

Appendix C

Measurements of Power, Modulation and Occupied Bandwidth, Spurious, Freq. Stability

Measured Test Data

The OA1900C NR NETWORK REPEATER was tested as required by 47 CFR 2.985 through 2.997, inclusive, in accordance with §2.999. The system was configured as follows:

- Two channels of CDMA (one each, Primary and Growth Enclosure),
- Reverse link Diversity,
- B-Block Diplex Filters,
- OEM handheld cellular phone and modem, required for remote network maintenance,
- Battery backup and battery charger board.

2.985 RF Power Output

Requirement

For the power levels expected, spurious signals including intermodulation distortion must meet industry and FCC requirements. The industry specification is published as ANSI J-STD-008 and ANSI J-STD-019 PCS CDMA Requirement. The FCC requirement is governed by 47 CFR 24.238.

Test Equipment

The following equipment was utilized:

1. HP E2507B Multi-format Communications Signal Simulator (MCSS), Model 60
2. HP 8563E Spectrum Analyzer, 9 kHz to 26.5 GHz
3. HP 437B Power Meter, with HP8481A sensor
4. HP 8491C Attenuator, 30 dB 'N'
5. Narda 768-30 Attenuator, 30 dB 'N' (two each)
6. Weinschel Egrg. 910-10-33 Continuously adjustable Attenuator, 1 to 10 dB

Test Method

In each direction, the repeater was driven with a two-channel CDMA test signal, to the rated output power of each channel, at mid-band frequency. In the system, the Channel 1 and Channel 2 forward outputs appear at different antenna connectors, so two traces of spectrum analyzer plots are shown on each page.

In the forward direction, the signal generator Walsh codes are set for the following signal, per industry standard:

Channel Name	Code Domain Channel Number	Relative Level, dB
Pilot	0	-7
Paging	1	-7.3
Traffic	8	-10.3
Traffic	9	-10.3
Traffic	10	-10.3
Traffic	11	-10.3
Traffic	12	-10.3
Traffic	13	-10.3
Sync	32	-13.3

In the reverse direction, the same signal is used except that Paging, Traffic, and Sync are turned off. Test frequencies are 80 MHz lower.

Spectral re-growth was checked for compliance with industry specification.

The input CDMA signal is then shifted to each of the frequency block edges. Measurement of spectral density due to IMD is measured in accordance with 47 CFR 24.238.

Test Results

Summarized as follows:

Direction	Frequency	Figure	Output Pwr., dBm	Requirement	Pass/Fail	Margin ¹ , dB
Forward	mid-block	P-1	+38.5	ANSI J-STD-008	PASS (ref. only)	2 dB (ref. only)
	Low-end of block	P-2	+38.5	47 CFR 24.238	PASS	-13 dBm -(-14 dBm) + 3.9 dB = 5 dB
	High end of block	P-3	+38.5	47 CFR 24.238	PASS	-13 dBm -(-14 dBm) + 3.9 dB = 5 dB
Reverse	mid-block	P-4	+18	ANSI J-STD-008	PASS (ref. only)	3 dB (ref. only)
	Low-end of block	P-5	+18	47 CFR 24.238	PASS	-13 dBm -(-36 dBm) + 3.9 dB = 27 dB
	high end of block	P-6	+18	47 CFR 24.238	PASS	-13 dBm -(-35 dBm) + 3.9 dB = 26 dB

Table P- 1
Output Power and Emissions

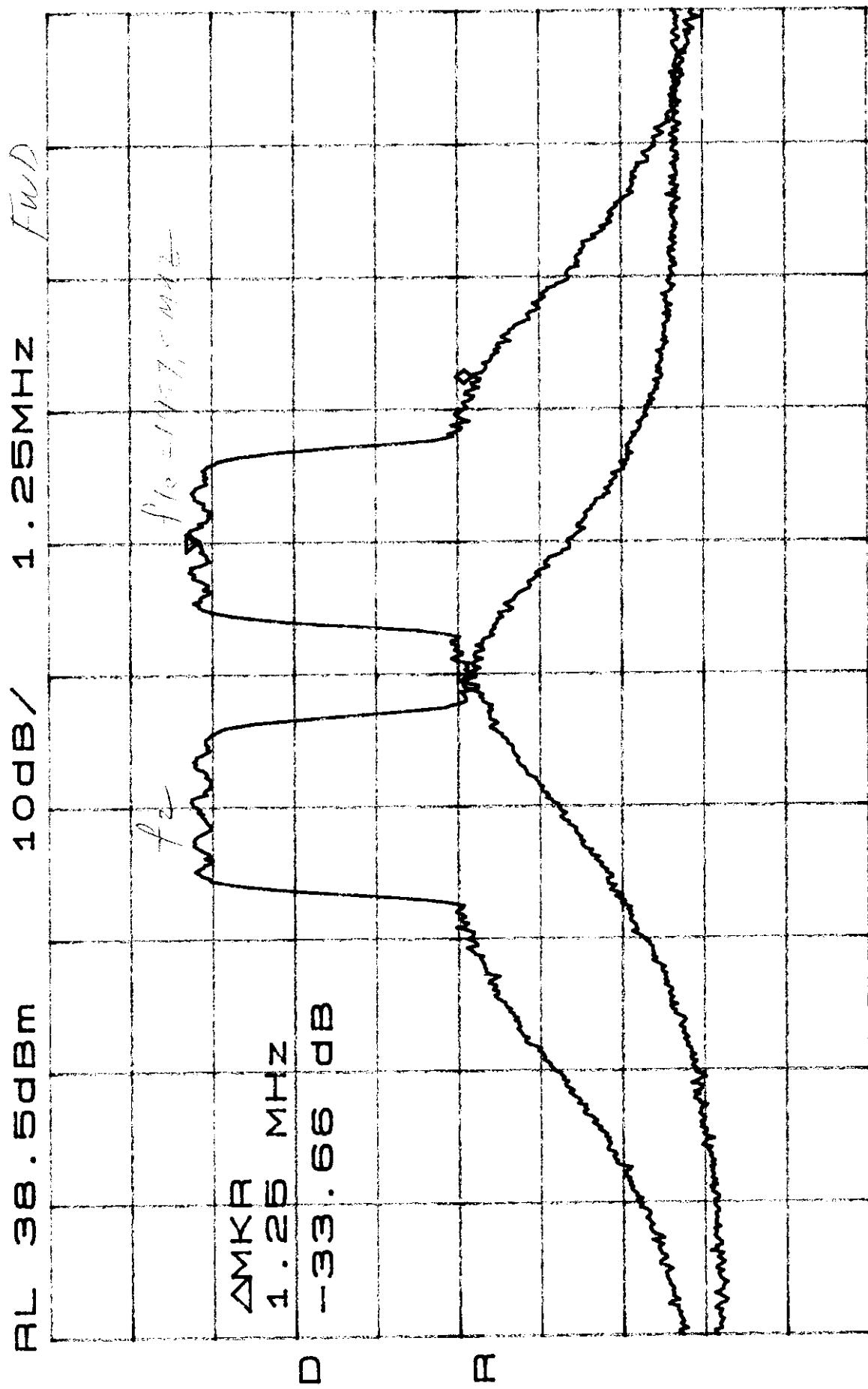
Conclusion: The two-channel OA1900C NR meets industry and FCC specifications for emissions, when transmitting at rated output.

¹ 47 CFR 24.238(b) only requires 1% minimum bandwidth for this measurement. For a 1.23 MHz CDMA signal, a 12.3 kHz minimum RBW filter would be necessary. Since spectrum analyzers are commonly available with RBW filters in 1-3-10 ratio, the 30 kHz filter was used. A correction factor of $10\log(30/12.3)=3.9$ dB is shown.

β_{5-6} - human infant growth protein

ANSWER - 33 : 66688

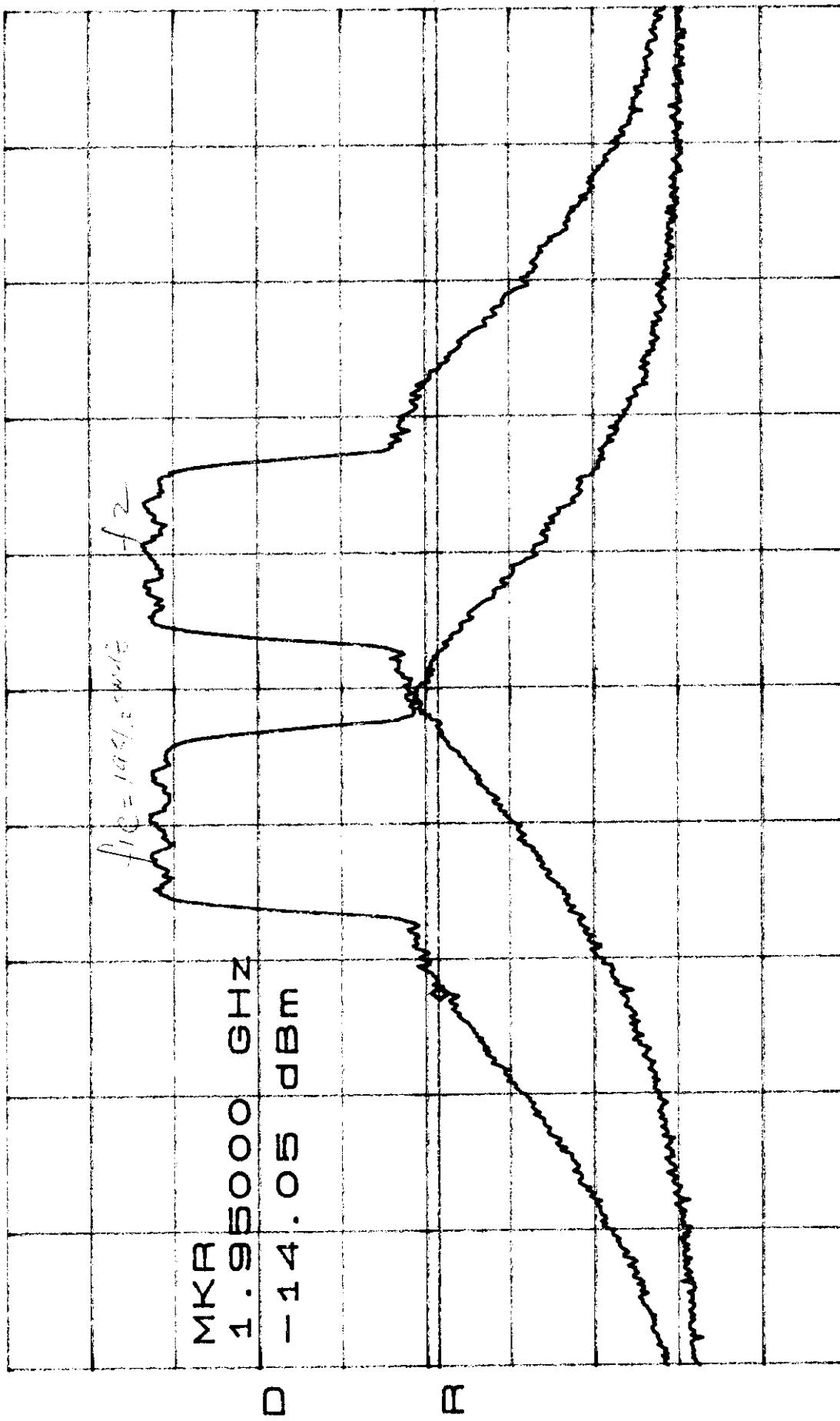
ATTEN 20dB
RL 38.5dB



CENTER 1.95650GHz *if Mid-band* SPAN 10.00MHz
 *RBW 30kHz VBW 100Hz SWP 8.40sec

ATTEN 20dB
RL 38.5dBm

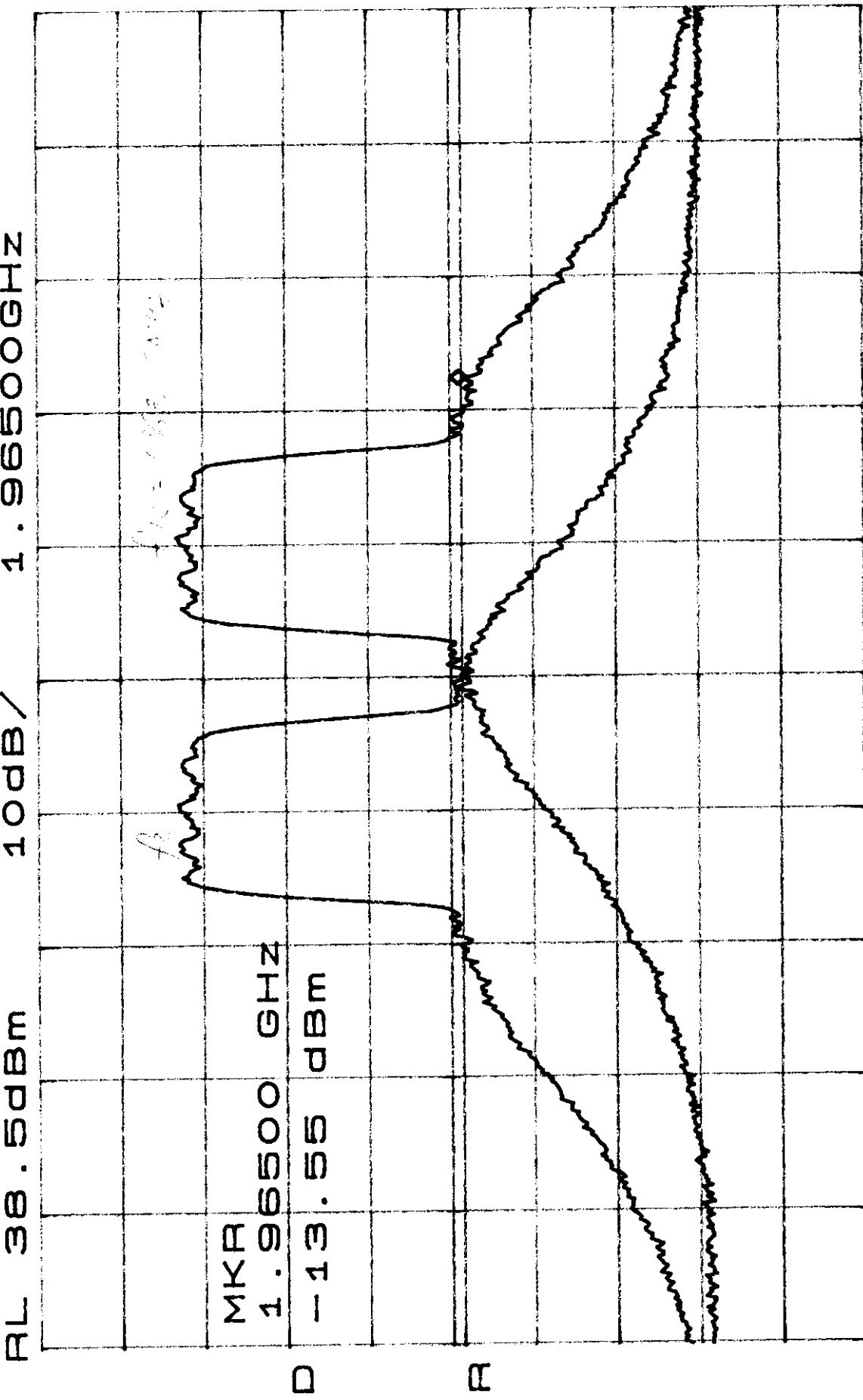
MKR -14.05dBm
1.95000GHz SWR



CENTER 1.95225GHz $f_{low} - f_{high}$ SPAN 10.00MHz
*RBW 30kHz *VBW 100Hz SWP 8.40sec

MKR - 13.55dBm *Ref*

ATTEN 20dB
B1 38.5dB

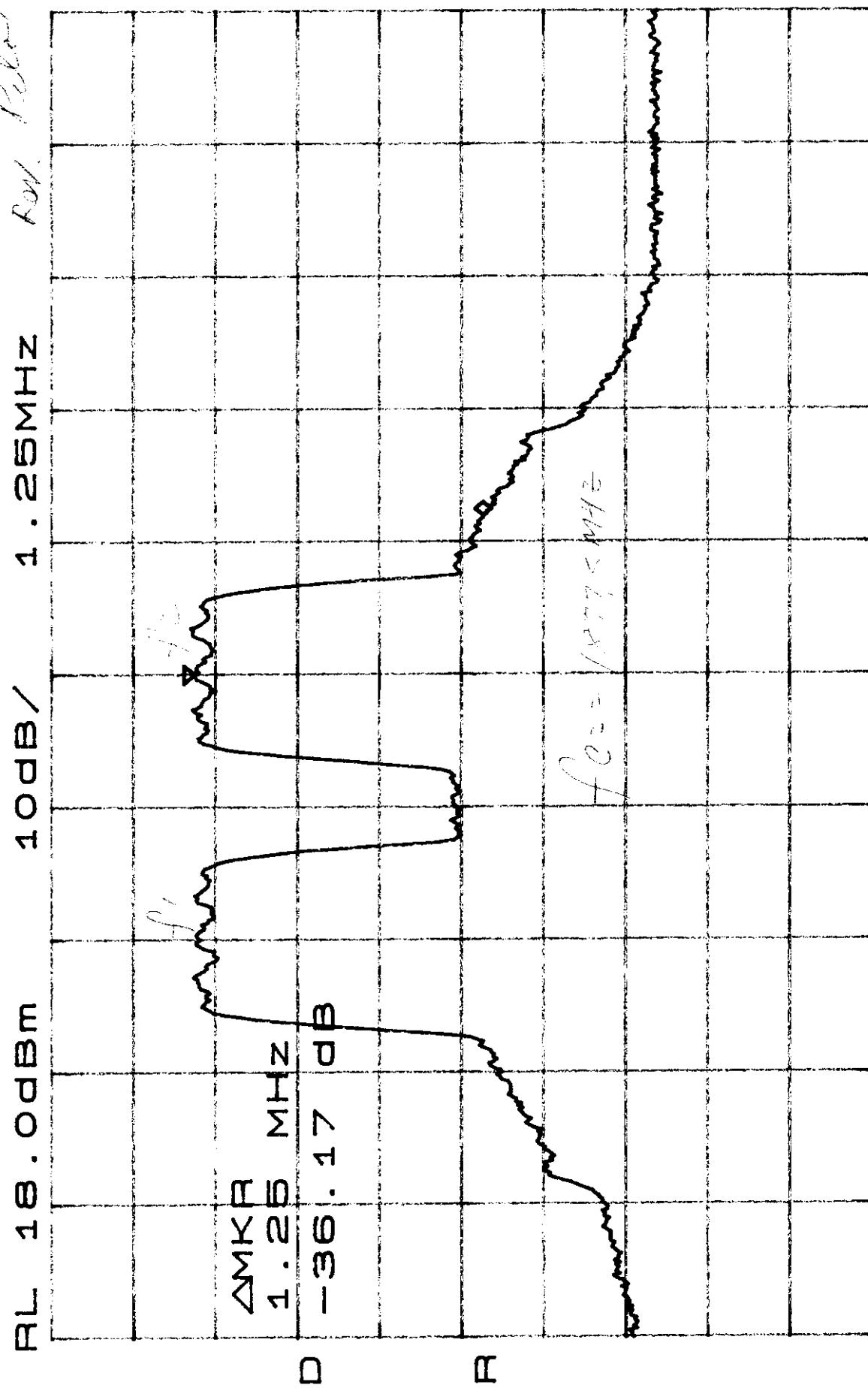


**BBW 30KHZ *VBW 100HZ SWP 8 : 40SEC CENTER 1 . 96275GHZ SPAN 10 . 00MHz

ATTEN 10dB
RL 18.0dBm

10dB/

AMKR -36.17dB



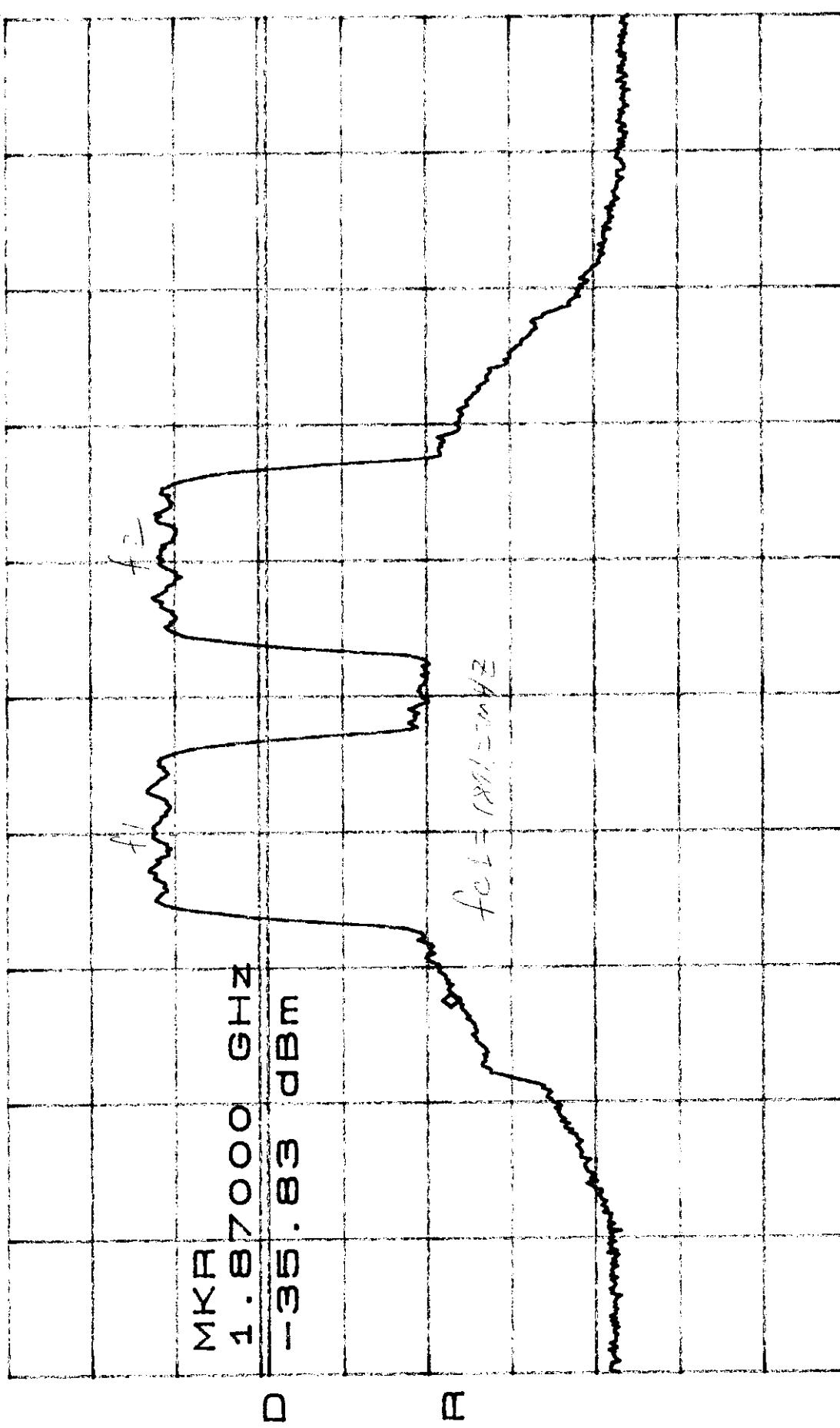
CENTER 1.87750GHz $f_{c1} = 877.50$ MHz SPAN 10.00MHz
*RBW 30kHz *VBW 100Hz SWP 8.40sec

B' block

ATTEN 10dB
RL 18.0dBm

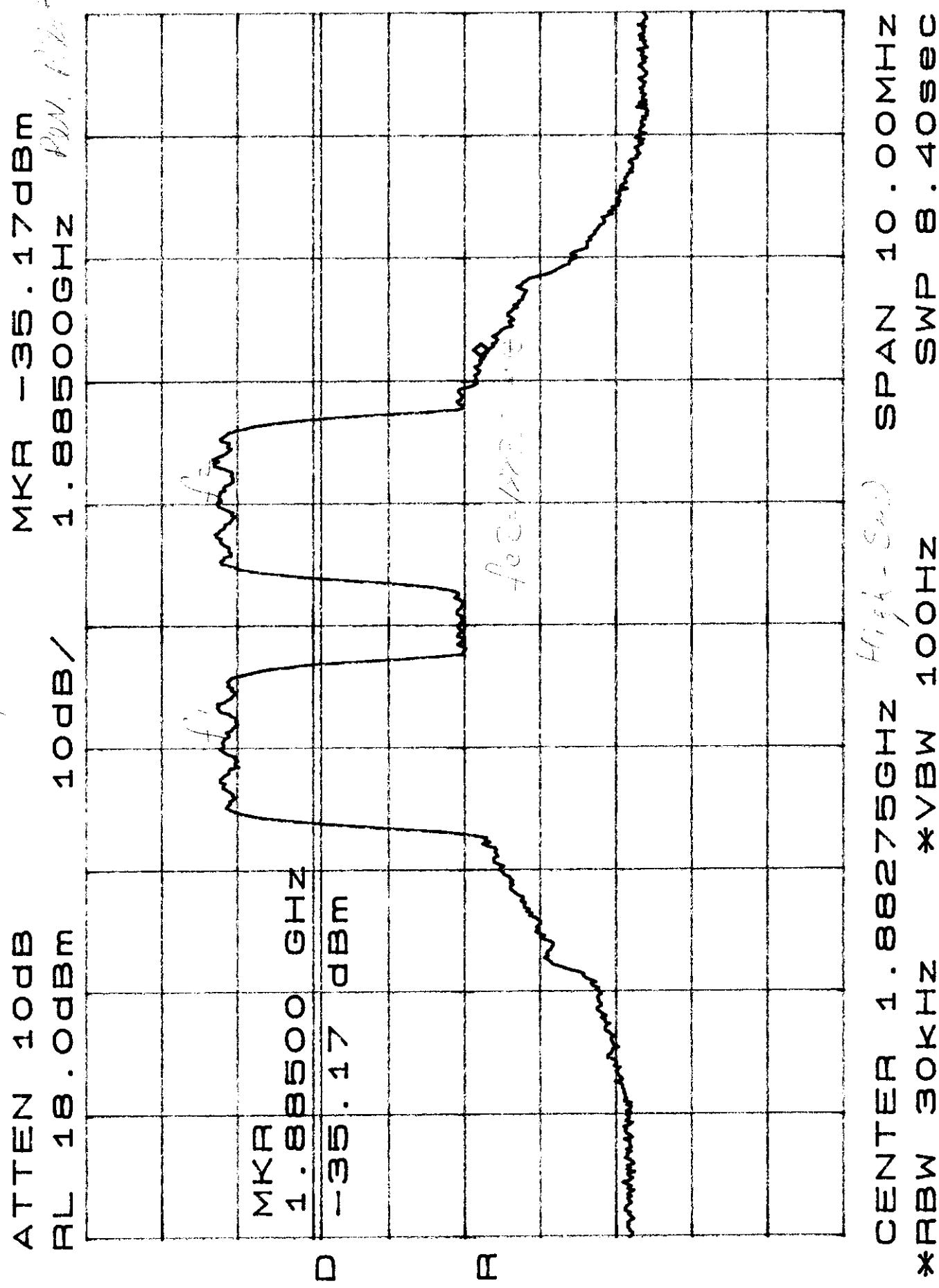
10dB /

MKR -35.83dBm
1.87000GHz



CENTER 1.872225GHz $f_{c1} = 1.87000$ SPAN 10.00MHz
*RBW 30kHz *VBW 100Hz SWP 8.40sec

Fig 15



Paragraph 2.987 Modulation Characteristics

Paragraph 2.989 Occupied Bandwidth

Requirements

A curve or equivalent data to show that the equipment will meet the modulation requirements of the rules under which equipment is to be licensed.

Test Method

The OA1900C NR repeater does not create any modulation of its own, only amplification of input signals occurs.

The test modulation used was the two-channel CDMA modulation format.

With the test signal applied to the main mobile antenna and the base antenna ports, the corresponding outputs were observed on a spectrum analyzer.

For each measurement direction, the transmitter was set to rated output power. A comparison of output spectrum to input spectrum was made.

Test Equipment

The following equipment was utilized:

1. HP E2507B Multi-format Communications Signal Simulator (MCSS), Model 60
2. HP 8563E Spectrum Analyzer, 9 kHz to 26.5 GHz
3. HP 437B Power Meter, with HP8481A sensor
4. HP 8491C Attenuator, 30 dB 'N'
5. Narda 768-30 Attenuator, 30 dB 'N' (two each)
6. Weinschel Egrg. 910-10-33 Continuously adjustable Attenuator, 1 to 10 dB

Test Results

Refer to Figures M-1 and M-2 for forward direction; Figures M-3 and M-4 for reverse direction.

The output signal spectrum as well as the input signal spectrum were recorded and compared. It was concluded that the two-channel OA1900 narrows the occupied bandwidth slightly. The output is within allowable limits.

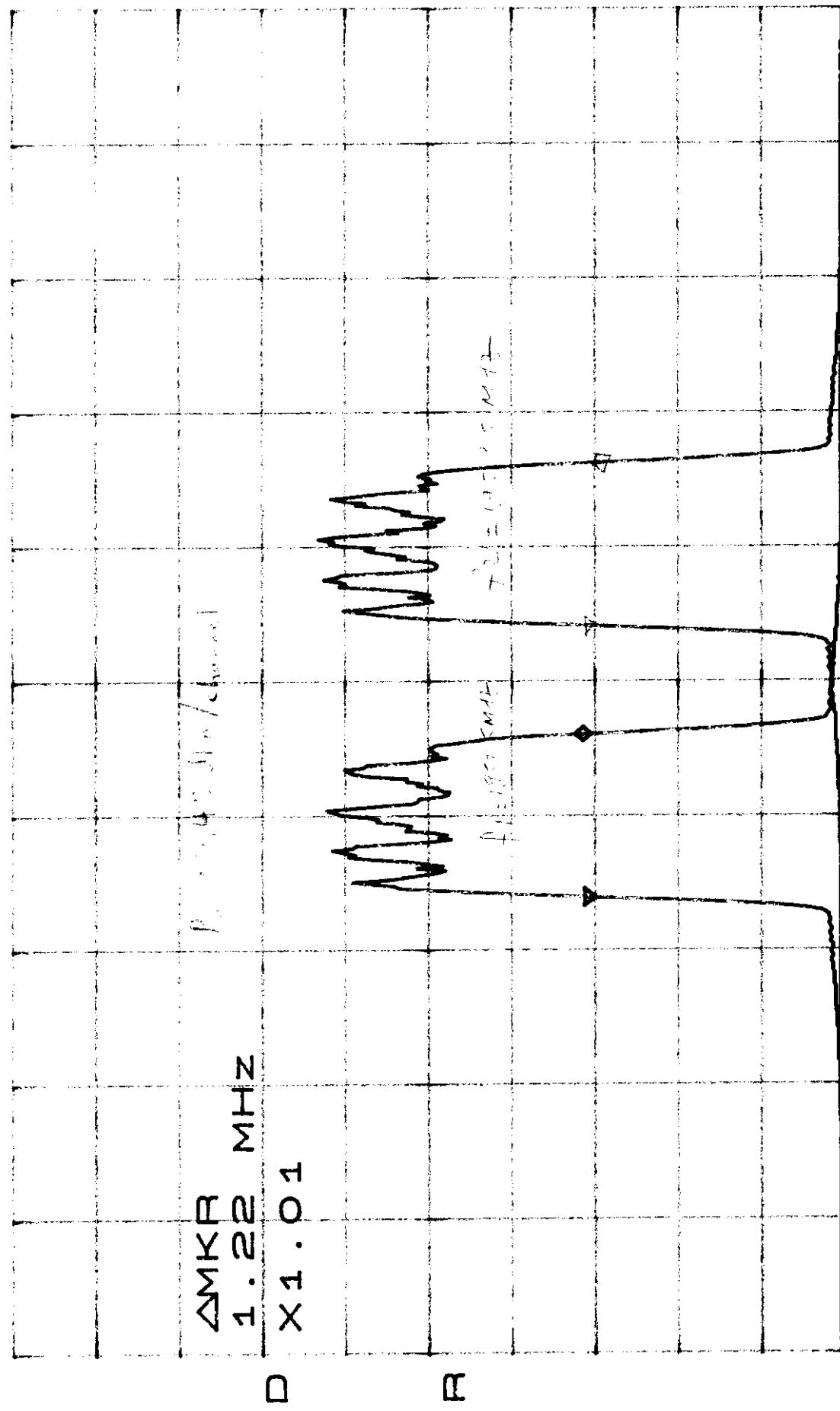
*ATTEN 10dB

RL 5.000V

ΔMKR X1.01

1.22MHz

LIN



CENTER 1.95850GHz

*RBW 30kHz *VBW 100MHz

SPAN 10.00MHz

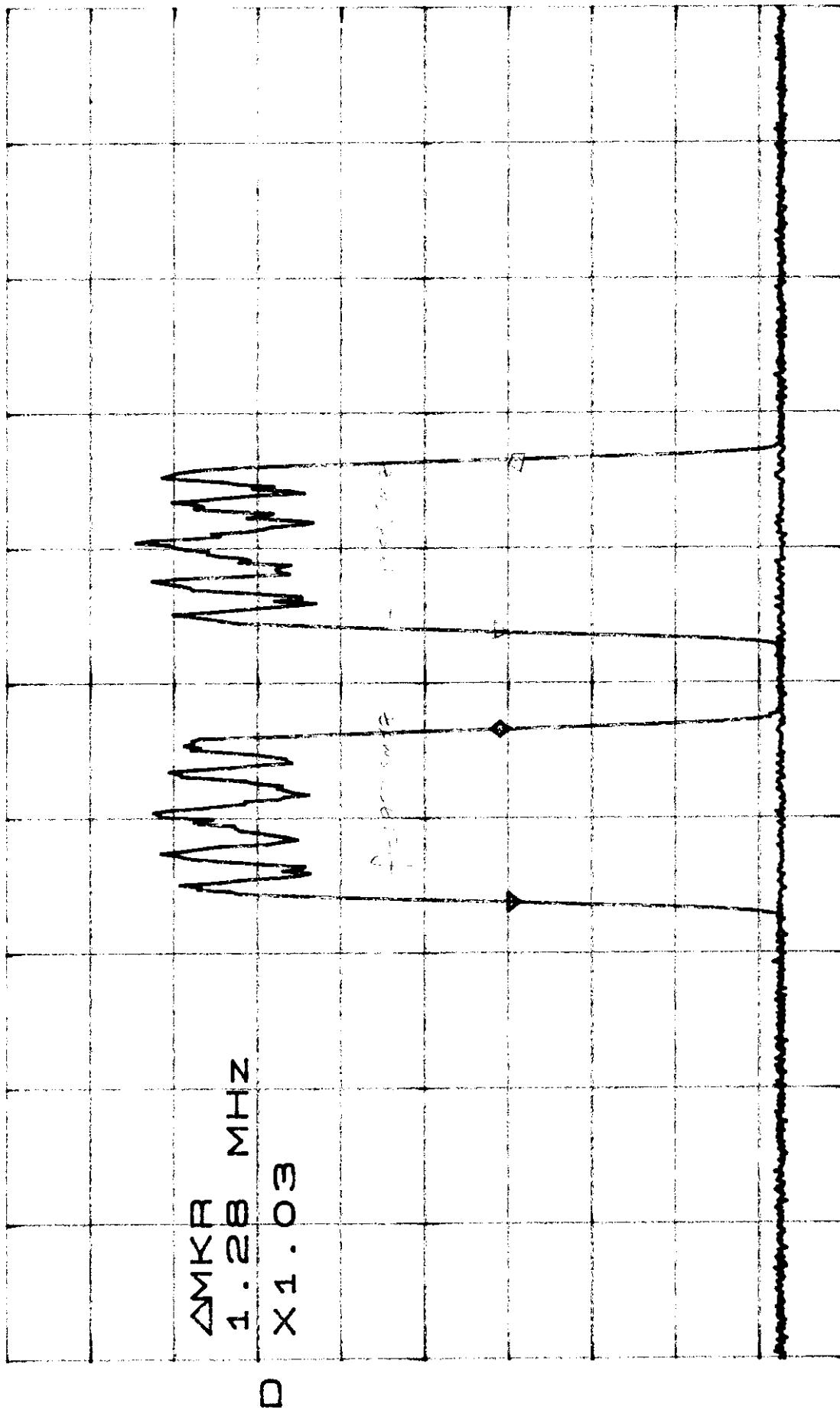
SWP 8.40sec

Surf

1.95850GHz

ATTEN 10dB
RL 59.98 mV

AMKAR X1.03
1.28MHz



*RBW 30KHz CENTER 1.95850GHz *VBW 400Hz

SPAN 10.00MHz
SWP 8:40sec

ATTEN 10dB
RL 299.9mV

ΔMKR X.99
1.22MHz

LIN

ΔMKR
1.22 MHz
X.99

D

R

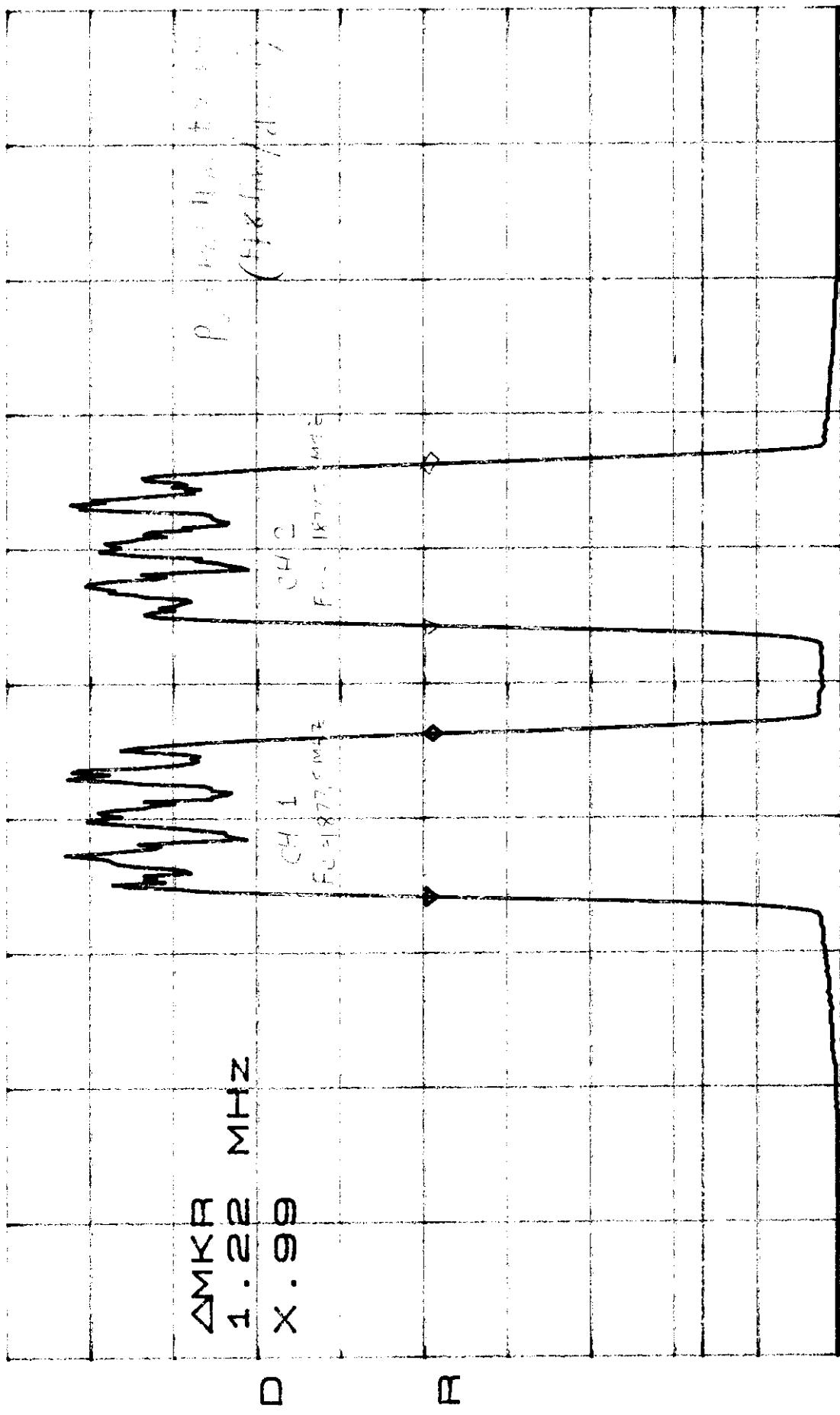


Fig. M-2

Output spectrum

ΔMKR × 1.03

1.32MHz

LIN

ATTEN 0dB

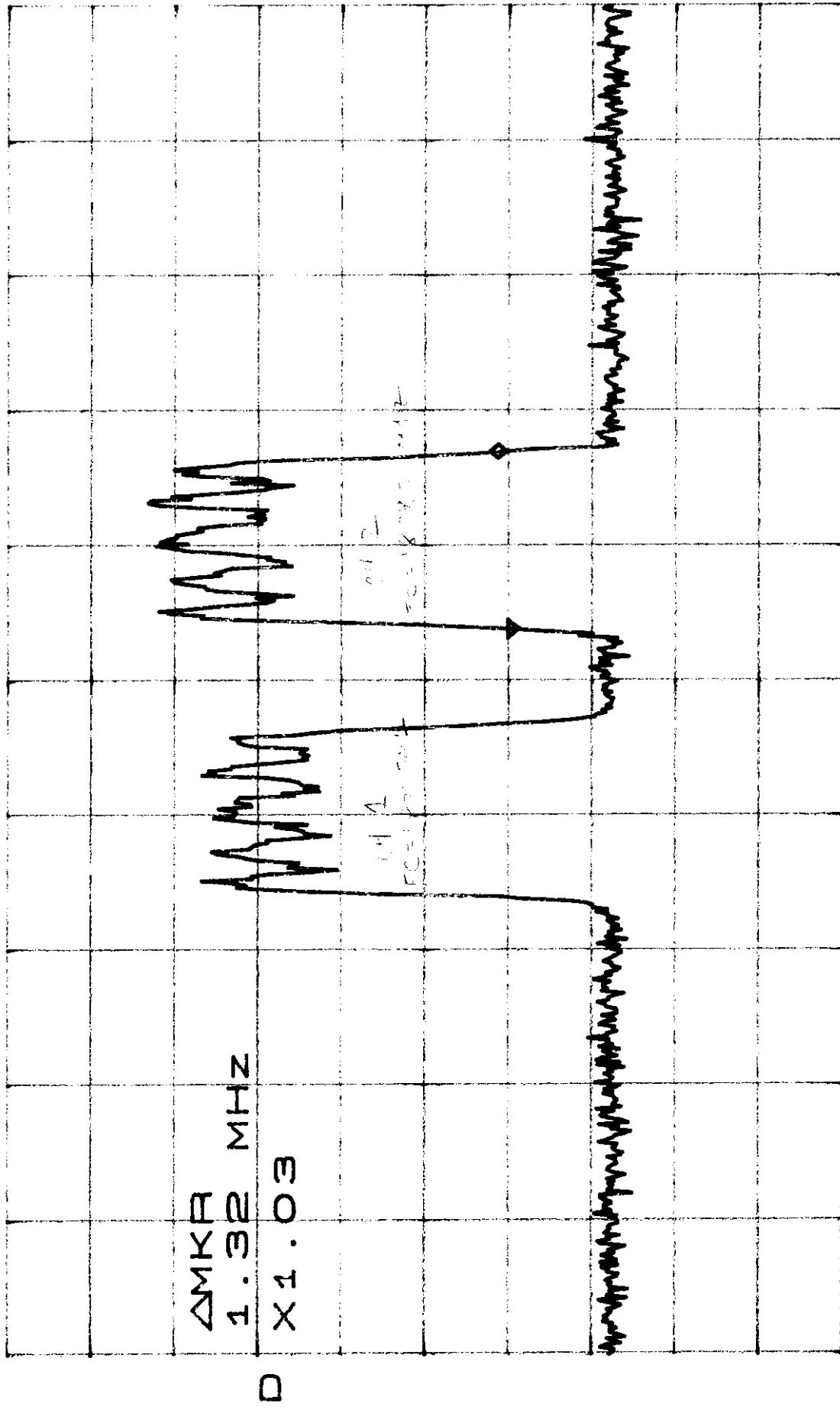


Fig. M-4

Paragraph 2.991 Spurious Emissions at the Antenna Terminals

Requirements

Under §2.991, the radio frequency power generated within the equipment and appearing on a spurious frequency shall be checked at the output terminals. The frequency range of the measurement is to include harmonics.

Section 24.238 (Broadband PCS) states that the spurious signal attenuation shall be at least $43 + 10\log(\text{output power})$, dB. The limit is -13 dBm.

Test Method

The two-channel OA1900 repeater system was operated with three 30 dB attenuators terminating each antenna port. Thus, the transmitters were each terminated into the design load impedance of 50 Ohms.

In each direction, the repeater was driven with a 2-channel CDMA signal source to full power, confirmed by the power meter.

A microwave spectrum analyzer was used to analyze each output port. Outputs were checked for spurious and/or harmonic signals, to a frequency of ten times the fundamental transmit frequency. In the Forward direction, the spectrum analyzer's reference level offset was set to the value of the output attenuator.

Test Equipment

The following equipment was utilized:

1. HP E2507B Multi-format Communications Signal Simulator (MCSS), Model 60
2. HP 8563E Spectrum Analyzer, 9 kHz to 26.5 GHz
3. HP 435B Power Meter, with HP8481A sensor
4. HP 8491C Attenuator, 30 dB 'N'
5. Narda 768-30 Attenuator, 30 dB 'N'
6. Weinschel Egrg. 910-10-33 Continuously adjustable Attenuator, 1 to 10 dB

Test Results

Figures CE-1 and CE-2 show the forward transmit spectrum that emanates from main and diversity mobile antenna ports, respectively.

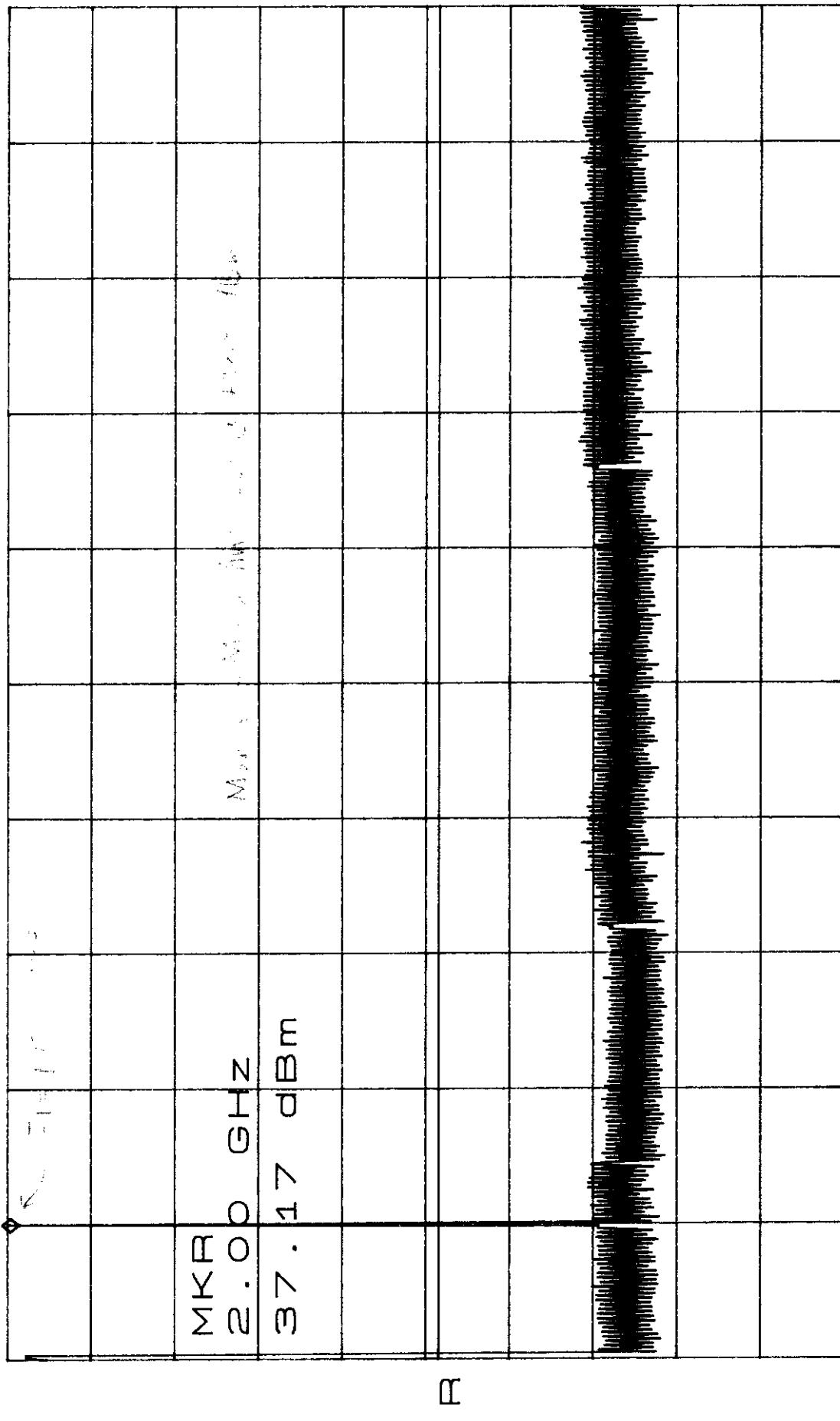
Figure CE-3 shows the transmit spectrum that gets transmitted to the base.

The noise floor of the spectrum analyzer and its automatic internal band changing are visible. The only spur visible is on the reverse direction plot, about 23 dB below the FCC threshold.

The OA1900C NR complies with FCC rules and regulations for conducted spurious emissions.

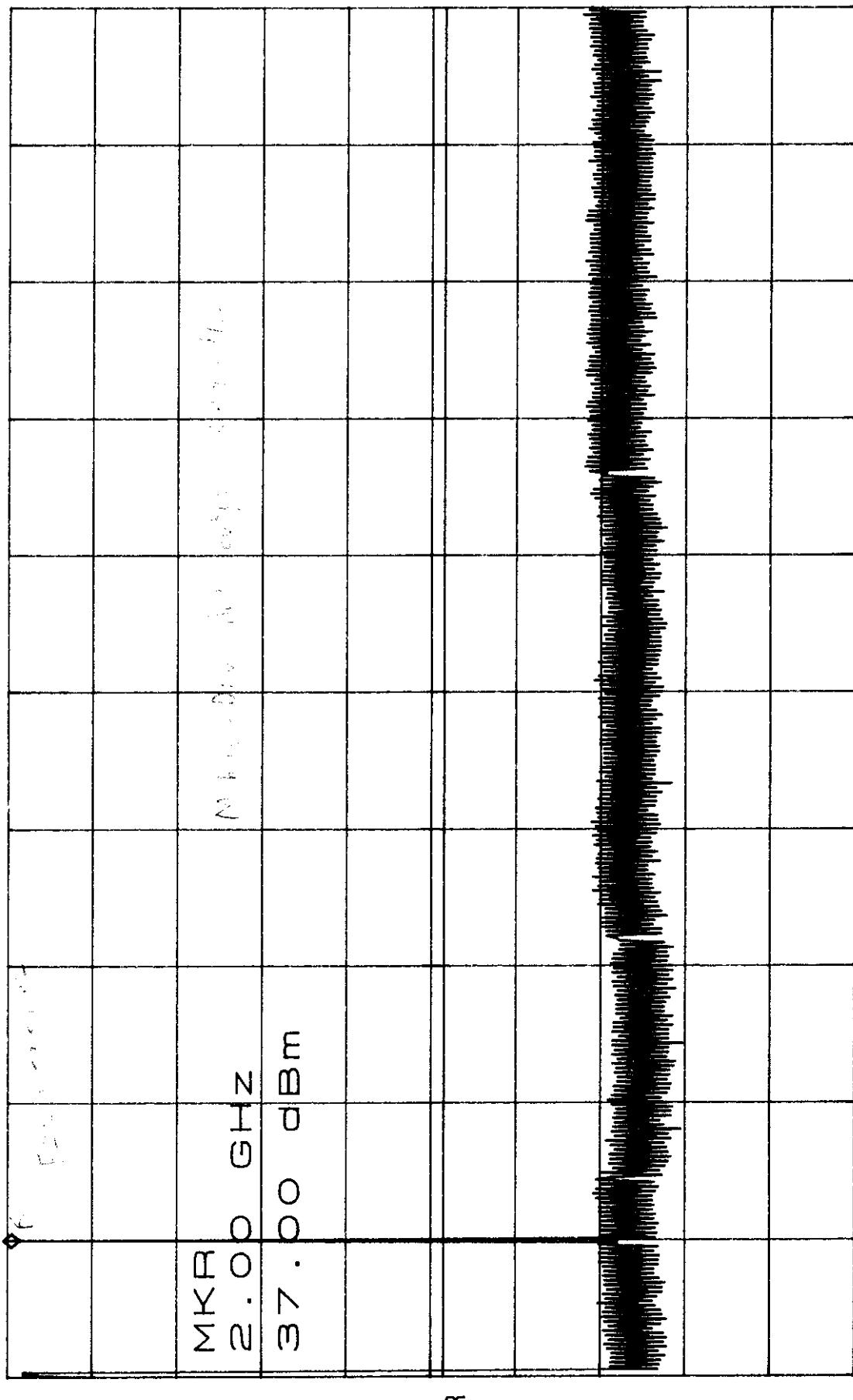
ATTEN 20dB
RL 38.5dB

MKR 37.17dBm
2.00GHz



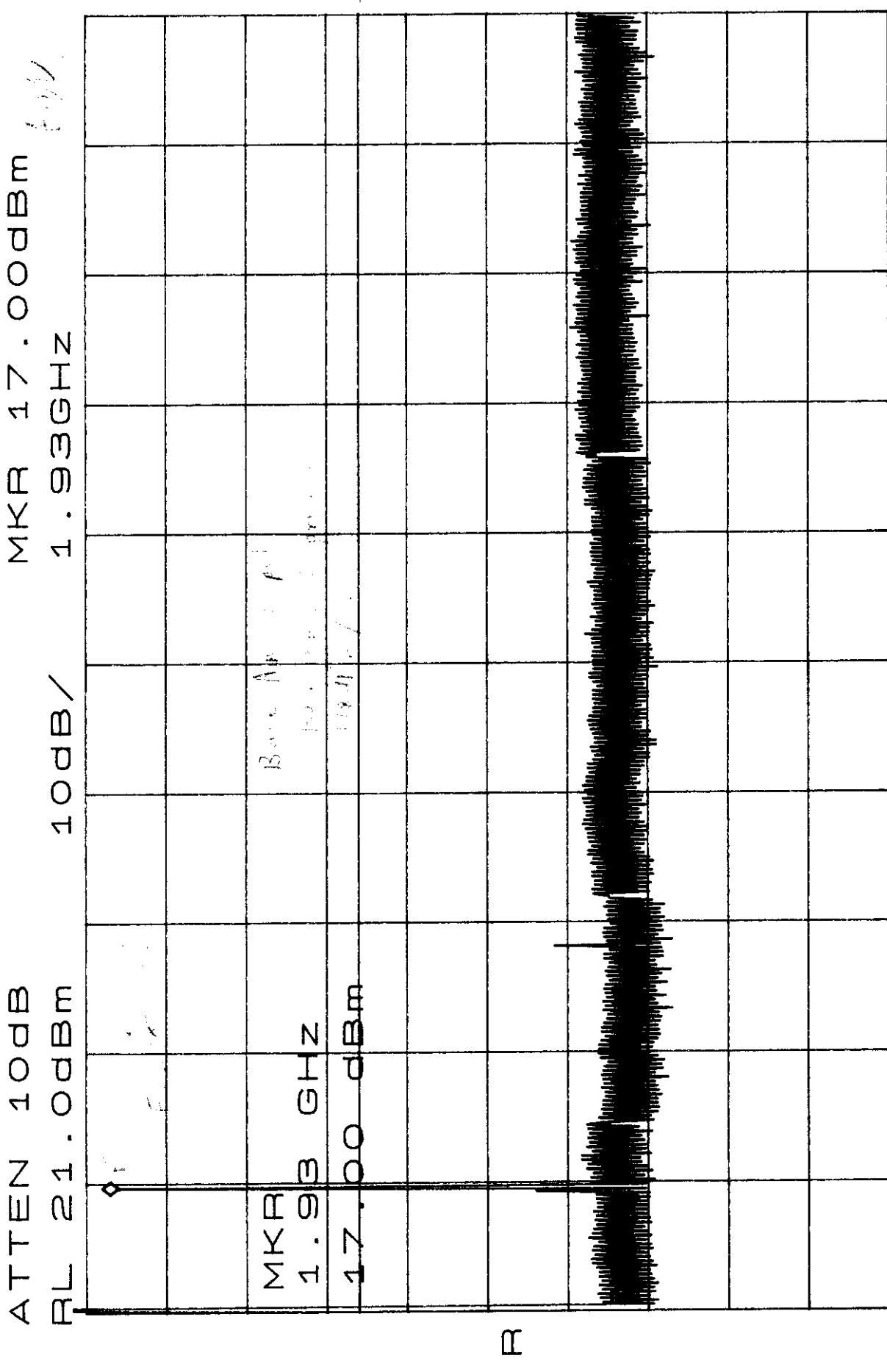
START 0Hz
RBW 1.0MHz *VBW 30kHz SWP 1.70sec
STOP 20.00GHz
MKR 37.17dBm
2.00GHz

ATTEN 20dB
RL 38.5dBm



START OHZ
RBW 1.0MHz *VBW 30kHz SWP 1.70sec

ATTEN 10dB
RL 21.0dBm



MKR 17.00dBm
1.93GHz

START 0Hz
RBW 1.0MHz *VBW 30kHz SWP 1.70sec

Fig. 6E-3

Paragraph 2.993: Field Strength of Spurious Emissions

Requirements

The OA1900C NR is to be measured for spurious emissions, to a frequency of at least 10 times the rated output frequency. All spurious and harmonic signals are to be less than that which would be received by a -13 dBm transmitter into a $\frac{1}{2}$ wave dipole, at the same distance as the DUT.

Test Method

The test location was a sheltered outdoor area between the building and the parking lot. The OA1900C NR REPEATER was operated with 2-channel forward traffic at 7 Watts/channel, and 2-channel reverse traffic at +18 dBm/channel, both directions simultaneously. RF Attenuators (30 dB) were connected to all three antenna ports.

A spectrum analyzer with suitable antennas was used as the test receiver. The antennas are listed below. Transmission line loss, between the measurement antenna and test receiver (spectrum analyzer), was entered into the spectrum analyzer as a reference level offset.

A sweep generator was used as a -13dBd signal source. A trace of the spectrum analyzer was used to record the amplitude of the substitution source across the frequency band. This result can be seen on the graphs as the wavy line above the measurement, roughly corresponding to the display line level. The display line is set to a calculated level, based on -13dBd minus path loss + RxAntennaGain – TransmissionLineLoss.

The test antenna was manually positioned with respect to DUT azimuth, elevation, and polarization, to maximize any spurious signals into the test receiver.

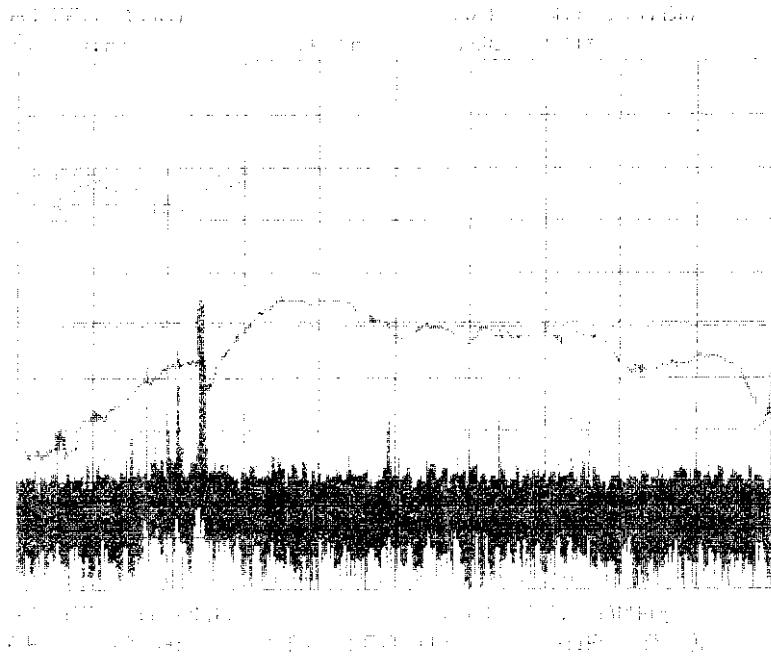
The following frequencies were used:

Forward direction: 1952.0 and 1954.0

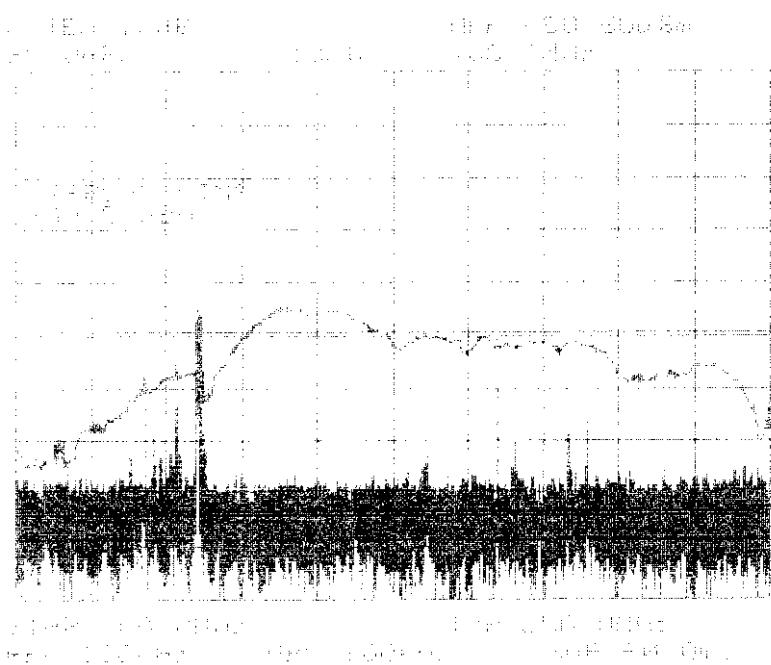
Reverse direction: 1872.0 and 1874.0

Freq. Band		Calculation method, based on path loss						Substitution method					
Figure number	Freq range	Freq for calc of path loss, MHz	Base power level into dipole, dBm	Dist. DUT to Rx antenna, m	Free Space path loss, dB	Measurement	Rx antenna gain, dBi	Max Allowed power level into dipole, dBm	Cable loss	Cable loss driving substitution	Gain of antenna, dBm	Tx Power into antenna, dBm (sweeper out, Level)	
RE-1	8 to 10 GHz	9000	-13	1	51.5	Electro-Metrics Horn, Double-ridged, RGA-60	12	6' RG-142	4	-52.5	-13	Coax to waveguide transition	
RE-2	5.5 to 8 GHz	7000	-13	1	49.4	Electro-Metrics Horn, Double-ridged, RGA-60	10.9	6' RG-142	3.5	-51.5	-13	Coax to waveguide transition	
RE-3	4 to 5.5 GHz	5500	-13	1	47.3	Electro-Metrics Horn, Double-ridged, RGA-60	10.5	6' RG-142	3	-49.8	-13	Coax to waveguide transition	
RE-4	3 to 4 GHz	4000	-13	1	44.5	Electro-Metrics Horn, Double-ridged, RGA-60	9.4	6' RG-142	2.5	-48.1	-13	Coax to waveguide transition	
RE-5	1 to 3 GHz	2000	-13	1	38.5	Electro-Metrics Horn, Double-ridged, RGA-60	7.5	6' RG-142	2	-44.0	-13	Coax to waveguide transition	
RE-6	0.5 to 1.0 GHz	900	-13	1	31.5	Watkins-Johnson Log-Periodic Discone, with low-freq. extension	5	6' RG-142	1	-39.5	-13	Coax to waveguide transition	
RE-7	250 to 500 MHz	400	-13	3	34	Watkins-Johnson Log-Periodic Discone, with low-freq. extension	4	5' RG-58	1	-43.0	-13	Coax to waveguide transition	
RE-8	60 to 250 MHz	200	-13	3	38.5	Whip. Diamond D-Discone, with low-freq. extension	2	5' RG-58	0.5	-49.5	-13	Coax to waveguide transition	
RE-9	25 to 60 MHz	38	-13	3	24	Whip. Diamond D-Discone, with low-freq. extension	-5	5' RG-58	0	-42.0	-13	Coax to waveguide transition	

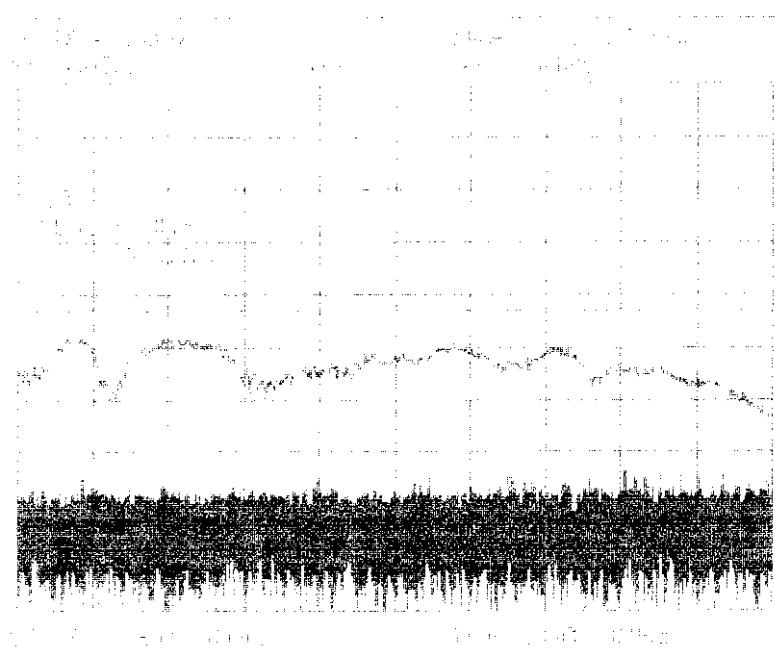
radiated.xls



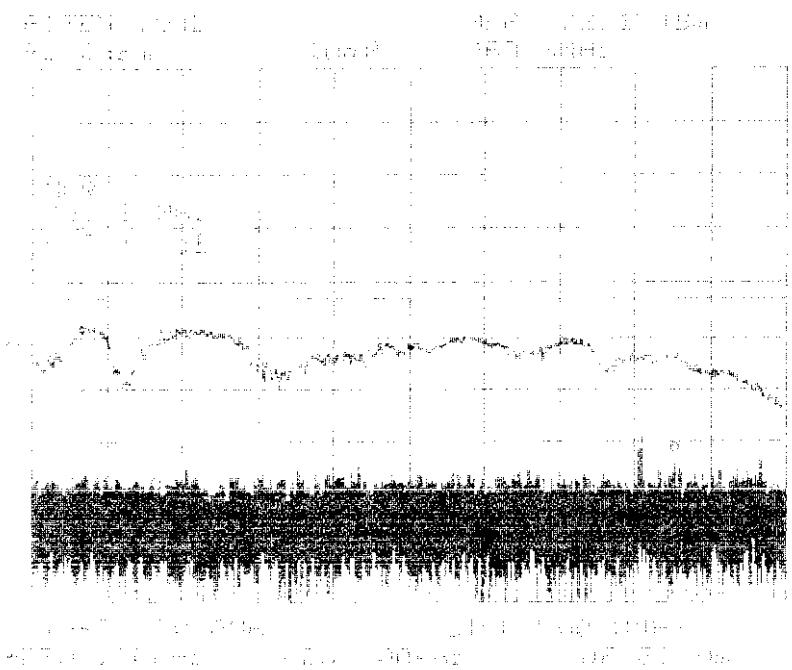
$\text{CH}_2^+ \text{ ON}$



$\text{CH}_2^+ \text{ OFF}$



Rpt. ON



EEG 117

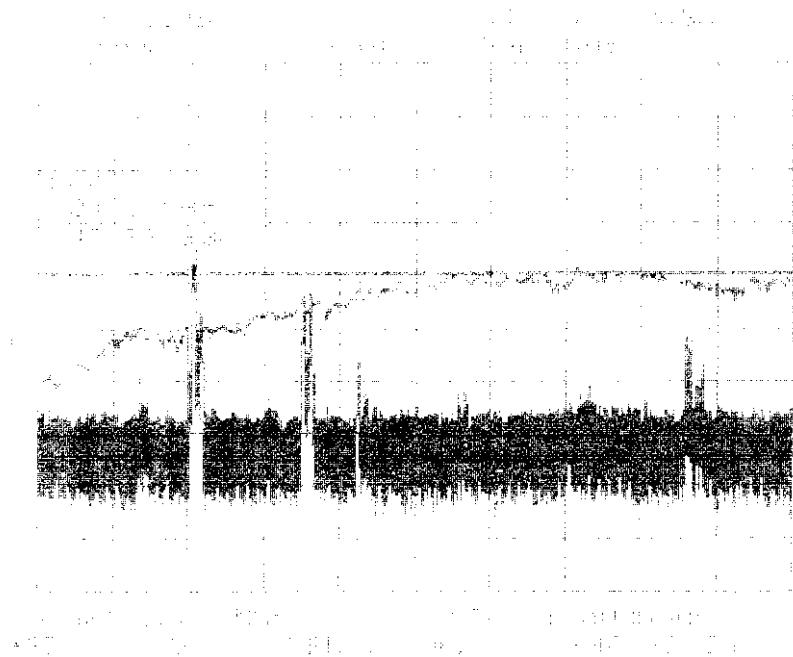


Fig. 2

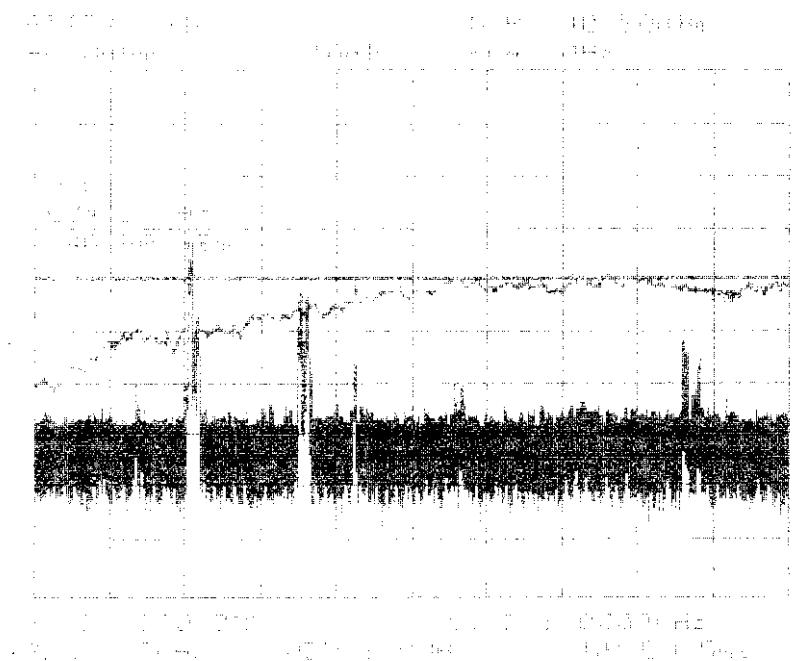
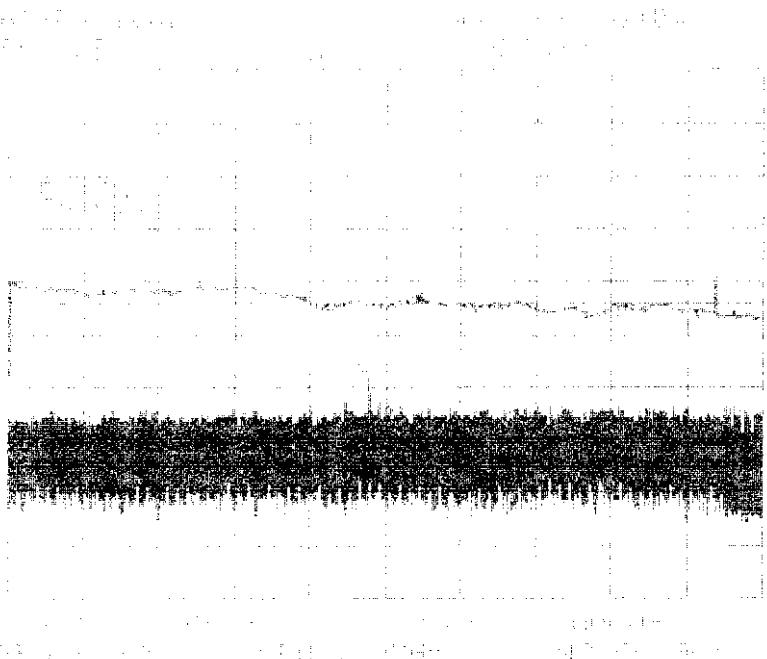
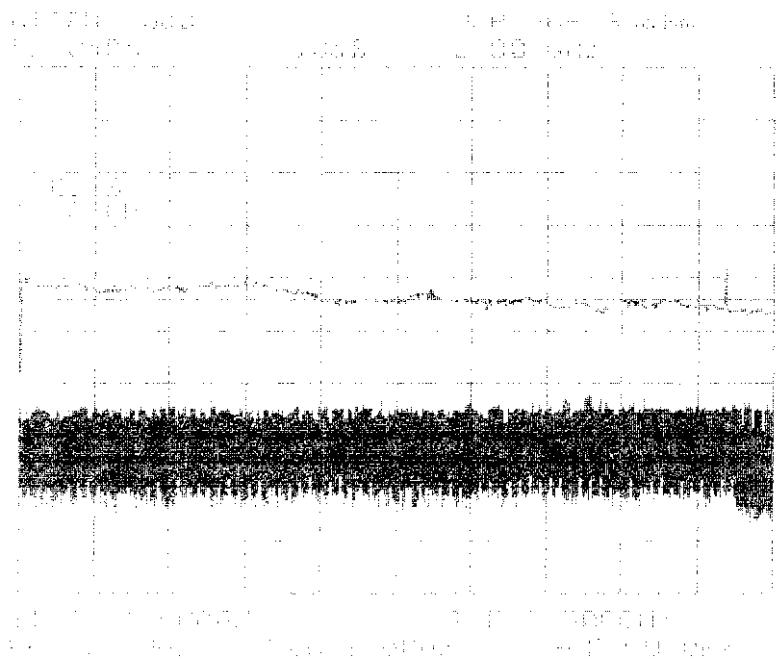


Fig. 4

1000



R_f , ON



R_f , OFF

1000 800 600 400 200

JOURNAL OF CLIMATE

19. *U. S. Fish. Comm.*, 1874, p. 111.

10

2000

LITERACY AND WORKERS

27

OFF

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1. The first step in the process of creating a new product is to identify a market need. This involves research into consumer behavior, market trends, and competitor analysis. The goal is to find a gap in the market that can be filled by a new product.

2. Once a market need is identified, the next step is to develop a product concept. This involves defining the product's features, benefits, and target audience. The product concept should be unique and differentiate it from existing products in the market.

3. The third step is to create a product prototype. This involves developing a physical or digital representation of the product. The prototype should be functional and reflect the product concept.

4. The fourth step is to test the product prototype. This involves conducting user testing and gathering feedback from potential consumers. The feedback is used to refine the product prototype and address any issues or concerns.

5. The fifth step is to manufacture the product. This involves finding a manufacturer who can produce the product in the required quantity and quality. The manufacturer should be able to meet the production timeline and budget.

6. The sixth step is to launch the product. This involves creating a marketing plan, setting a launch date, and launching the product to the market. The marketing plan should include promotional activities, pricing, and distribution channels.

7. The seventh step is to monitor and evaluate the product's performance. This involves tracking sales, customer feedback, and market trends. The performance data is used to make informed decisions about the product's future.

8. The eighth step is to refine and improve the product. This involves addressing any issues or concerns that arise during the product's life cycle. The goal is to continuously improve the product and maintain its relevance in the market.

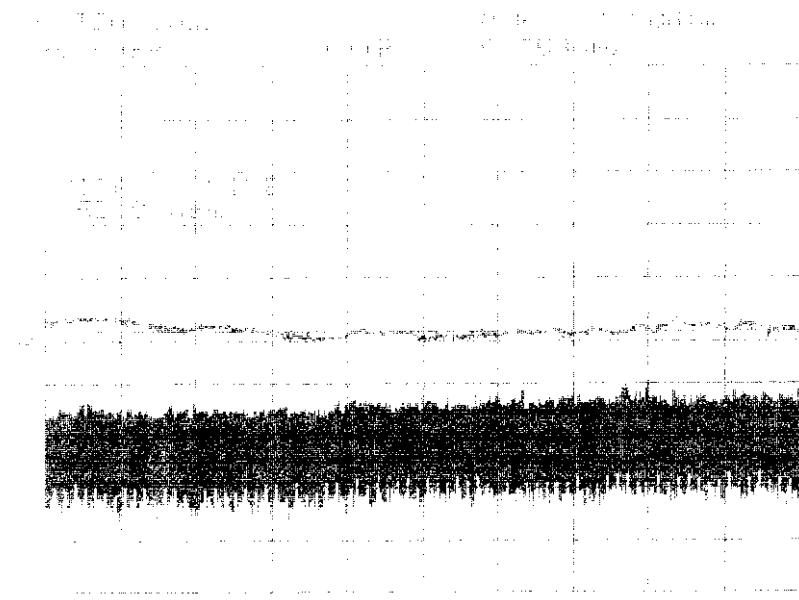
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OFF

FEBRUARY 1955

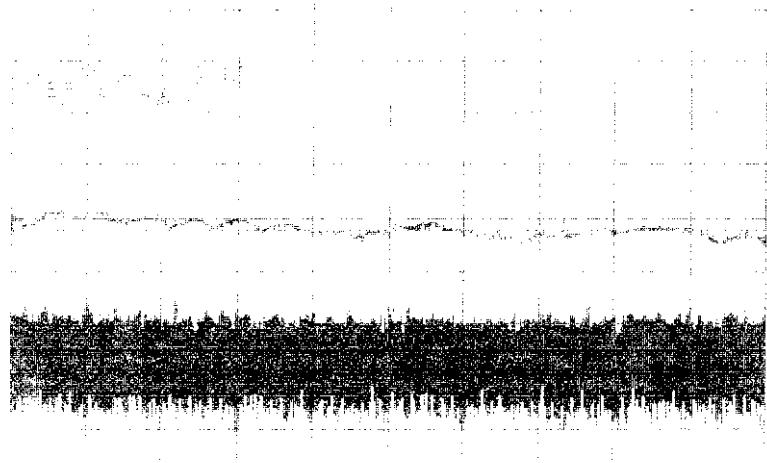


$R_p + \sigma N$

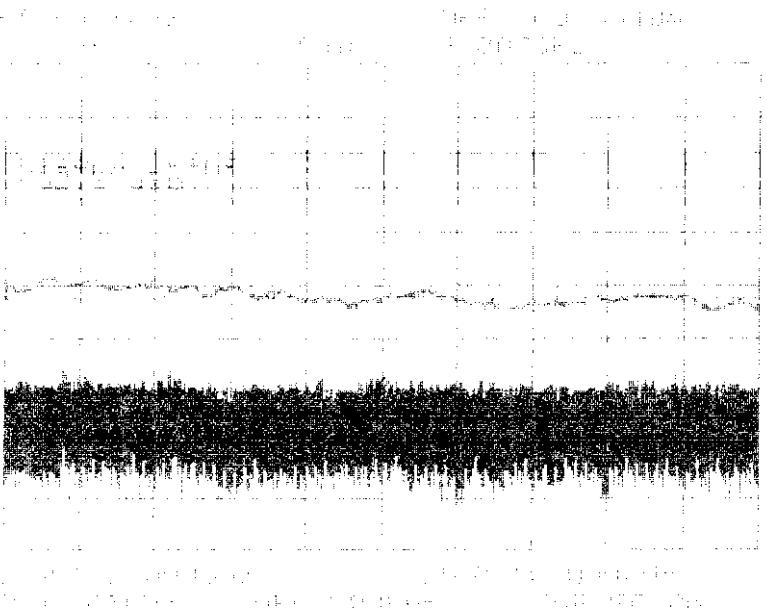


$R_p + \sigma F$

$F = \sigma F + 2$



Ref. ON



Ref OFF

Ref ON

Paragraph 2.995 Frequency Stability

Requirements

The output frequencies of the OA1900C NR repeater system are to be measured vs. primary power supply voltage and variations in temperature. The primary power supply voltage is varied over 85 to 115 % of nominal. The temperature is varied from -30 degree C to +50 degree C.

Section 24.235 states that the freq. stability shall be sufficient to ensure that the fundamental emission stays within the authorized frequency block.

Test method

The repeater system under test was put in a temperature chamber and a variable power source was used to power the DUT. Input signal was from the signal generator, whose 10 MHz reference input was supplied by the high stability timebase of the counter. Over the temperature and line voltage ranges of interest, frequency error was calculated from input and output frequency measurements of the second channel Growth Enclosure. Both forward and reverse measurements were made.

Because the OA1900C NR Off-Air repeater is a linear amplifying device, exactly zero Hertz freq. error is expected. This is always true because the same Local Oscillator that mixes input down to IF is used to mix IF back up to output frequency.

Test Equipment

Signal Generator:	HP 83620A
Frequency Counter:	HP 53131A
Attenuators:	MaCom 30 dB and Narda 766-30
Variable AC power source:	B&K Precision 1655 AC Power Supply
AC Voltmeter	Fluke 8060A multimeter with true rms
Temperature Chamber	Thermotron S-32

Test Signals

For the forward test, a CW signal of 1,877.500 000 MHz was used. For the reverse test, a CW signal of 1,957.500 000 MHz was used.

Test Results

Refer to Table FS-1 for test results.

The OA1900C NR Repeater exhibits zero Hz. freq. error and meets FCC requirement.

Test Equipment

Item	Description	Usage
HP 83620A	Synthesized Sweep Signal Generator, 10 MHz to 20 GHz	Substitution signal source
HP 8563E	Spectrum Analyzer, 9 kHz to 26.5 GHz	Measurement receiver
Narda 768-30	Attenuator, 30 dB, 20 Watt	2 ea., use to terminate each port and inject signals
HP 437B and HP 8481A	Power meter and power sensor	Use to set power levels
HP E2507B, Model 60	Multi-format Communications Signal Simulator (MCSS)	Generate forward traffic signals
HP 8935	CDMA Base Station Test Set	Use to generate one channel reverse traffic
Anritsu MG3670B	Digital Modulation Signal Generator	Use to generate one channel reverse traffic
Antennas	See table	Various receive and substitute transmitter antennas

Test Results

Measurements were taken with the repeater DUT turned on, and then off, for comparison.

Each of the RE-1 through RE-9 graphs shows three curves:

1. a display line at the power calculated to correspond with FCC limit of -13 dBd,
2. a stored trace that represents the substitution signal generator's received level,
3. the actual measurement from the DUT.

In all graphs, the actual measurement from the DUT is well below either of the thresholds. Therefore, radiated spurious emissions are FCC compliant.

Ambient Temp.	Line Voltage, Vrms					
	95	100	110	117	125	135
-30	0	0	0	0	0	0
-20	0	0	0	0	0	0
-10	0	0	0	0	0	0
0	0	0	0	0	0	0
10	0	0	0	0	0	0
20	0	0	0	0	0	0
30	0	0	0	0	0	0
40	0	0	0	0	0	0
50	0	0	0	0	0	0
55	0	0	0	0	0	0

Table FS - 1

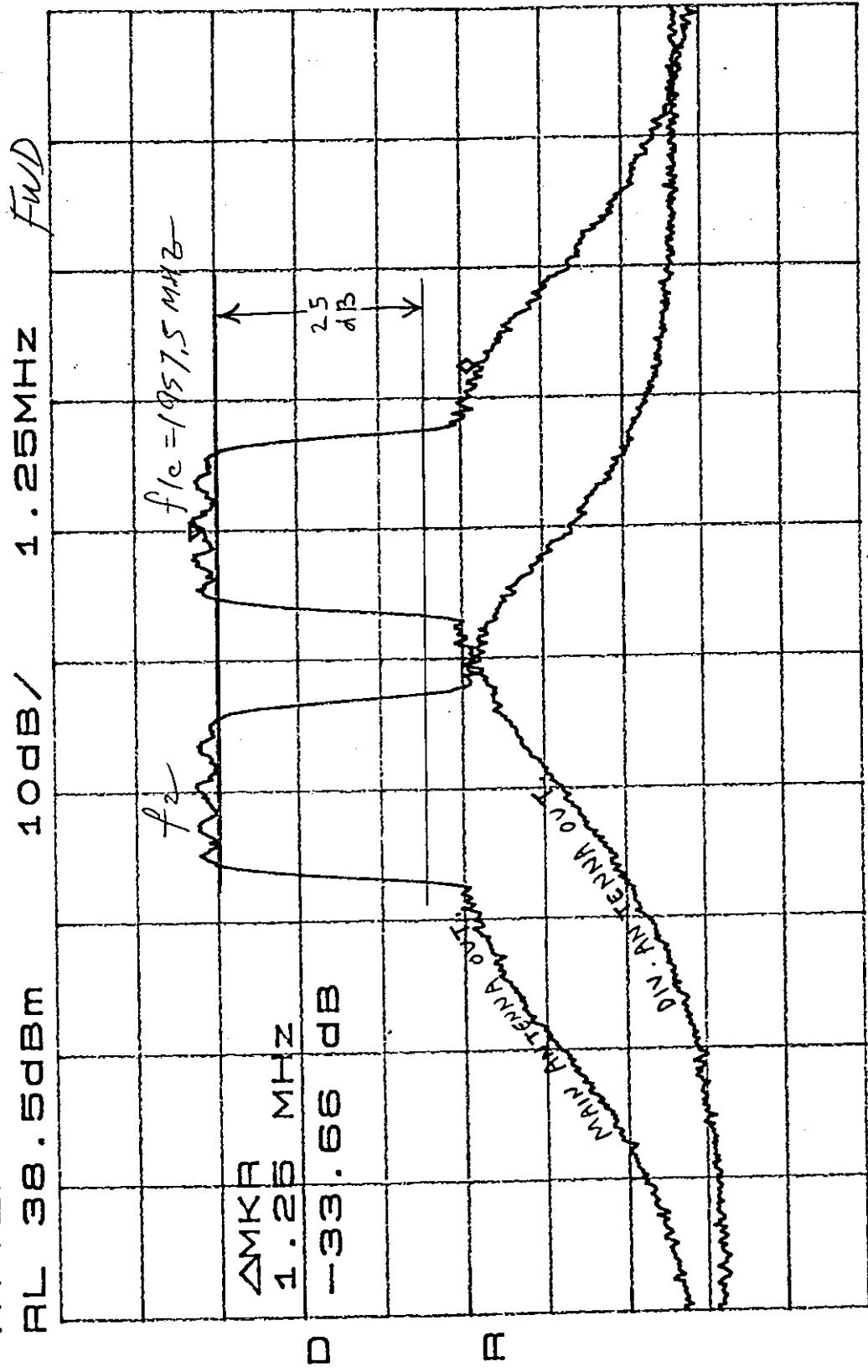
**Freq. error, Hertz,
vs.
Line voltage and Ambient Temperature**

I.C. RSS-131-1 (6.4)

Growth unit $P/0 = +38.45 \text{ dBm} = 7 \text{ W}$.

86th channel w/full power gain
 $\Delta \text{MKR} = -33.66 \text{ dB}$

ATTEN 20dB
RL 38.5dB
D



CENTER 1.95650GHz ΔMKR Mid-band SPAN 10.00MHz
*RBW 30kHz *VBW 100Hz SWP 8.40sec

Fig. P-1

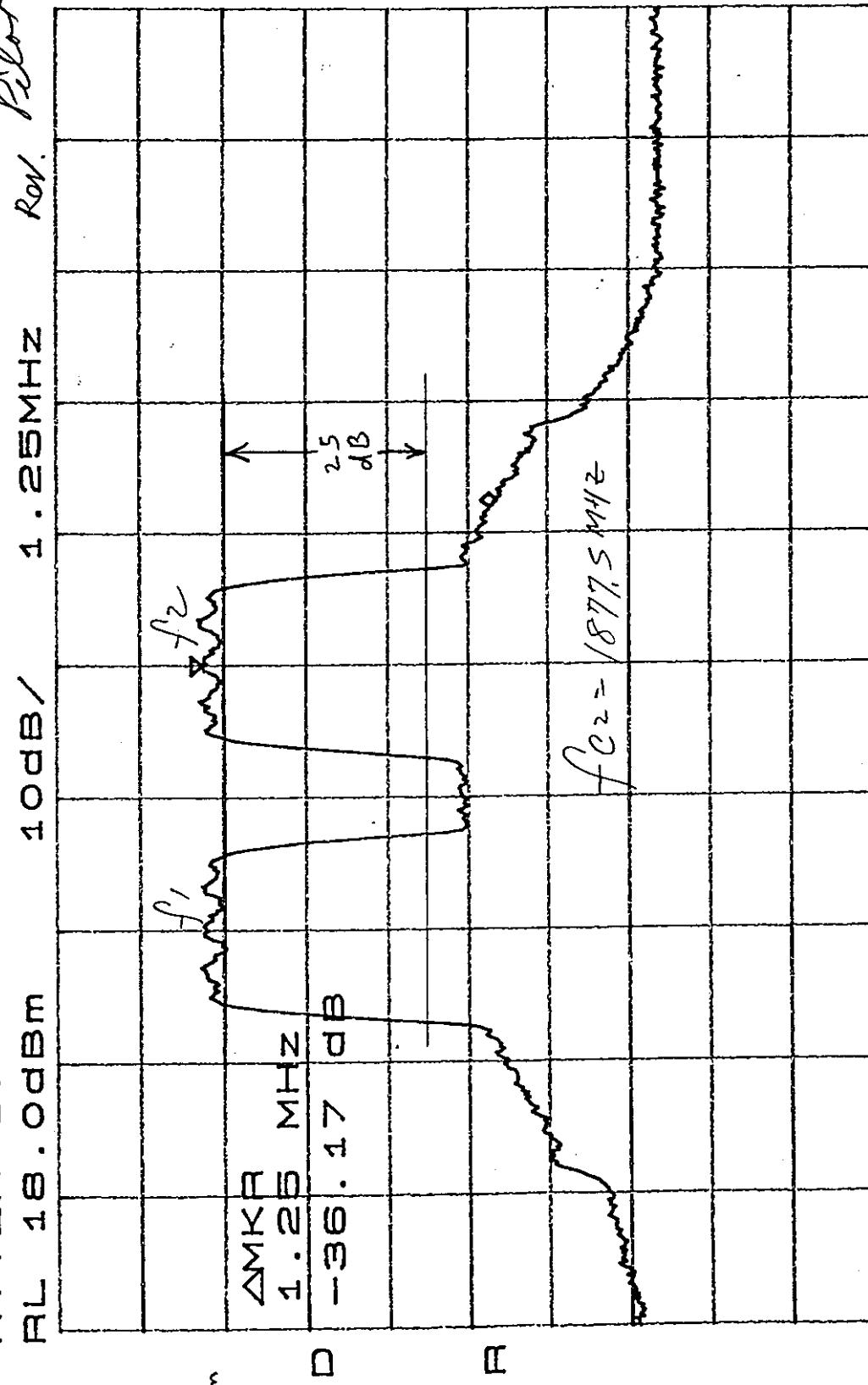
I.C. RSS-131-1 (6.4)

Growth unit
" " Block C

$P/0 = +21 \text{ dBm} = 12.5 \text{ mW}$ TOTAL PWR,
Both channel w/Full power gain

$\Delta \text{MKR} = 36.17 \text{ dB}$
Rev. Pilot only

ATTEN 10dB
RL 18.0dB



Power per
channel = +18 dBm

CENTER 1.87750GHz Mid-Band SPAN 10.00MHz
*RBW 30kHz *VBW 100Hz SWP 8.40sec

Fig. P-4