

4. TEST REPORT

4.1 RF Power Measurements

Figure 4-1 shows the test equipment setup for the RF power measurements.

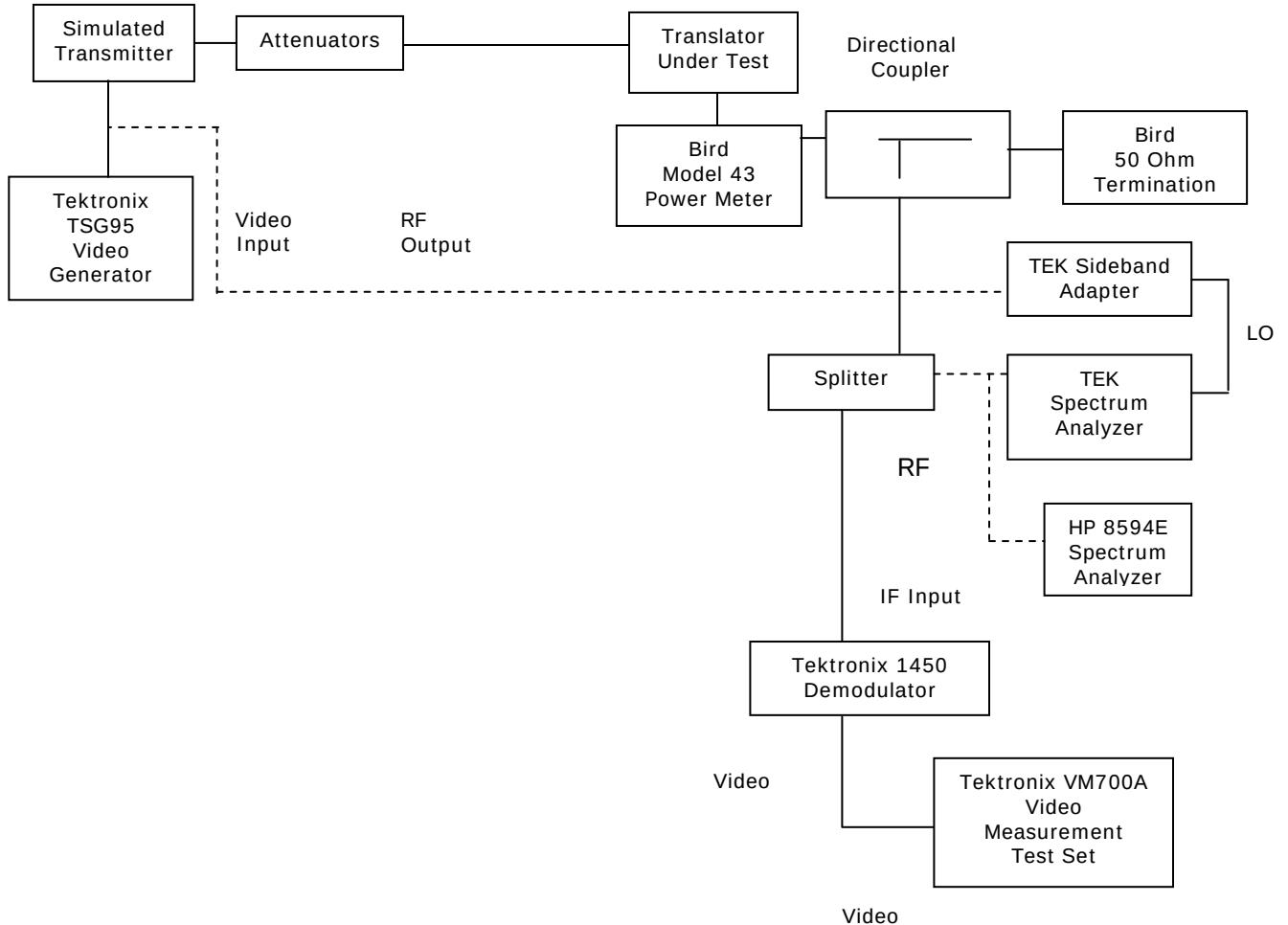


Figure 4-1. Test Equipment Setup for RF Power Measurements

The video modulation was adjusted for 25% with sync and blanking video signals and the aural power was turned off. The power was then adjusted to obtain 60 watts of average visual RF output (100 watts peak sync at the output connector). This level was used to establish a reference on the spectrum analyzer.

Next, the aural power was turned on and adjusted to 10 dB below the visual power. The following operating parameters were recorded:

Peak Visual Power /100% = 100 Watts
 Aural Power /100% = 10 Watts continuous wave (CW)
 Reflected Power: <2%

4.2 Modulation Characteristics

4.2.1 Video Modulation

The test setup shown in Figure 4-1 was used to adjust the video signal to obtain a white picture level using the Tektronix 1450 Demodulator chopper function, the modulation was accurately measured to be 87.5% while maintaining a depth of modulation at blanking.

Next, the video was adjusted for modulated staircase and the differential phase and gain were measured and recorded as follows:

- Differential phase: $\pm 1.5^\circ$
- Differential gain : 4%

Figure 4-2 shows the substantially linear transfer characteristics of the transmitter as a demodulated video waveform.



Figure 4-2. Substantially Linear Transfer Characteristics of the Transmitter as a Demodulated Video Waveform

4.2.2 Video Envelope Delay

Not Applicable - Unit under test is a translator.

4.2.3 Video Noise

Not Applicable - Unit under test is a translator.

4.2.4 Video Frequency Response

The test setup shown in Figure 4-1 was used to record the detected video frequency response; the results are shown in Table 4-2 and Figure 4-3.

Note: For this test, the video signal was adjusted to provide a 50 % average picture level and the video sweep signal level was set to cover the range from black to white picture.

Table 4-2. Detected Video Frequency Response

VIDEO FREQUENCY	RELATIVE RESPONSE
200 kHz	+2 dB
500 kHz	0 dB
750 kHz	+0.2 dB
1.0 MHz	-0.2 dB
1.25 MHz	+0.4 dB
1.5 MHz	+0.3 dB
2.0 MHz	+0.4 dB
2.5 MHz	0 dB
3.0 MHz	+0.3 dB
3.5 MHz	+0.3 dB
3.58 MHz	+0.1 dB
4.1 MHz	-0.6 dB
4.18 MHz	-2.0 dB
4.5 MHz	-21 dB
4.75 MHz	-40 dB
5.0 MHz	-47 dB

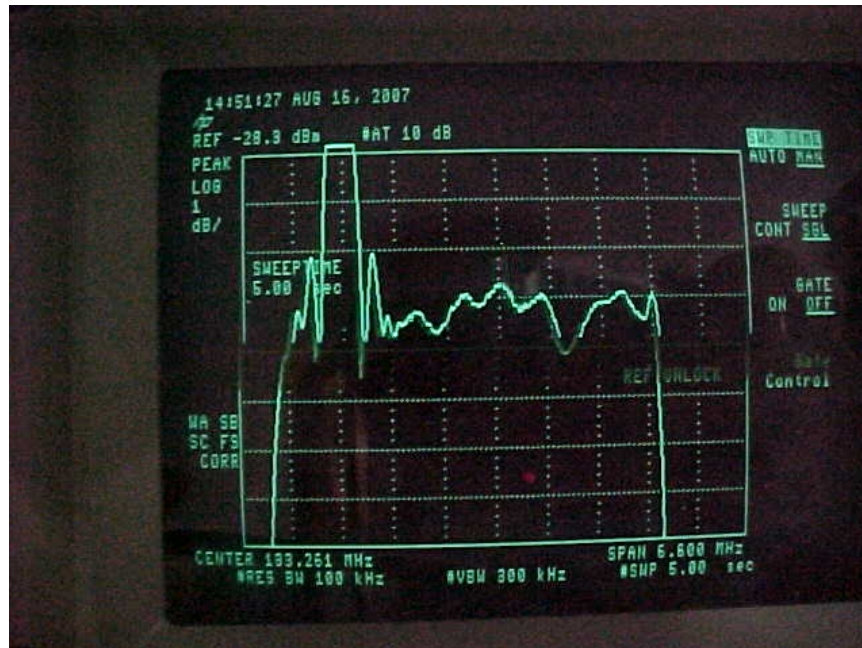


Figure 4-3. Graph of Detected Video Frequency Response

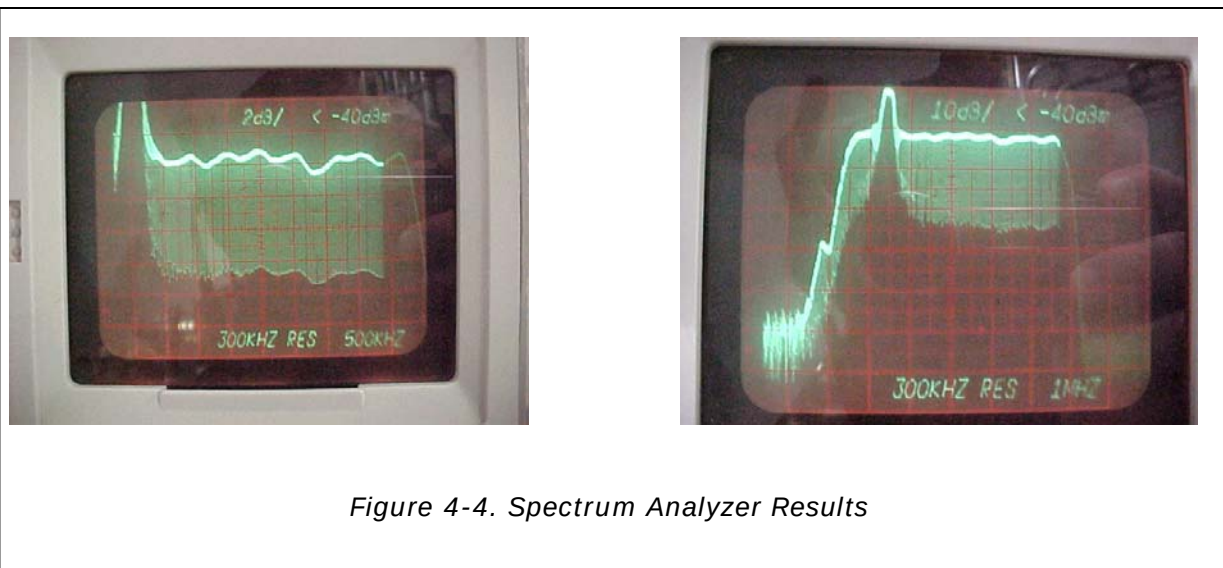
4.2.5 RF Sideband Response

The RF sideband response was recorded using the test setup shown in Figure 4-1. With the output power set to 100 watts peak of sync, the Tektronix Sideband Adapter was adjusted to provide a sweep test signal and the RF sideband response was recorded. Data from this test is provided in Table 4-3.

Photographs of the spectrum analyzer results are shown in Figure 4-4.

Table 4-3. RF Sideband Response

OUTPUT FREQUENCY (MHz)	VIDEO FREQUENCY	RESPONSES
181.25	Carrier	--
181.45	+200 KHz	0 (reference)
181.50	+250	-1.0
181.75	+500	-4.0
182.00	+750	-3.8
182.25	+1000	-3.8
183.25	+2000	-3.6
184.25	+3000	-4.4
185.25	+4000	-4.0
185.75	+4500	-22.0
186.00	+4750	-42.0
186.25	+5000	-50.0
181.00	-250	-1.2
180.75	-500	-4.2
180.50	-750	-4.5
180.25	-1000	-14.0
179.00	-1250	-34.0
179.75	-1500	-32.0
179.50	-1750	-36.0
179.25	-2000	-52.0
178.25	-3000	-54.0
177.67	-3580	-54.0
177.25	-4000	-54.0
176.25	-5000	-54.0
187.00	+5750	-54.0



4.2.6 Audio Modulation

Not Applicable - Unit under test is a translator.

4.2.7 AM and FM Noise

- Not Applicable - Unit under test is a translator.

4.3 Occupied Bandwidth

Using the test setup in Figure 4-6, with the transmitter operating at maximum power, photographs of the translator-occupied bandwidth spectrum were taken and are shown in Figures 4-7 and 4-8.

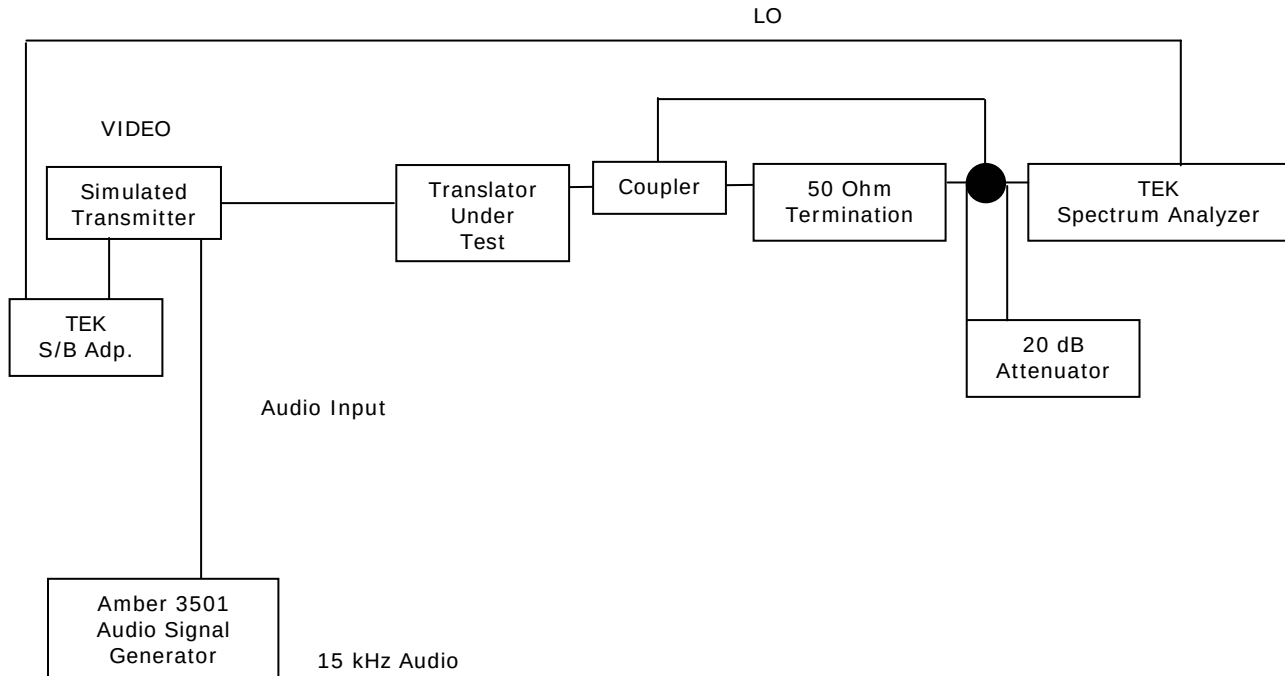


Figure 4-6. Test Setup for Occupied Bandwidth Spectrum Analysis

Note: Using the test procedure shown in Figure 4-1, the visual modulation was adjusted to 87.5% at white with the modulated staircase waveform and aural deviation adjusted to ± 25 kHz (100%) with the 400 Hz audio tone.

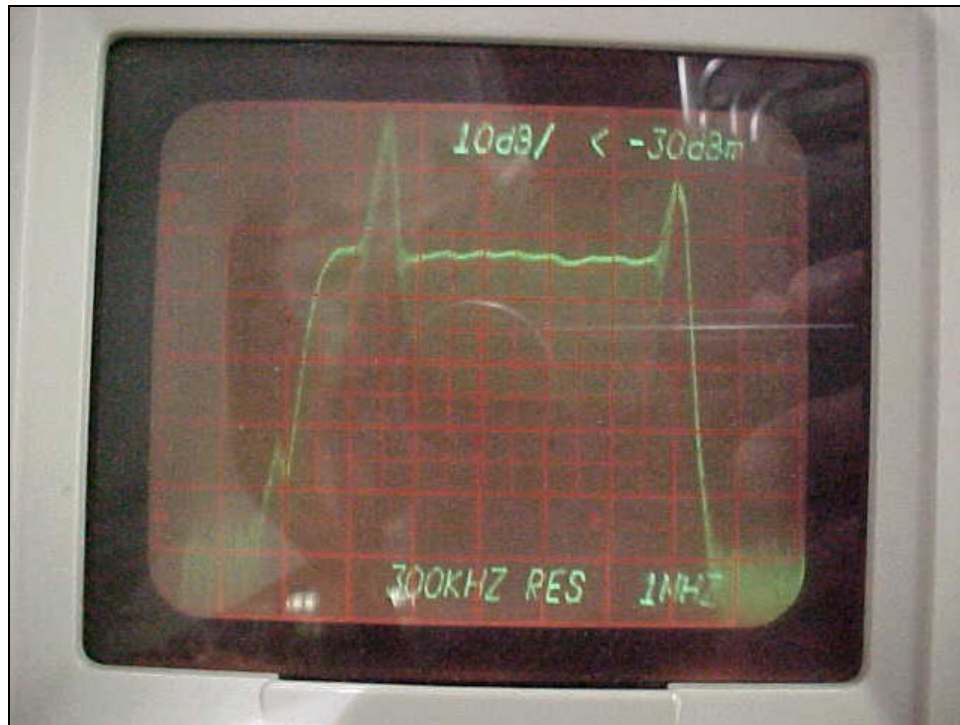


Figure 4-7. Channel-Occupied Bandwidth



Figure 4-8. Aural Carrier-Occupied Bandwidth

4.4 Conducted Spurious Emissions

Using the test setup shown in section 4.1, the spectrum outside of the specified channel was observed and the data was recorded on all products above the 70 dB noise floor of the spectrum analyzer. This data is shown in Table 4-6 and is presented as graphs in Figures 4-9 and 4-10.

Table 4-6. Products Above the 70 dB Noise Floor of the Spectrum Analyzer

FREQUENCY (MHz)	SOURCE	PEAK LEVEL OBSERVED (dB)
272.75	Image Visual Carrier	None observed
268.25	Image Aural Carrier	None observed
227.00	Local Oscillator	None observed
172.25	-9 MHz Product	None observed
176.75	-4.5 MHz Product	None observed
185.75	Aural Carrier	-10
181.25	Visual Carrier	0
188.45	+7.2 MHz Product	None observed
192.05	+10.8 MHz Product	None observed
190.25	+9 MHz Product	None observed
189.33	+8.08 MHz Product	None observed
186.67	+5.42 MHz Product	None Observed
177.67	-3.58 MHz Product	None Observed
371.50	Second Harmonic-Aural Carrier	None observed
362.5	Second Harmonic-Visual Carrier	None observed
557.25	Third Harmonic-Aural Carrier	None observed
543.75	Third Harmonic-Visual Carrier	None observed

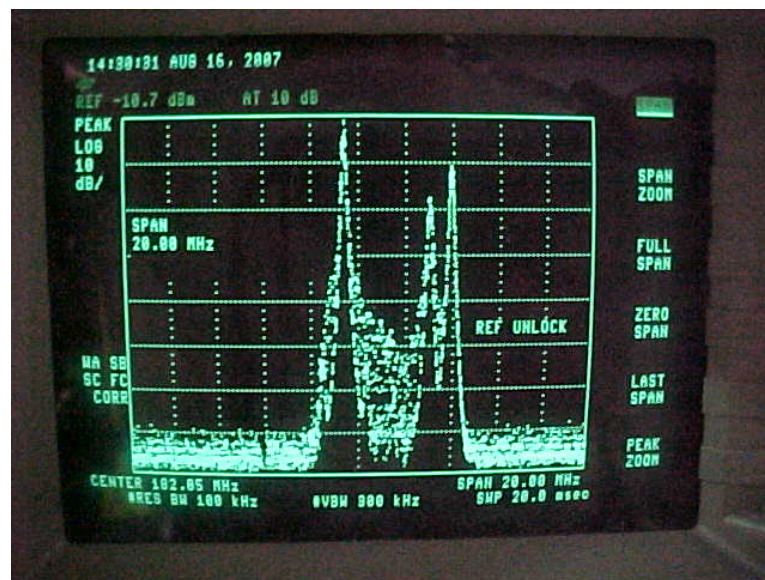


Figure 4-9. Products Above the 70 dB Noise Floor of the Spectrum Analyzer (1 of 2)

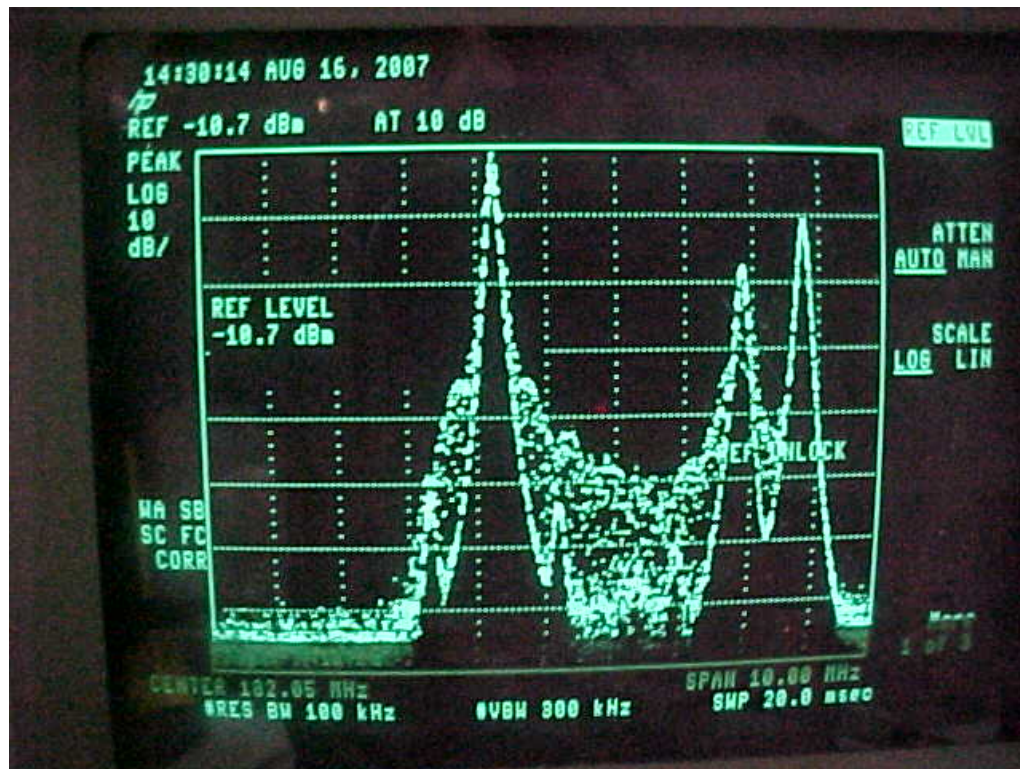


Figure 4-10. Products Above the 70 dB Noise Floor of the Spectrum Analyzer (2 of 2)

4.5 Radiated Emissions

Using the test setup shown in Figure 4-11, with the transmitter operating at full power, the spectrum analyzer was moved 20 meters from the transmitter and connected to a dipole antenna cut to 185 MHz. This antenna was oriented to maximize the received level and the data was recorded. The antenna was then cut to the local oscillator frequency and the second and third harmonic frequencies of the transmitter, and all of the signals received, were maximized by antenna orientation and their absolute levels were recorded.

With these various antennas, and with an adjustable length dipole for 40 to 600 MHz, the frequency spectrum from 40 MHz to 2,100 MHz was observed. The only measurable levels observed were at 181.25 and 185.75 MHz. These levels are shown below in Table 4-8 and an analysis of the relative field and strength are provided in the following paragraphs.

Table 4-8. Measurable Levels Observed in Frequency Spectrum

FREQUENCY	MEASURED LEVEL (INTO 50 Ω)
181.25	-45 dBm
185.75	-56 dBm

The spectrum analyzer had a maximum sensitivity of -110 dBm during these tests.

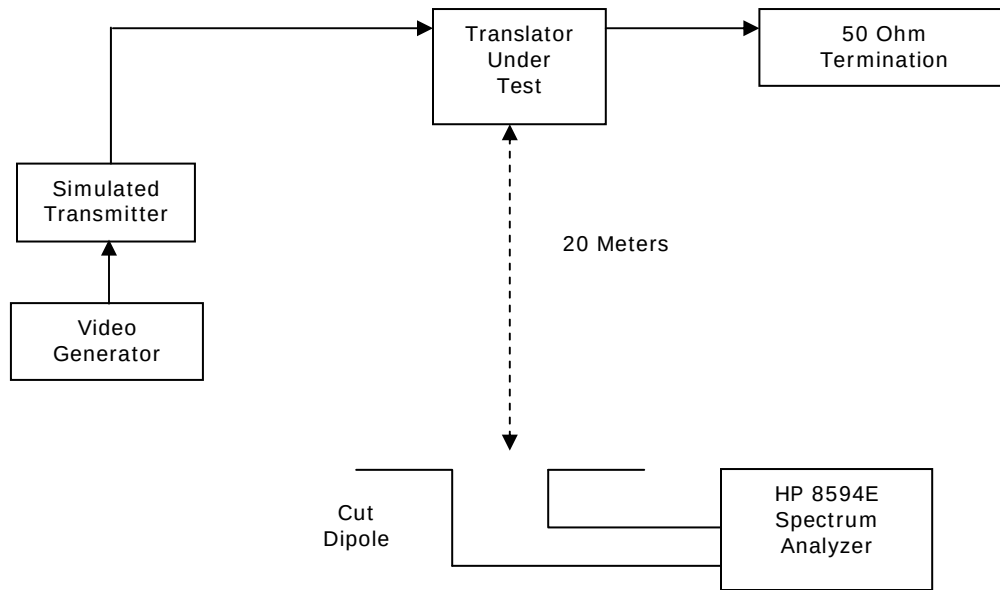


Figure 4-11. Test Setup for Measuring Radiated Emissions

Three levels were compared to the following reference level.

If all of the power of the translator was radiated by an isotropic radiator, the power density at 20 meters would be:

$$P = P_t / 4\pi R^2 = 100 / 4\pi \cdot (20)^2 = .02 \text{ w/m}^2$$

Using a dipole-transmitting antenna increases this by 1.64 to:

$$1.64 \times .02 = 3.3 \times 10^{-2}$$

If a dipole-receive antenna of area $1.64 \times \lambda^2 / 4\pi$ is used to receive the signal, the received level would be:

$$335 \text{ mw} = +25 \text{ dBm}$$

The receive levels at –45 dBm and –56 dBm were therefore at –70 dB and –81 dB relative to this level.

The receive levels were therefore at the relative levels shown in Table 4-9.

Table 4-9. Receive Levels

FREQUENCY	(REF = +25 dBm) RELATIVE MEASURED LEVEL
181.25	-70 dB
185.75	-81 dB

With the receive dipole cut to 181.25 MHz, the cabinet radiation was also checked, within very close proximity to the trays of the translator, and the received level that was recorded, and shown below, did not exceed a power density above of -10 dBm:

$$Pr/A = 0.01 \text{ mw/cm}^2$$

This level is far less than the current or proposed standard for safe radiation levels.

4.6 Frequency Stability

The LHV100AL is designed to operate using either an internal or external 10 MHz precise reference oscillator. The frequency stability of this reference determines the frequency stability of the transmitter.

The frequency determining variables of the transmitter may be defined as follows:

F_{LO1} = Desired local oscillator 1 frequency

F_{LO2} = Desired local oscillator 2 frequency

F_{IF} = Desired IF oscillator frequency

F_R = Desired external reference oscillator frequency

F_{RF} = Desired RF output frequency

E_{LO1} = Local oscillator 1 frequency offset error

E_{LO2} = Local oscillator 2 frequency offset error

E_{IF} = IF oscillator frequency offset error

E_R = External reference oscillator frequency offset error

E_{RF} = RF output frequency error

The PLL circuitry maintains a constant ratio between the external reference frequency and the output frequency of the oscillator. This ratio is defined below for both the LO and IF oscillators.

1

$$G_{LO1} = F_{LO1} / F_R$$

$$G_{LO2} = F_{LO2} / F_R$$

$$G_{IF} = F_{IF} / F_R$$

Any change in the external 10 MHz reference will effect a corresponding change in the output frequency such that the above ratios are maintained.

$$G_{LO1} = (F_{LO1} + E_{LO1}) / (F_R + E_R) = F_{LO1} / F_R$$

$$G_{LO2} = (F_{LO2} + E_{LO2}) / (F_R + E_R) = F_{LO2} / F_R$$

$$G_{IF} = (F_{IF} + E_{IF}) / (F_R + E_R) = F_{IF} / F_R$$

Solving for the change in output frequency yields:

$$E_{LO1} = E_R * (F_{LO1} / F_R) = E_R * G_{LO1}$$

$$E_{LO2} = E_R * (F_{LO2} / F_R) = E_R * G_{LO2}$$

$$E_{IF} = E_R * (F_{IF} / F_R) = E_R * G_{IF}$$

The desired RF carrier frequency is equal to the LO2 frequency minus the LO1 Frequency and the IF frequency:

$$F_{RF} = F_{LO2} - F_{IF} - F_{LO1}$$

The actual RF frequency, including any error introduced by the external reference, may be defined as follows:

$$\begin{aligned} F_{RF} + E_{RF} &= (F_{LO2} + E_{LO2}) - (F_{IF} + E_{IF}) - (F_{LO1} + E_{LO1}) \\ F_{RF} + E_{RF} &= (F_{LO2} - F_{LO1} - F_{IF}) - (E_{LO2} - E_{LO1} - E_{IF}) \\ F_{RF} + E_{RF} &= F_{RF} + (E_{LO2} - E_{LO1} - E_{IF}) \end{aligned}$$

Calculating for the error of the carrier yields:

$$\begin{aligned} E_{RF} &= (E_{LO2} - E_{LO1} - E_{IF}) \\ E_{RF} &= E_R (G_{LO2} - G_{LO1} - G_{IF}) \\ E_{RF} &= E_R / F_R * (F_{LO2} - F_{LO1} - F_{IF}) \\ E_{RF} &= E_R / F_R * F_{RF} \end{aligned}$$

Therefore, the error of the RF carrier is a function of the external 10 MHz reference error.

The maximum RF frequency error for this service is +/- 1.0 KHz. The highest channel frequency for this service (CH. 13 = 211.25 MHz) represents the worst case condition. With these values, the maximum allowable reference error ($E_{R(max)}$) can be calculated.

$$E_{R(max)} = 12.48 \text{ Hz}$$

The required reference oscillator stability may be calculated as follows:

$$\begin{aligned} \text{Stability} &= E_{R(max)} / F_R \\ \text{Stability} &= 12.48 \text{ Hz} / 10 \times 10^6 \text{ Hz} = 1.248 \times 10^{-6} \end{aligned}$$

Therefore, the RF frequency error of the translator will not exceed +/- 1.0 KHz when operated with a precise reference oscillator with a stability equal to or better than 1.248×10^{-6} .

The internal 10 MHz reference oscillator used in the translator has a stability of 1.000×10^{-6} (See included Crystek Crystals Corporation Datasheet, Part Number CXOH-APY-10.00) which insures a frequency stability within tolerance specified in the Rules and Regulations for this service.

Commercially available GPS precise reference oscillators, such as the TRACK Systems 8821, which has a frequency stability of 1×10^{-9} over a temperature range of 0 to 50 degrees C and a line voltage/frequency range from 85 to 265 VRMS/48 to 440Hz (See included TRACK Systems 8821 Specifications), insures a frequency stability within tolerance specified in the Rules and Regulations for this service.

Automatic Level Control Test

Using the test setup of Figure 4-1, the RF input level to the receiver tray was varied with Telsonic 5070-04 and 5010-02 step attenuators. The output level was monitored on the spectrum analyzer and recorded.

Table 4-13. Automatic Level Control Results

RF Input (dBm)	RF Output (dBm)
-62	Shut down (below receiver threshold)
-60	+49.6
-58	+49.7
-56	+49.8
-46	+50.0 (100 Watts)
-36	+50.2
-26	+50.3

4.8 Test Equipment

The test equipment that was used to analyze the Axcera LHV100AL system is listed in Table 4-14.

Table 4-14. Test Equipment

MODEL	MANUFACTURER	DESCRIPTION	SERIAL #
TSG95	Tektronix	Video Generator	10346
1450-1	Tektronix	Demodulator	10028
43	Bird	Power Meter	20060
100C	Bird	100W Power Meter VHF Element	N/A
8164	Bird	50 Ω Termination	11127
5253B	Hewlett-Packard	Frequency Counter	716-18295
VM-700A	Tektronix	Delay and Test Set	10911
ZFM-15	Mini-Circuits	Mixer	N/A
3501	Amber	Distortion Analyzer	20014
1405	Tektronix	Sideband Adapter	20159
7623A	Tektronix	Spectrum Analyzer	20092
8594E	Hewlett-Packard	Spectrum Analyzer	10118
5010-02	Telsonic	Step Attenuator	N/A
5070-04	Telsonic	Step Attenuator	N/A
1265-1300	Axcera	Exciter	N/A
2022-D	Marconi	Signal Generator	20069