.63
	n261	AiP_0	30	158	27.925	Bottom of Laptop	5.51	2mm	CW	55.5	0.162	4.3	4.58
	n261	AiP_1	34	-	28.35	Bottom of Laptop	7.15	2mm	CW	34.2	0.094	0.642	0.744
	n261	AiP_1	-	163	28.35	Bottom of Laptop	2.03	2mm	CW	57.5	0.141	2.52	3.06
	n261	AiP_1	47	175	28.35	Bottom of Laptop	3.5	2mm	CW	25.5	0.069	0.624	0.722
	n261	AiP_2	39	-	27.5	Bottom of Laptop	8.84	2mm	CW	60.6	0.142	4.18	4.82
	n261	AiP_2	-	168	27.5	Bottom of Laptop	6.22	2mm	CW	65.5	0.175	4.51	5.09
	n261	AiP_2	51	179	28.35	Bottom of Laptop	5.22	2mm	CW	67.6	0.2	5.67	6.06

**11. 5G NR + LTE + WLAN + BT Sim-Tx analysis**

In 5G NR + LTE + WLAN + BT simultaneous transmission, 5G NR and LTE transmission are managed and controlled by Qualcomm® Smart Transmit, while the RF exposure from WLAN and BT radios is managed using legacy approach, i.e., through a fixed power back-off if needed.

Since WLAN and BT do not employ time-averaging, 1gSAR and 10gSAR measurement for WLAN and BT need to be conducted at their corresponding rated power following current FCC test procedures to determine reported SAR values.

Smart Transmit current implementation assumes hotspots from 5G NR and LTE are collocated. Therefore, for a total of 100% exposure margin, if LTE uses x%, then the exposure margin left for 5G NR is capped to (100-x)%. Thus, the compliance equation for LTE + 5G NR is

$$x\% * A + (100-x)\% * B \leq 1.0,$$

Where, A is normalized reported time-averaged SAR exposure ratio from LTE, and $A \leq 1.0$; B is normalized reported time-averaged exposure ratio from 5G NR (i.e., PD exposure for mmW NR or SAR exposure for sub6 NR), and $B \leq 1.0$.

Let C = normalized reported SAR exposure ratio from WLAN+BT, then for compliance,

$$x\% * A + (100-x)\% * B + C \leq 1.0 \quad (1)$$

$$x\% * A + (100-x)\% * B \leq x\% * \max(A, B) + (100-x)\% * \max(A, B) \leq \max(A, B)$$

$$x\% * A + (100-x)\% * B + C \leq \max(A, B) + C \leq 1.0 \quad (2)$$

if $A + C \leq 1.0$ and $B + C \leq 1.0$ can be proven, then " $x\% * A + (100-x)\% * B + C \leq 1.0$ ". Therefore simultaneous transmission analysis for 5G NR + LTE + WLAN + BT can be performed in two steps

Step 1: Prove total exposure ratio (TER) of LTE + WLAN + BT < 1

Step 2: Prove total exposure ratio (TER) of 5G NR + WLAN + BT < 1

Else, if $A + C > 1.0$ and/or $B + C > 1.0$, then the followings need to hold true for compliance:

i. A and C are decoupled based on the SPLSR criteria , and

ii. $(100-x)\% * B + C \leq 1.0$, and

iii. $x\% * A + (100-x)\% * B \leq 1.0$

Note iii. is covered in Part 2 report; i. and ii. should be addressed in Part 2 report.

Step 1: it's justified in Part 1 SAR report (Sporton report number FA1D1645, rev.01)

Step 2: it's justified in section 11.1



Furthermore, for LTE + WLAN + BT and 5G sub6 NR + WLAN + BT, the reported SAR from each radio should be used in total SAR exposure analysis, where reported SAR from WLAN and BT is determined using corresponding rated power (denoted as SAR_{WLAN} and SAR_{BT}, respectively), and the reported time-averaged SAR for LTE and 5G sub6 NR should be scaled to their corresponding power level that is equal to “minimum {[P_{limit} (dBm) + design related total uncertainty], P_{max}}”. Here, the design related total uncertainty is the device design uncertainty for all radios operating at frequency below 6GHz.

Similarly, for 5G mmW NR + WLAN + BT, the normalized reported exposure ratio from each radio should be used in total exposure ratio (TER) analysis, where,

$$\text{Reported SAR exposure ratio from WLAN or BT} = \frac{SAR_{WLAN} \text{ or } SAR_{BT}}{\text{regulatory limit}}$$

$$\begin{aligned} & \text{Reported time average PD exposure ratio from 5G mmWave NR} \\ &= (\text{PD_design_targer}) + \text{mmWave device design related total uncertainty} \end{aligned}$$

The TER analysis for the simultaneous transmission containing WLAN and BT is similar to legacy approach. It is worth to note that in the case of 5G mmW NR + WLAN + BT, perform TER for only mmW modules that are close to WLAN/BT antennas. Some of mmW modules can be excluded from TER analysis if they meet below criteria:

Demonstrate exclusion by showing no overlap in -10dB contours (relative to hotspot value) for both simulated PD distributions for all supported beams by this mmW module and measured SAR distributions of WLAN/BT, assuming PD exposure ratio is less than 0.9 (note that PD is capped to 75% for 3dB in reserve_power_margin setting) and TER of WLAN+BT is less than 0.9. Note that PD distributions be included in Section 11 of Part 1 report to support this analysis.



12. Simultaneous-Tx analysis

NO.	Simultaneous Transmission Configurations
1.	WLAN2.4GHz Ant 1+2 + FR2
2.	WLAN5G/6GHz Ant 1+2 + Bluetooth Ant 2 + FR2
3.	WLAN2.4GHz Ant 1+2 + FR2
4.	WLAN5G/6GHz Ant 1+2 + Bluetooth Ant 2 + FR2

General Note:

1. The WLAN and Bluetooth SAR test results were referring the report of FCC ID: PU5-TP00139AM Part1 SAR Report No. FA1D1645.
2. Considering FR2 transmitter with WLAN and Bluetooth can transmit simultaneously, the basic restrictions are on SAR and power density, and summation of these quantities should follow below formula and the simultaneous transmission analysis was following below step.
 - i) Step 1, Use the standalone SAR according original report to collocate with n260/n261 transmitter power density at each exposure positions, if the result < 1, additional analysis is not necessary.
 - ii) Step 2, if the ration is larger than 1, but WWAN and WLAN/BT meet SPLSR criteria, then it means WWAN and WLAN/ are decoupled, therefore mmWave design target + uncertainty * 75% will be used for simultaneous transmission analysis. (it's justified in Part 1 SAR report (Sporton report number FA9N2705A, rev.01))
 - iii) Step 3, If the ratio still is larger than 1, Demonstrate exclusion by showing no overlap in -10dB contours (relative to hotspot value) for both PD distributions for all supported beams by this mmW module and measured SAR distributions of WLAN/BT.
 - iv) Step 4, if step 3 which the demonstrate exclusion by showing no overlap in -10dB contours (relative to hotspot value) of mmWave and WiFi/BT, the maximum ratio = mmWave design target + uncertainty * 75%, so when the summed ratio is higher than 1, that the maximum summation ratio is 0.75 in this report.

The $[\sum \text{ of (the highest measured or estimated SAR for each standalone antenna configuration, adjusted for maximum tune-up tolerance) / 1.6 W/kg}] + [\sum \text{ of MPE ratios}]$ is ≤ 1.0 .



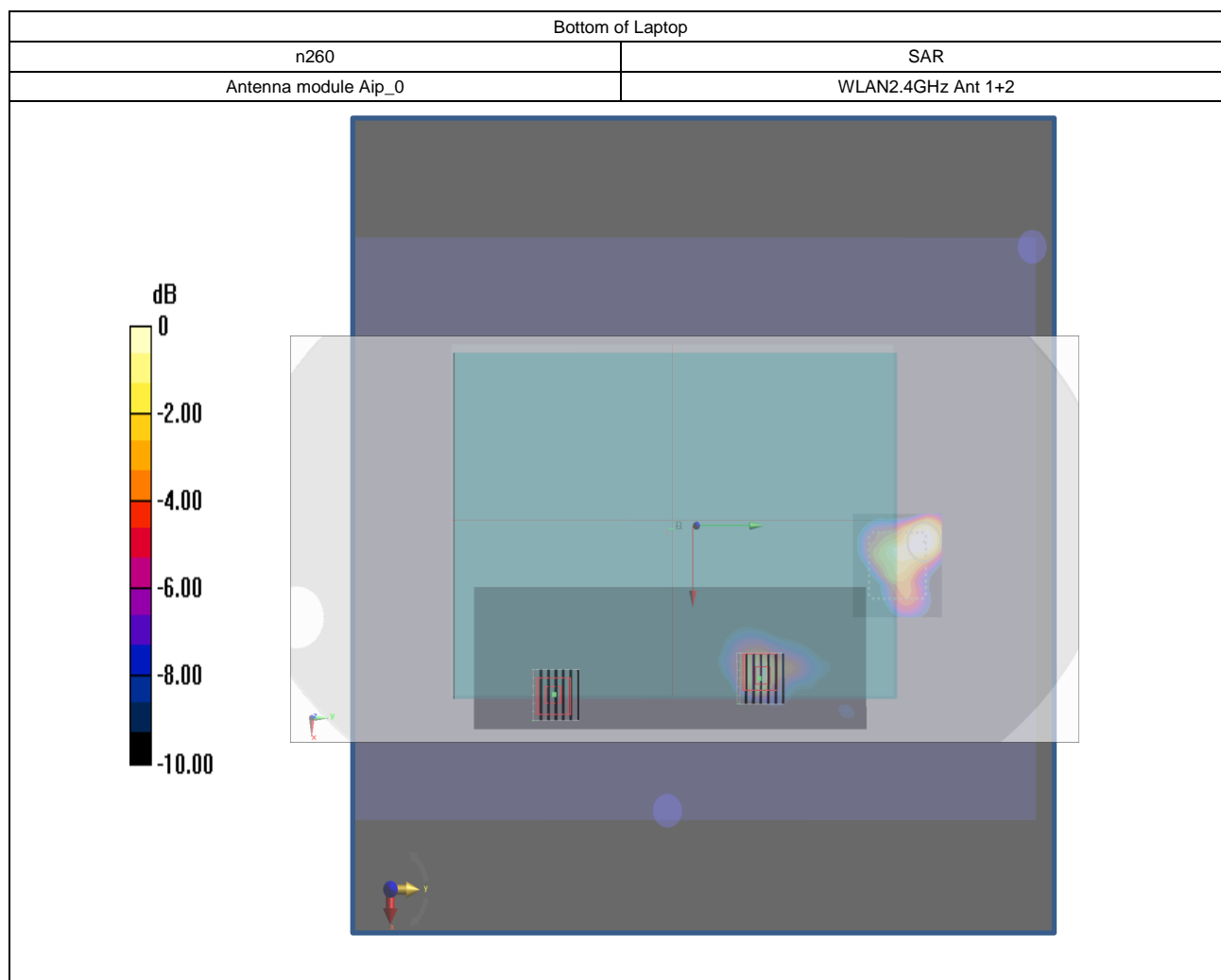
12.1 Simultaneous transmission analysis for WiFi/BT + 5G NR

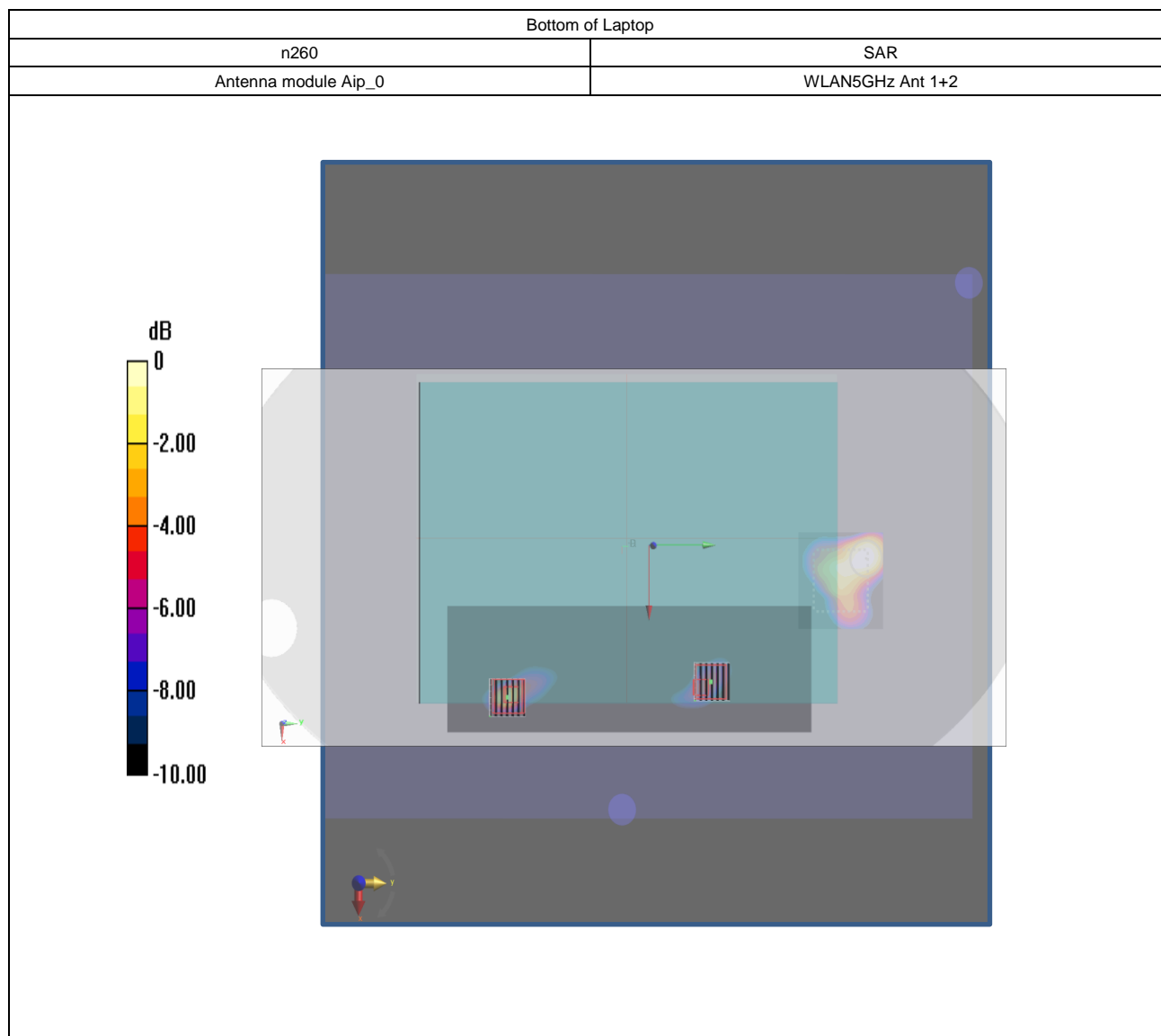
<Step 1>

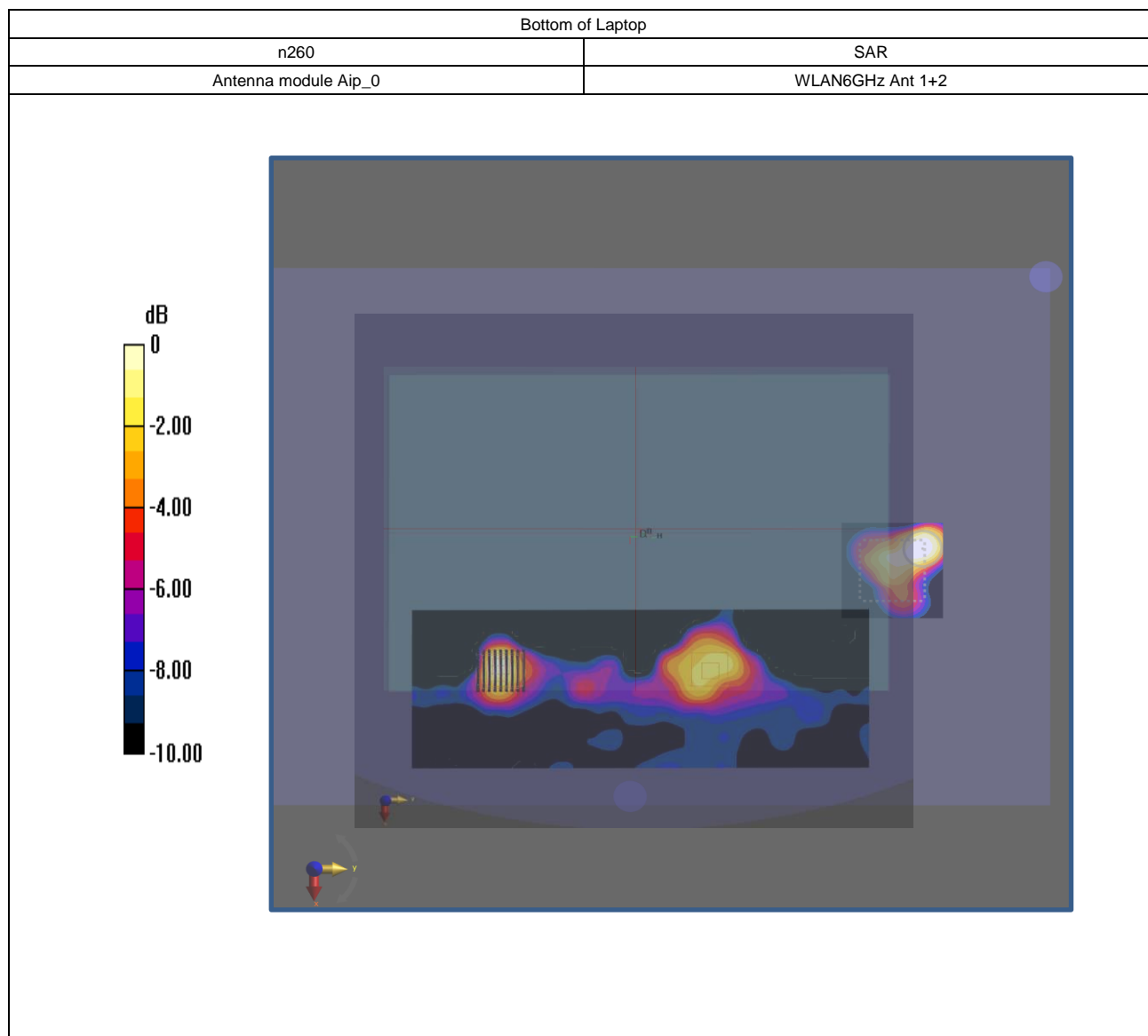
WWAN Band		2	3	4	5	6	Reported SAR/1.6 + PD/10 Summation		
		2.4GHz WLAN Ant 1+2	5GHz WLAN Ant 1+2	6GHz WLAN Ant 1+2	Bluetooth Ant 1	PD	2+6 Summed	3+5+6 Summed	4+5+6 Summed
		1g SAR (W/kg)	1g SAR (W/kg)	1g SAR (W/kg)	1g SAR (W/kg)	4cm ² (W/m ²)			
n260	Antenna Module 0	0.738	0.598	0.492	0.115	9.000	1.361	1.346	1.279
n260	Antenna Module 1	0.738	0.598	0.492	0.115	5.000	0.961	0.946	0.879
n260	Antenna Module 2	0.738	0.598	0.492	0.115	9.000	1.361	1.346	1.279
n261	Antenna Module 0	0.738	0.598	0.492	0.115	9.000	1.361	1.346	1.279
n261	Antenna Module 1	0.738	0.598	0.492	0.115	5.000	0.961	0.946	0.879
n261	Antenna Module 2	0.738	0.598	0.492	0.115	9.000	1.361	1.346	1.279

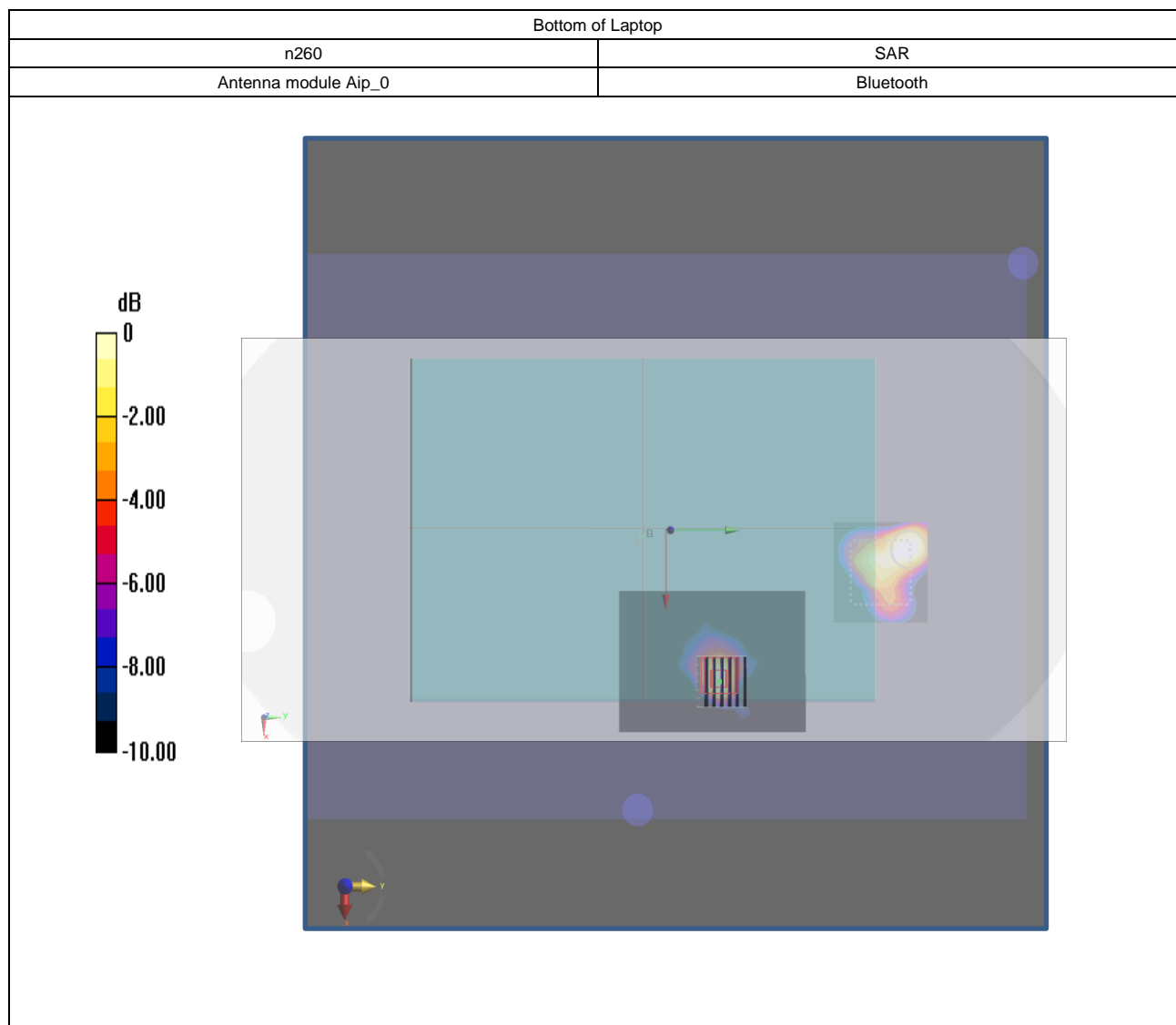
<Step 2>
General Note:

- below simulated PD distributions for all supported beams by this mmW module and measured SAR distributions of WLAN/BT are demonstrate exclusion by showing no overlap in -10dB contours(relative to hotspot value).

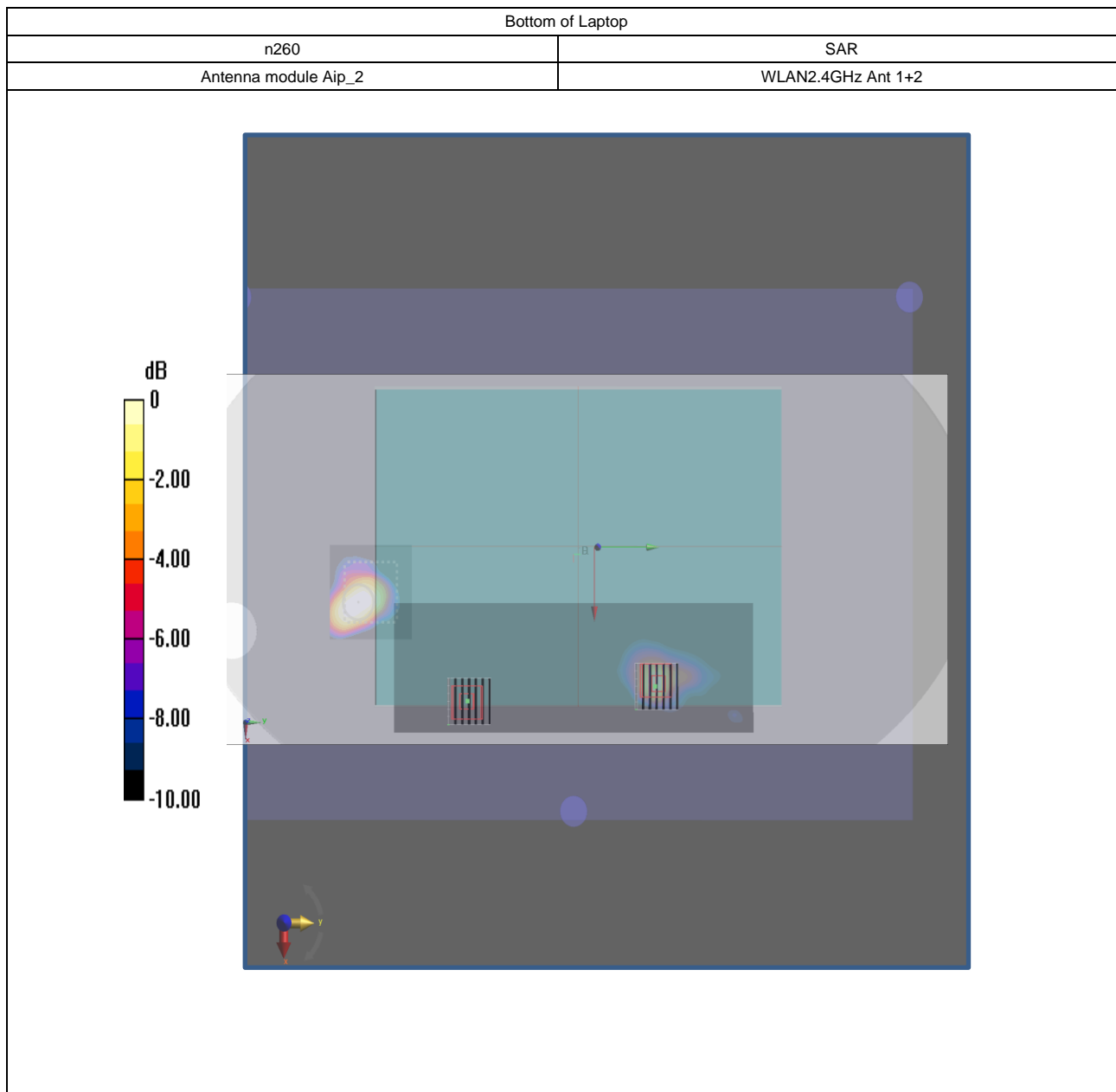
<n260 antenna module 1>


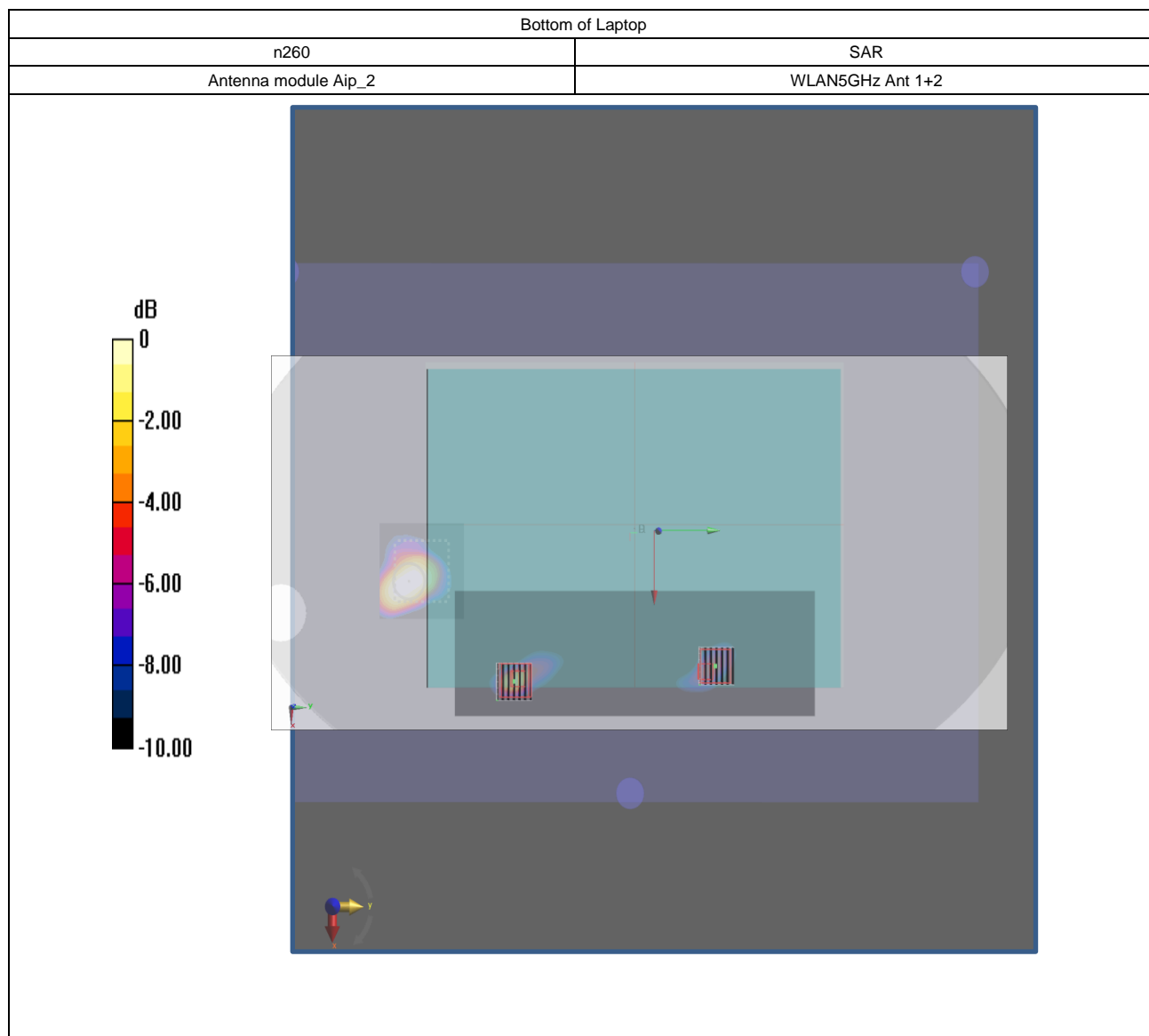


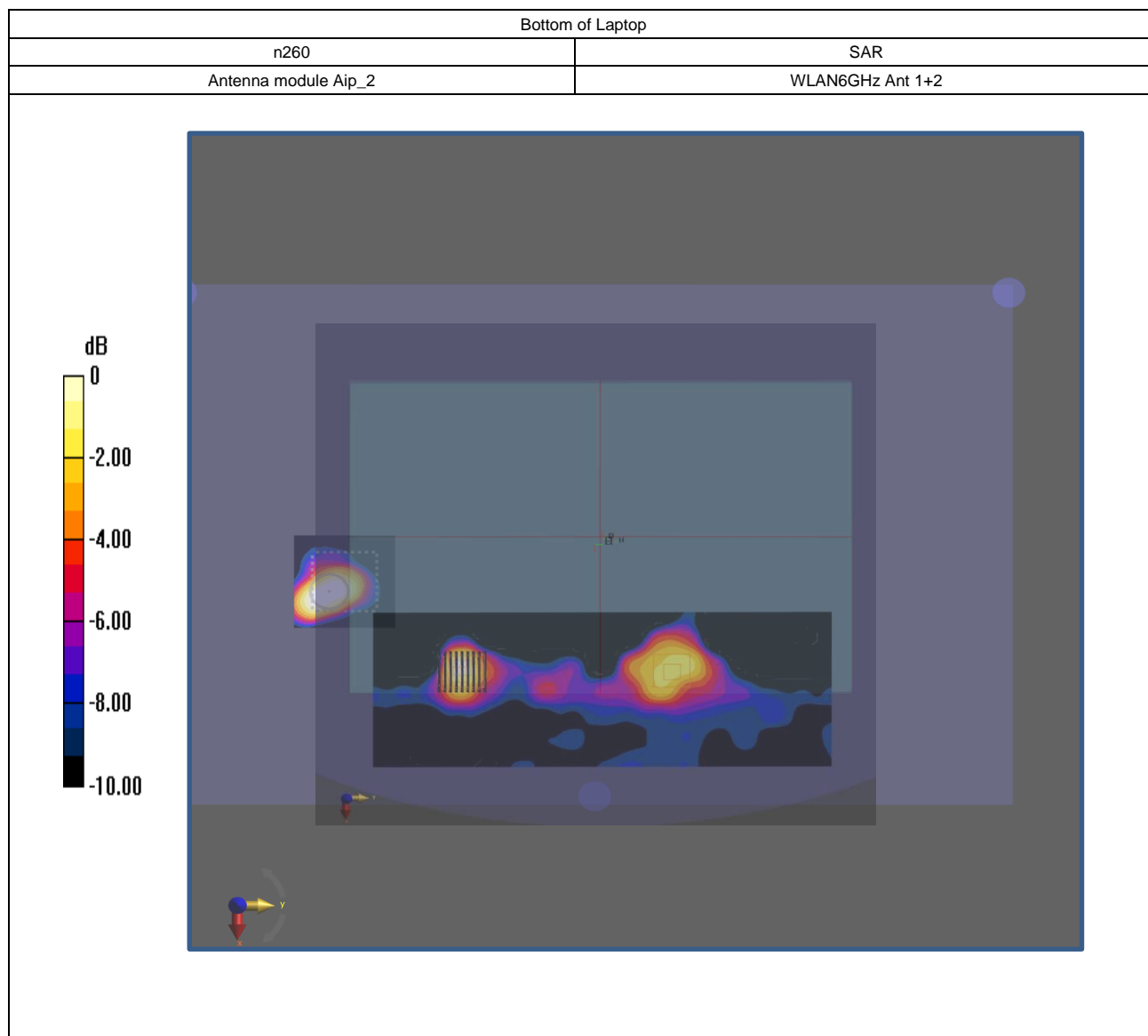


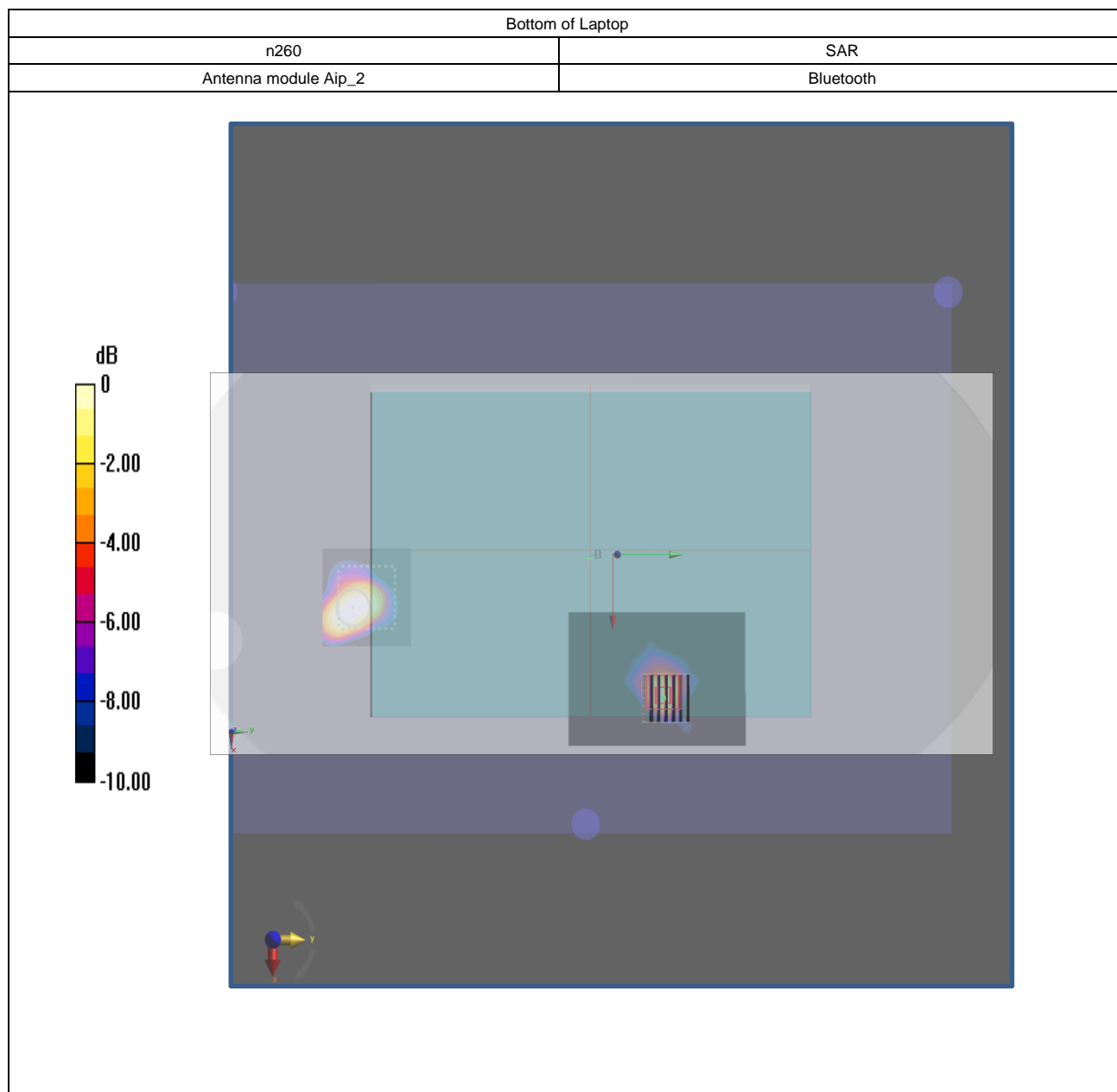


<n260 antenna module 2>

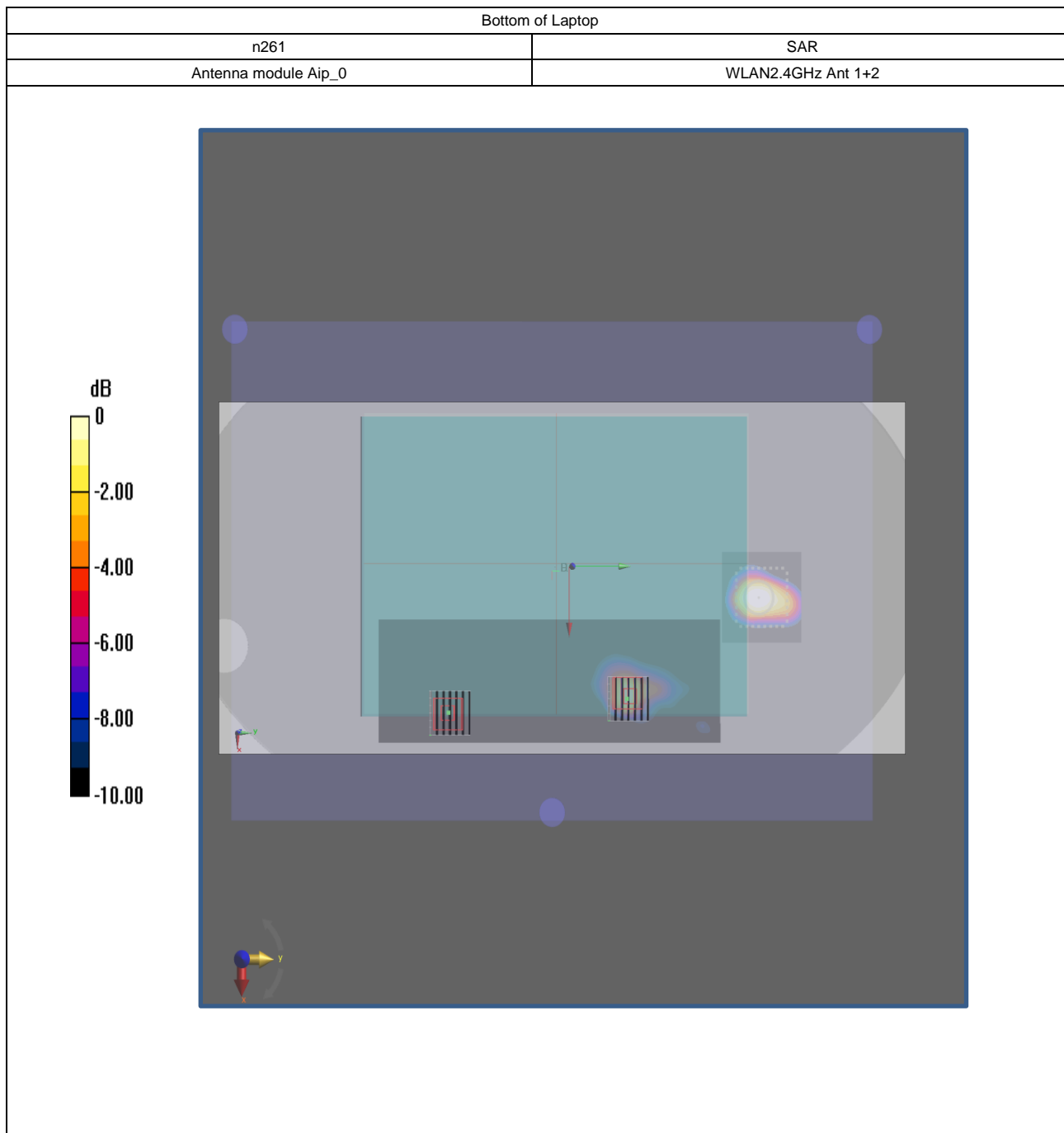


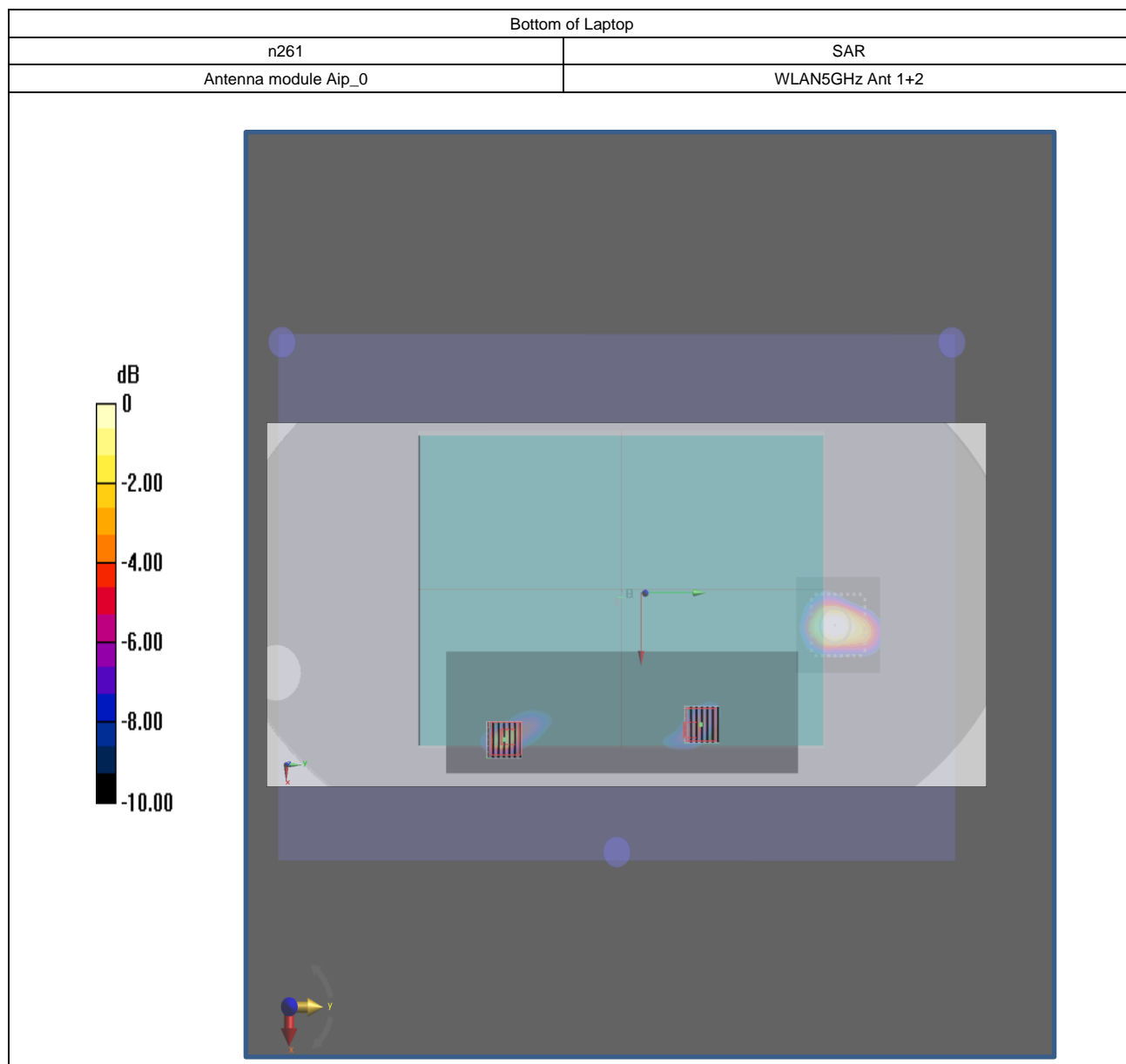


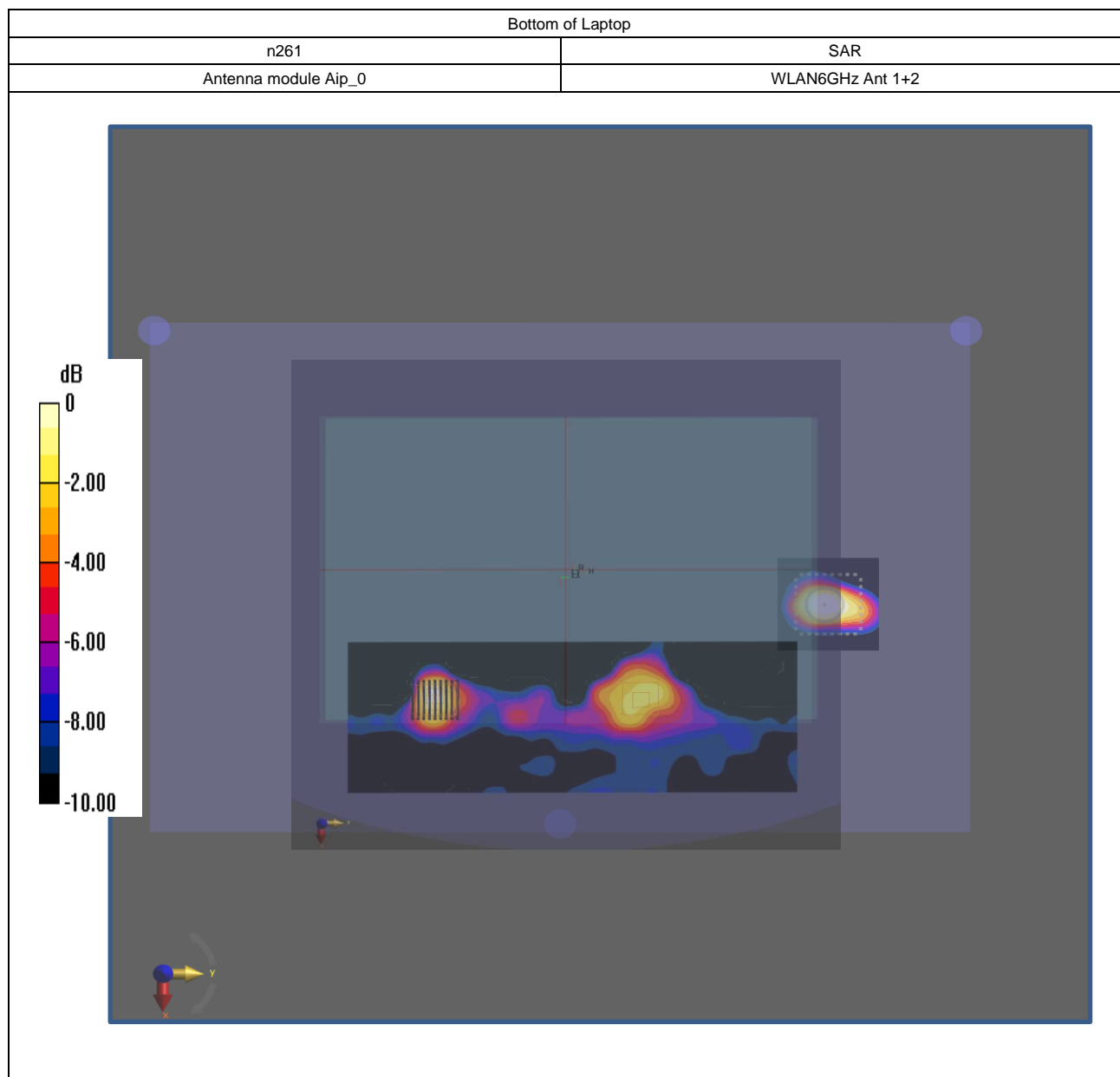


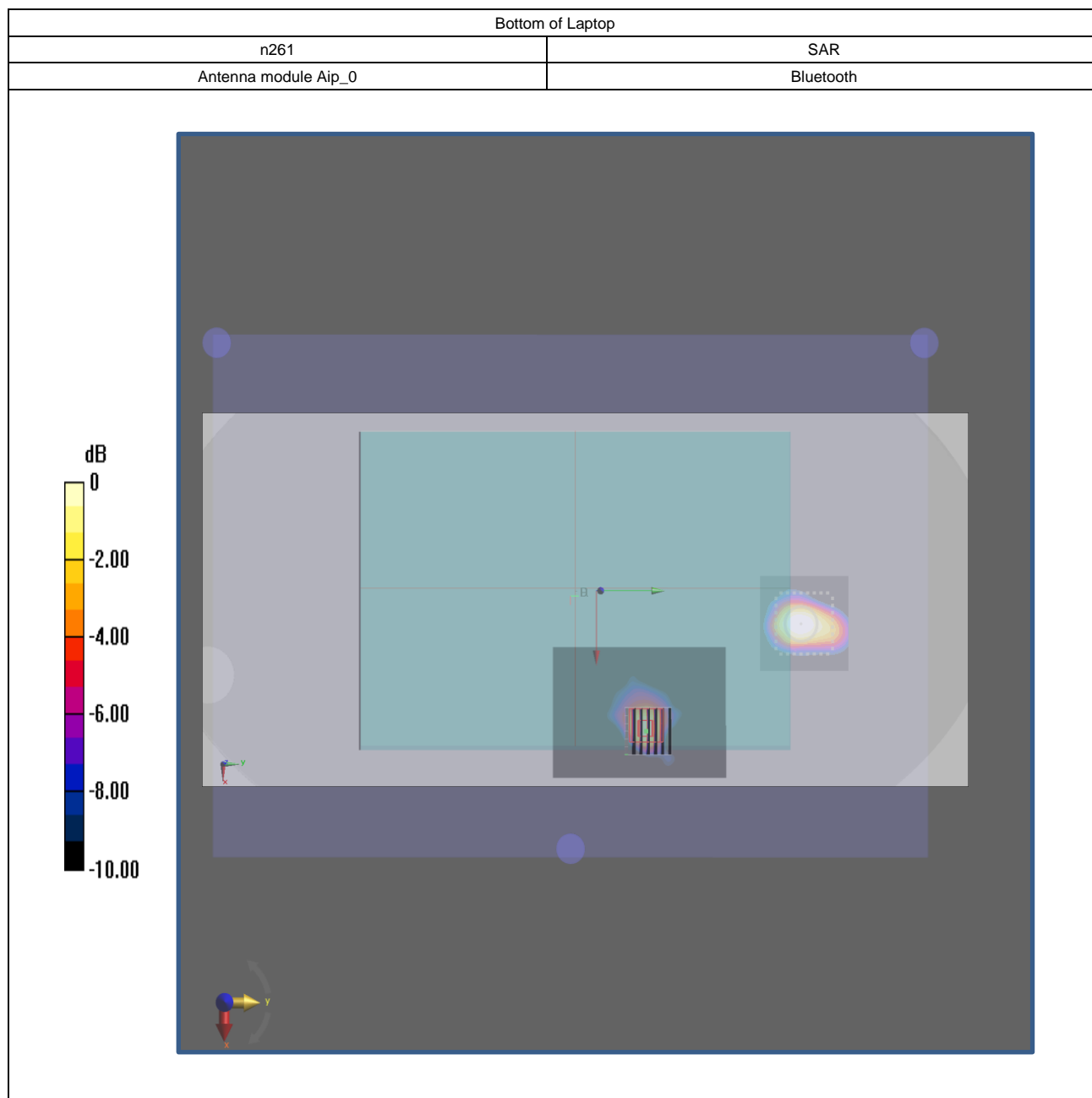


<n261 antenna module 0>

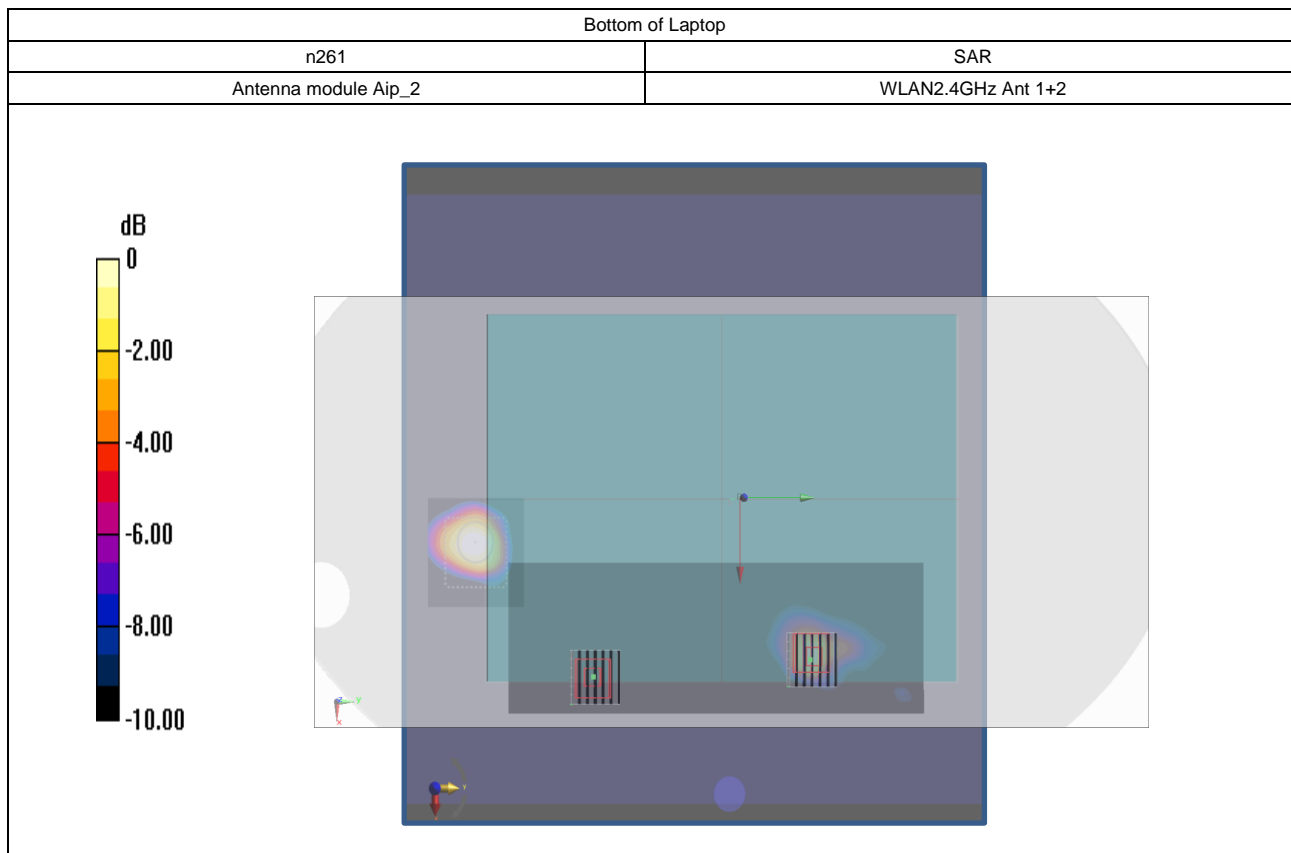


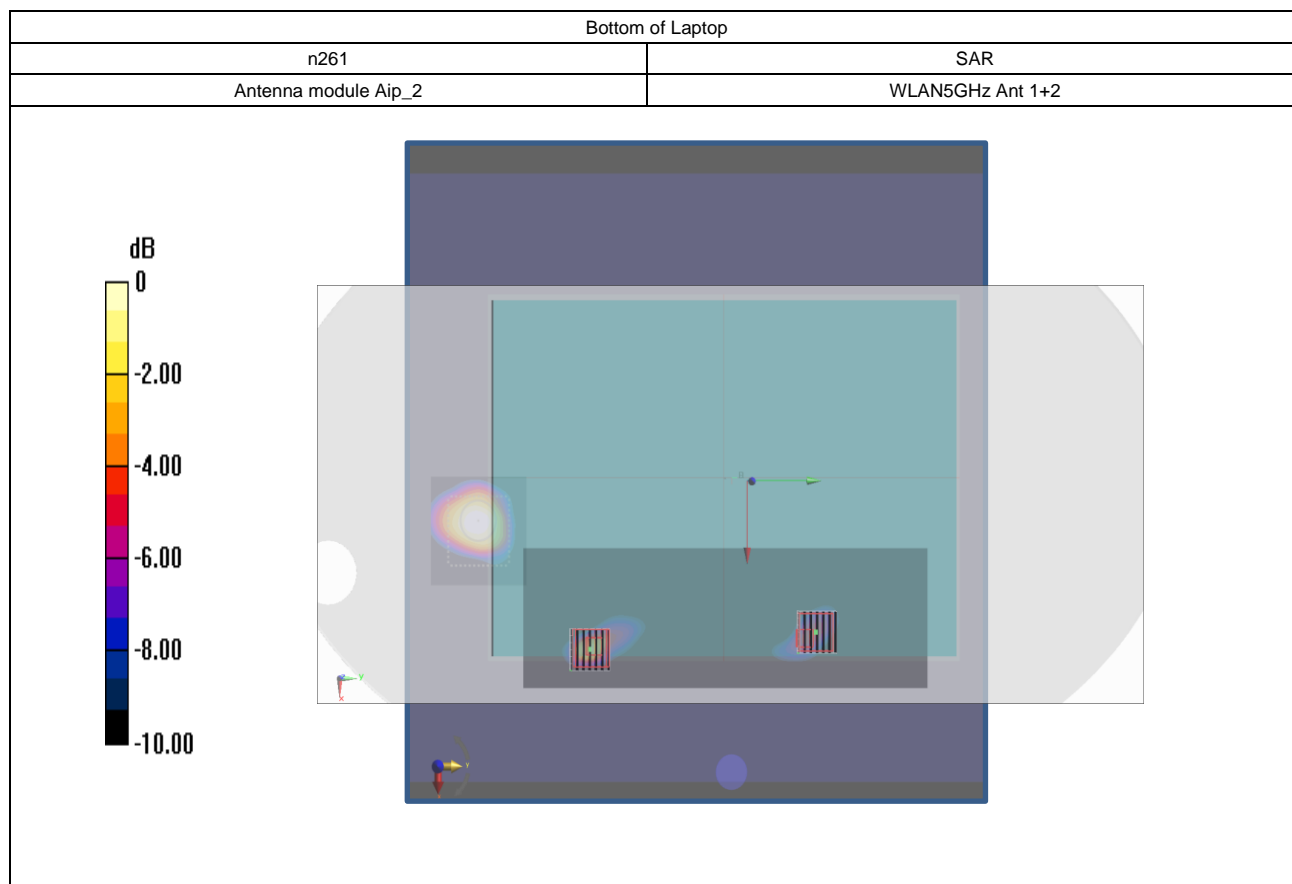


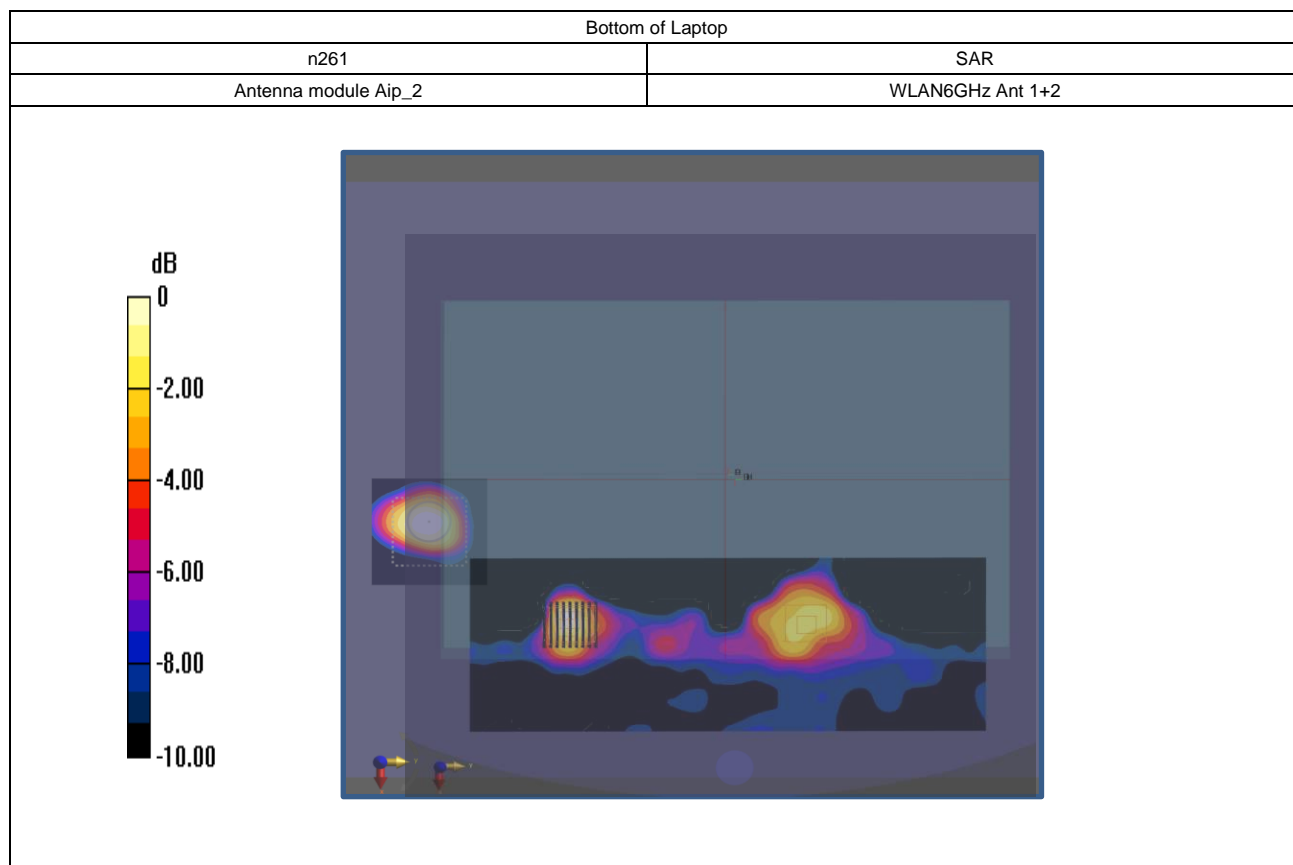


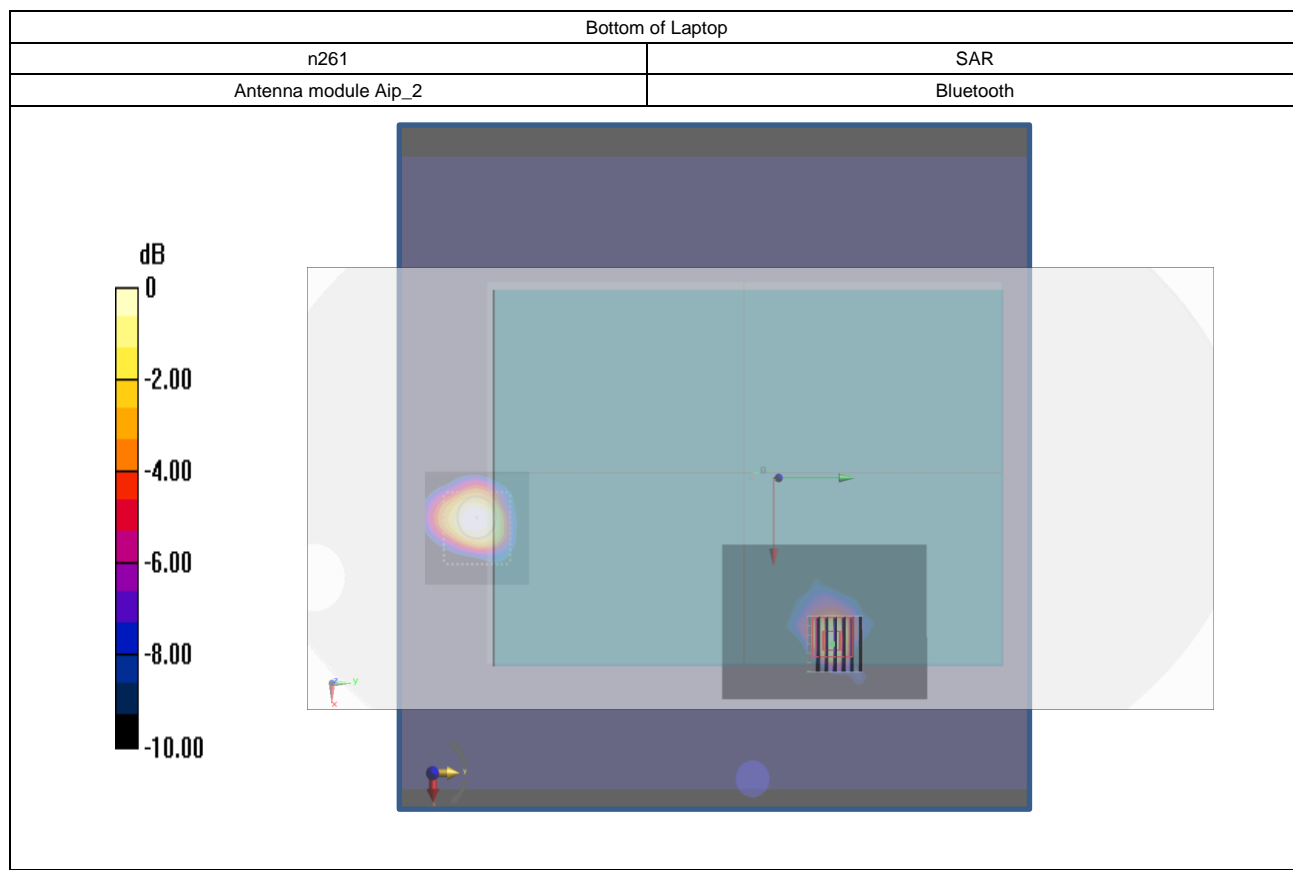


<n261 antenna module 2>









Test Engineer : Mood Huang and Carter Jhuang

13. Uncertainty Assessment

The budget is valid for evaluation distances $> \lambda/2\pi$. For specific tests and configurations, the Uncertainty could be considerably smaller.

Preliminary Module mmWave Uncertainty Budget Evaluation Distances to the Antennas $> \lambda / 2\pi$						
Error Description	Uncertainty Value (\pm dB)	Probability	Divisor	(Ci)	Standard Uncertainty (\pm dB)	(Vi) Veff
Measurement System						
Probe Calibration	0.49	N	1	1	0.49	∞
Hemispherical Isotropy	0.50	R	1.732	1	0.29	∞
Linearity	0.20	R	1.732	0	0.12	∞
System Detection Limits	0.04	R	1.732	1	0.02	∞
Modulation Response	0.40	R	1.732	1	0.23	∞
Readout Electronics	0.03	N	1	1	0.03	∞
Response Time	0.00	R	1.732	1	0.00	∞
Integration Time	0.00	R	1.732	1	0.00	∞
RF Ambient Noise	0.2	R	1.732	1	0.12	∞
RF Ambient Reflections	0.21	R	1.732	1	0.12	∞
Probe Positioner	0.04	R	1.732	1	0.02	∞
Probe Positioning	0.30	R	1.732	1	0.17	∞
S _{avg} Reconstruction	0.60	R	1.732	1	0.35	∞
Test Sample Related						
Power Drift	0.2	R	1.732	1	0.12	∞
Input Power	0	N	1	0	0.00	∞
Combined Std. Uncertainty					0.76 dB	∞
Coverage Factor for 95 %					K=2	
Expanded STD Uncertainty					1.52 dB	



14. References

- [1] FCC 47 CFR Part 2 "Frequency Allocations and Radio Treaty Matters; General Rules and Regulations"
- [2] FCC KDB 447498 D01 v06, "Mobile and Portable Device RF Exposure Procedures and Equipment Authorization Policies", Oct 2015
- [3] FCC KDB 865664 D02 v01r02, "RF Exposure Compliance Reporting and Documentation Considerations" Oct 2015.
- [4] FCC KDB 648474 D04 v01r03, "SAR Evaluation Considerations for Wireless Handsets", Oct 2015.